

Gujarat Maritime Board
Ahmedabad

DEVELOPMENT OF PORT FACILITIES AT POSITRA

DETAILED PROJECT REPORT - Final Report

Volume III : Reports on Model Studies and Field Investigations



HARRIS Frederic R. Harris, Inc.

in association with

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DEVELOPMENT OF PORT FACILITIES AT POSITRA

DETAILED PROJECT REPORT

VOLUME III :- REPORTS ON MODEL STUDIES & FIELD INVESTIGATIONS

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APPENDIX A

TOPOGRAPHIC SURVEY REPORT

BY

**INTERCONTINENTAL CONSULTANTS AND
TECHNOCRATS PVT. LTD., NEW DELHI.**

**DEVELOPMENT OF PORTS AT POSITRA
IN
STATE OF GUJARAT**

TOPOGRAPHIC SURVEY REPORT

June 1997



Intercontinental Consultants and Technocrats Pvt. Ltd.
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**DEVELOPMENT OF PORTS AT POSITRA
IN
STATE OF GUJARAT**
TOPOGRAPHIC SURVEY REPORT

1. General

The Gujarat Maritime Board is planning to develop ports and related facilities at Positra, at a distance of about 30 km from Okha Port in the Rann of Kutch area of the State of Gujarat. The Port development at Positra will comprise two parts : Positra-II and Positra-III. Both these ports will handle containers as well as petroleum products and LPG including coal. The infrastructure will comprise a central platform and breasting and mooring dolphins complete with cargo handling equipment as required. On shore, container yard facilities for storage and transhipment and storage tanks for different petroleum products as well as special facilities for storage of LPG will be provided. It will also be fully equipped for the off loading and through transport of coal to the stacking yard.

This part of the Report covers Topographic Survey of the on shore areas for providing on shore facilities.

2. Area Surveyed

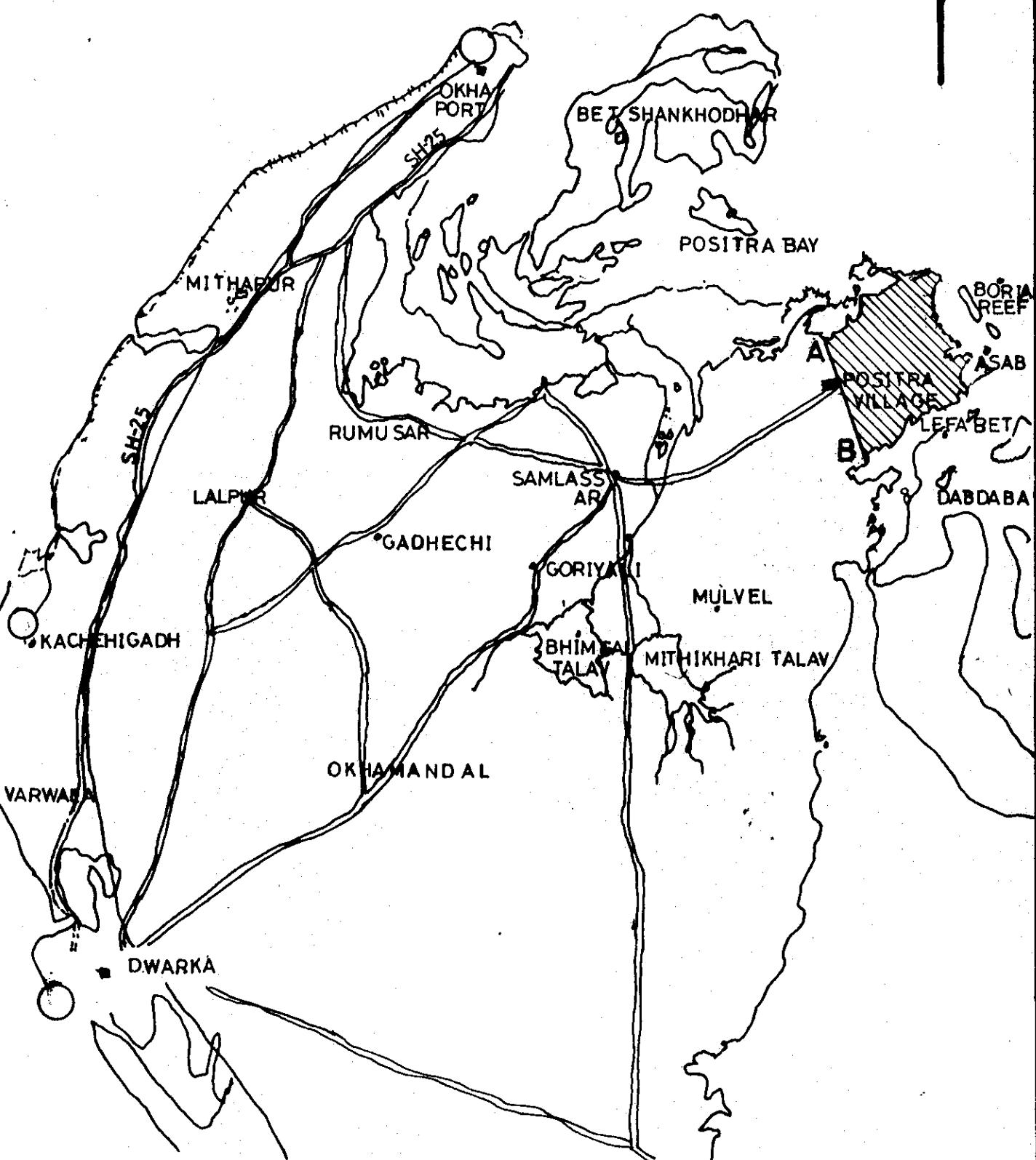
The area surveyed is near Positra village in the North-East direction as shown in Fig.-1. It is surrounded by sea on three sides. The area is approximately 9.5 sq. km. and covers the sand dunes on North and Eastern sides.

3. Methodology for Land Survey Works

3.1 Scope

The methodology for carrying out the land surveys covered the following :

- a) Preparation of contour survey maps, with spot levels. The levels were carried over from Survey of India Bench Mark (BM) of the area.
- b) Establishment of base line and grid system for defining the coordinates of the various areas.
- c) Preparation of survey map indicating all structures and prominent features, high water and low water levels, low tide, high tide and mean tide levels.
- d) Preliminary survey to identify existing control points to ensure their correctness.
- e) The horizontal control was fixed by :
 - i) Closed traverse
- f) The vertical control points were fixed by auto levels and closed by coming back to the starting point



AERA SURVEYED FOR POSITRA
PORTS-STATE OF GUJARAT



SCALE-150000

FIG-1

g) Spot levels and contour plans

For taking the spot level, the area was divided with main grids of 50 m x 50 m and levels observed at every intersection.

- h)** Boundary Pillars were provided at 500 metres centre to centre and at all corners. These were of size 300 x 300 x 1000 mm deep. Permanent pillars of size 1500 x 1500 x 2000 mm, 2 nos. were provided with steel plates of 150 x 150 x 10 mm embedded in concrete with 12 mm dia x 150 mm long anchor bolts. These were provided with punch lines and painted with anticorrosive paint.
- i)** Survey map indicating the contours, boundary pillars, permanent pillars and all permanent feature were prepared.

4. Land Survey Operations

4.1 Survey Team

The Consultants M/s Intercontinental Consultants and Technocrats Pvt. Ltd. mobilised the survey team at the end of March, 1997 consisting of the following personnel.

1. Survey Expert - 1 No.
2. Survey Engineer - 1 No.
3. Surveyors - 3 No.
4. Support Staff - as necessary

In addition to the members of the team, guidance was also available from Shri H.S. Verma, General Manager of the Consultants and Shri Avinash Patil, Dy. Project Manager (Ports) of M/s Fredric R. Haris (India) Pvt. Ltd. who visited the site during survey operations. Full cooperation was available from GMB technical staff posted at Okha port.

The entire survey work was completed in 2 months time.

4.2 Survey Instruments

The following survey instruments were used :

- a - Auto levels - 2 Nos.
- b - Theodolite - 1 No.
- c - Total Station - 1 No. (Topcorn GTS-304)
- d - Plane Tabling - 2 No.
- e - Measuring tapes - 50m - 3 Nos.

4.3 Transfer of Levels

The nearest Survey of India Bench Mark was available at Okha Port at a distance of about 30 km. The levels were transferred from this bench mark to the bench marks established at site (2 nos.) shown as A and B in Fig-1.

The correctness of the levels was ensured by starting and closing on the Survey of India Bench Mark at Okha port.

4.4 Horizontal Control

The horizontal control was fixed by Closed Traverse. Since about 1/3 area was covered by thorny thick bushes, triangulation was not possible. First grid pillars were provided and base line AB, indicated in Fig.-1, was established. The traversing followed along the boundary of the area surveyed. The closed traverse was set by measurement of coordinates directly read from Total Station. The number of traverse stations was 48.

4.5 Vertical Control

Vertical control points were fixed by auto level on all the traverse stations and were closed by coming back to the starting point. The closing error was 5 mm. The levels of the control points (boundary pillars) are given in **Table-1**.

4.6 Spot Levels and Contour Plans

For taking the spot levels, the area was divided into main grids of 50m x 50m, with reference to the base line AB, indicated in Fig.- 1.

The levels were observed at every intersection. For locating prominent physical features of the terrain, these grids were further divided into smaller grids of 25m x 25m. The field levels were so obtained as to get a contour interval of 0.5 metre. All the contours are indicated in the Map at **Annexure-A**. All spot heights in a mesh of 50m x 50m are also shown therein.

4.7 Coordinates

M/s Comaco Ltd., Bombay established coordinates of bore hole no. 10 at site with the help of G.P.S. All the coordinates of the permanent pillars and boundary pillars were transferred from this bore hole with the help of Total Station. The coordinates of permanent pillars and boundary pillars are given in **Table-2**.

4.8 Survey Map

The Survey Map has been prepared to a scale of 1:5000. All the boundary pillars and permanent pillars have been shown in the map. Important features of the area are also shown. The Survey Map is enclosed at **Annexure-B**. This also shows the 100m grid for defining the coordinates of various areas. The spot levels and contours are shown in the map at **Annexure-A** as mentioned in para 4.6 above.

TABLE - 1
Bench Marks List
Based on Survey of India Bench Mark R.L. 6.5487 (GTS)
Near Deputy Executive Engineer, Civil, Office – Okha Port

S.No.	Bench Marks No.	Reduced Levels (m)	Remarks
1.	B.M. -1	8.548	On Pillar No.1
2.	B.M. -2	10.020	On Pillar No.2
3.	B.M. -3	9.220	On Pillar No.3
4.	B.M. -4	6.013	On Pillar No.4
5.	B.M. -5	6.303	On Pillar No.5
6.	B.M. -6	5.258	On Pillar No.6
7.	B.M. -7	4.192	On Pillar No.7
8.	B.M. -8	4.425	On Pillar No.8
9.	B.M. -9	5.071	On Pillar No.9
10.	B.M. -10	6.344	On Pillar No.10
11.	B.M. -11	6.994	On Pillar No.11
12.	B.M. -12	6.990	On Pillar No.12
13.	B.M. -13	8.020	On Pillar No.13
14.	B.M. -14	8.557	On Pillar No.14
15.	B.M. -15	7.760	On Pillar No.15
16.	B.M. -16	7.306	On Pillar No.16
17.	B.M. -17	8.488	On Pillar No.17
18.	B.M. -18	9.055	On Pillar No.18
19.	B.M. -19	12.397	On Pillar No.19
20.	B.M. -20	14.984	On Pillar No.20
21.	B.M. -21	16.844	On Pillar No.21
22.	B.M. -22	16.097	On Pillar No.22
23.	B.M. -23	22.843	On Pillar No.23
24.	B.M. -24	21.530	On Pillar No.24
25.	B.M. -25	21.030	On Pillar No.25
26.	B.M. -26	12.673	On Pillar No.26
27.	B.M. -27	11.708	On Pillar No.27
28.	B.M. -28	5.587	On Pillar No.28
29.	B.M. -29	6.634	On Pillar No.29
30.	B.M. -30	4.883	On Pillar No.30
31.	B.M. -31	5.640	On Pillar No.31
32.	B.M. - A	7.014	A & B Pillars on Base line
33.	B.M. - B	16.705	And both are Main Pillars

Note : The Bench Mark height pertains to the top of the pillar. The height of the pillars above ground level is as under –

BM_s A & B = 1.00 m
 BM-1 to BM-31 = 0.50 m

TABLE - 2

**List of Stations with Coordinates on Modified Everest Spheroid
Reference Station - Bore hole No. 10**

Stations	Latitude	Longitude
Bore hole No. 10 T 10	° , " 22 25 03 N	° , " 69 11 16 E
P2	22 24 17.858237 N 69	69 10 42.110706 E
B	22 22 46.785307 N	69 10 49.019813 E
P-21	22 22 55.953570 N	69 10 45.765693 E
P-22	22 23 5.393646 N	69 10 42.201001 E
P-23	22 23 17.032404 N	69 10 38.213783 E
P-24	22 23 34.953758 N	69 10 31.726758 E
P-25	22 23 48.735783 N	69 10 26.884814 E
P-26	22 24 0.251670 N	69 10 22.928305 E
P-27	22 24 19.558759 N	69 10 16.214053 E
A	22 24 31.480973 N	69 10 11.885133 E
P-1	22 24 24.913104 N	69 10 27.454226 E
P-3	22 24 12.103503 N	69 10 57.054686 E
P-4	22 24 8.448397 N	69 11 0.892242 E
P-5	22 24 3.524022 N	69 11 25.397553 E
P-6	22 23 58.712743 N	69 11 37.939065 E
P-7	22 23 58.417789 N	69 11 46.845110 E
P-8	22 24 4.204084 N	69 12 2.183467 E
P-9	22 23 56.093611 N	69 11 53.697490 E
P-10	22 23 49.192010 N	69 11 50.354513 E
P-11	22 23 41.346748 N	69 11 51.902417 E
P-12	22 23 38.377276 N	69 11 48.024783 E
P-13	22 23 32.778476 N	69 11 55.698179 E
P-14	22 23 26.633037 N	69 11 57.307554 E
P-15	22 23 27.761471 N	69 11 53.873488 E
P-16	22 23 22.041786 N	69 11 48.173062 E
P-17	22 23 15.347947 N	69 11 41.356058 E
P-18	22 23 14.304757 N	69 11 24.292604 E
P-19	22 23 5.502901 N	69 11 8.192822 E
P-20	22 22 58.739114 N	69 10 54.809884 E
P-28	22 24 49.288671 N	69 10 29.796946 E
P-29	22 25 8.672866 N	69 11 1.036021 E
P-30	22 25 13.494733 N	69 11 36.764115 E
P-31	22 24 36.889686 N	69 11 26.068672 E

APPENDIX B

**REPORT ON METEOROLOGICAL
DATA FOR OKHA PORT**

BY
OCEAN ENGINEERING CENTRE,
I.I.T., MADRAS, CHENNAI.

**DETAILED PROJECT PROPOSAL FOR
POSITRA , GUJARAT**

**REPORT ON
METEOROLOGICAL DATA FOR OKHA PORT**

**CLIENT
FREDERIC R. HARRIS INC.
NEW DELHI**

**BY
Prof. V. SUNDAR
Dr. R. SUNDARAVADIVELU
Dr. R. NATARAJAN
Dr. S. R. GANDHI
Dr. S. MEENAKSHISUNDARAM**



**OCEAN ENGINEERING CENTRE
INDIAN INSTITUTE OF TECHNOLOGY
MADRAS**

NOVEMBER 1996

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REPORT ON METOROLOGICAL DATA AT OKHA PORT

1. INTRODUCTION

Gujarat Maritime Board has plans to develop various ports along the Gujarat coast as shown in Fig. 1. Gujarat Maritime Board has appointed **Frederic R. Harris India private limited** to prepare the detailed project report for **Positra Port**. Frederic R. Harris Inc. have appointed **IIT, Madras** to perform certain tasks in connection with the development of master plan. This report gives all the details of analysis of meteorological data at **Okha Port** which is the nearest meteorological observatory for the location of Positra.

The port development at Positra is comprising of Positra I and Positra II. Positra I is approximately located $22^{\circ}28'24''$ N and $69^{\circ}08'48''$ E. Positra II is located at $22^{\circ}25'15''$ N and $69^{\circ}11'24''$.

2. DATA COLLECTION

The meteorological data at **Okha** have been collected from **I.M.D. Pune** and are given in Annexure I.

- a. Fig I.1 and Fig I.2 gives the wind rose diagram collected from **I.M.D. Pune** for the period 1969-1985 for 0830hrs and 1730hrs respectively for January to December.
- b. Fig I.3 gives the Wind rose diagram for 0830 hrs and 1730 hrs for the period 1969 - 1985, for Jan, Feb & March.
- c. Fig.I.4gives the wind rose diagram for 0830 hrs and 1730 hrs for the period 1969-1985 for Oct, Nov & Dec.
- d. Fig. I.5 gives the wind rose diagram for 0830 hrs and 1730 hrs for the period 1969 - 1985 for July, Aug & Sept.
- e. Fig. I.6 gives the wind rose diagram for 0830 hrs and 1730 hrs for the period 1969 - 1985 for Oct, Nov & Dec.

f. Fig. I.7 gives the representative wind rose diagram considering all the months for the period 1969 - 1985 which can be used for design purposes.

3. WIND

The Wind Rose diagram shown in Fig I.1 to Fig I.7 should be read considering the wind directions shown in Fig. 2.

The wind rose diagram shown in Fig. I.3 indicates that during the month of January the wind direction in the morning is from North East and in the evening it is from the North West. The mean wind speed during the month is generally under 22 Kmph.

During February to April, from the Fig I.3 and Fig I.4 the wind direction generally changes from North to NorthWest in the morning and in the evening it is from the NorthWest. The mean wind speed during this period is generally under 24 Kmph which can be read from the above Figures.

From May to September the predominant direction of the winds in the morning and in the evening it is SouthWest to West. The mean wind speed is usually under 30 Kmph during this period.

The predominant wind direction during the months of October to December the wind direction change in the morning from North to NorthEast and it is NorthWest in the evening. The mean wind speed during this period is generally below 23 Kmph.

The wind rose diagram shown in figure 1.7 is prepared using the method of probability percentage for the whole period, including all seasons. The wind rose diagram shows that general direction of the wind is from West to North-west.

4. SEASONS

The climate in a year can be divided into four seasons comprising non-monsoon during Jan to May, southwest monsoon season during June to September and Northeast monsoon season during October to December as generally observed in the country.

5. CYCLONES AND DEPRESSIONS

Wind speed upto 60 Kmph is described as cyclonic depression, and in the range of 60 Kmph to 80 Kmph as storm, and wind speeds exceeding 80 Kmph, signal severe storm

TABLE 2

Frequency of Occurrence of Depressions / Storm within 2.5° of Okha

during the Period 1891-1970

MONTH	DEPRESSION	STORM	SEVERE STORM	TOTAL
January	0	1	0	1
February	0	0	0	0
March	0	0	0	0
April	1	0	1	2
May	0	0	2	2
June	7	4	7	18
July	8	1	0	9
August	3	1	0	4
September	8	2	1	11
October	3	3	0	6
November	4	0	2	6
December	0	0	0	0
Total	34	12	13	59

The number of depressions is maximum in the months of June, July and September. The number of depressions and storms is zero in the months of February, March and December. The number of tropical storms in the month of January is zero. The storm in January does not pertain to a tropical storm. It relates to a western disturbance which attained 'storm' intensity while moving eastwards over the North Arabian sea. The diagrams (numbering 13) showing Tracks of storms depressions are enclosed as (Annexure II)

The total number of tropical disturbances within 77km of Okha for the period 1891-1970 is shown in Table 3.

TABLE 3

Frequency of Occurrence of Depressions / Storms within 77kms of Okha during the Period 1891-1970

MONTH	DEPRESSION	STORM	SEVERE STORM	TOTAL
January	0	0	0	0
February	0	0	0	0
March	0	0	0	0
April	0	0	1	1
May	0	0	0	0
June	2	0	1	3
July	3	0	0	3
August	1	0	0	1
September	1	1	0	2
October	2	0	0	2
November	2	0	0	2
December	0	0	0	0
Total	11	1	2	14

Out of these 11 are depressions, 2 are tropical storms and 2 are severe tropical storms. January, February, March, and December, are months with the number of tropical storms zero. In April and June one severe storm each has occurred during the period 1891-1970. The maximum number of depressions recorded is in the month of July which also is the month with maximum rainfall.

6. RAINFALL

Rainfall varies from year to year. For example the total rainfall in the period from **October 1975 to June 1980** was **0 mm**. The heaviest rainfall recorded in one day during the period **1967-1995** is **283.3 mm** which is recorded on **10-08-1973**.

The average monthly rainfall for the period **1967-1995** which is calculated using the method of average given below:

Average rainfall for a particular month for a certain period of years = $\Sigma x/n$

where Σx - is the total rainfall for a particular month for a certain period of years and n - the number of years.

The average rainfall for the month of July is **145.62mm** which is the wettest month of the year.

Average annual rainfall is **304.48mm**.

The average of 10% of the heaviest rainfall recorded during the period is **101.67mm**. These values are obtained from Fig. 3 which is drawn using Meteorological data.

The Average monthly rainfall and maximum number of rainy days is given in Table 2 which is as follows

TABLE 4

MONTH	RAINFALL IN MM	MAXIMUM NUMBER OF RAINY DAYS
January	0.94	1
February	2.08	1
March	1.46	2
April	0.08	0
May	0.69	1
June	47.22	8
July	145.62	12
August	69.06	11
September	19.87	7
October	5.87	7
November	10.28	4
December	1.31	1
TOTAL	304.48	

7. TEMPERATURE

The mean temperatures recorded during the period of 1967-1985 are presented in Table 3 using the method of Average.

The mean maximum temperature are of the order of 33°C while the mean minimum temperature is of the order of 18°C .which is shown in Figure 4 which is drawn based on Table 3.

The highest maximum temperature recorded in the period 1967-1985 is 39.8°C ,recorded on 11-06-1969, while the lowest minimum temperature is 10.9°C recorded on 10-02-1968.

TABLE 5

MONTH	MAXIMUM TEMPERATURE	MINIMUM TEMPERATURE
JANUARY	24	18.7
FEBRUARY	24.6	19.3
MARCH	27.3	21.8
APRIL	29.8	24.4
MAY	31.8	26.6
JUNE	32.5	27.7
JULY	31.1	26.7
AUGUST	30	25.7
SEPTEMPER	30.1	25.4
OCTOBER	30	24.8
NOVEMBER	28.6	23.5
DECEMBER	25.8	20.6

TABLE 6

Temperature variation in 24 hours

YEAR	MONTH	DATE	MAXIMUM	MINIMUM	DIFFERENCE
1967	October	22	33.4	22.4	11
1970	June	30	35.3		
	July	1		26.7	8.5
1973	June	9	36.2	27.3	8.9
	July	9	33.5		
		10		24.5	9
	October		33.4	22.3	
	November	30	31.6		
	December	1		27.7	3.8
1977	September	3	31.1	21.8	9.2
1981	September	24	31	24.4	6.6

From the above data it is clear that the maximum temperature variation within 24 hours is 11°C

8. VISIBILITY

The meteorological datas obtained for Okha port gives us the Number of Days with visibility in KM as follows:

- a. Less than 1 KM
- b. Between 01 - 10 KM
- c. Between 10 - 20 KM
- d. Greater than 20 KM

Based on this the visibility less than 1 KM, is sorted out from the Data and presented in Table 7. It is clear from the table that the visibility less than 1 KM in Okha area during the month of March and June has occurred totally for 10 days between 1967 - 1985.

TABLE 7

No. Of days with visibility less than 1 KM

YEAR	1967	1971	1972	1973		1975	1984	TOTAL
TIME (hrs)	0830	0830	0830	0830	1730	0830	0830	
MONTH								
JANUARY	-	-	-	-	-	-	-	-
FEBRUARY	1	-	-	1	1	-	-	3
MARCH	-	-	2	2	2	1	3	10
APRIL	-	1	-	1	-	1	-	3
MAY	-	-	-	-	-	-	-	-
JUNE	-	-	-	4	6	-	-	10
JULY	-	-	-	-	-	-	-	-
AUGUST	-	-	-	-	-	-	-	-
SEPTEMBER	-	-	-	-	-	-	-	-
OCTOBER	-	-	1	-	-	-	1	2
NOVEMBER	1	-	-	-	-	-	-	-
DECEMBER	-	-	-	-	-	-	-	-

9. RELATIVE HUMIDITY

Using meteorological data, the Relative Humidity at Okha port is maximum in the morning and minimum in the evening which can be seen from Table 8 and Figure 5 which is arrived by using the Methods of Average.

The relative humidity is maximum during the SouthWest monsoon season and is around 85% and minimum during winter around 60%.

TABLE 8

Relative Humidity

MONTH	08.30HRS	17.30HRS
	%	%
JANUARY	63.7	60.6
FEBRUARY	71.8	66.8
MARCH	79.7	73.6
APRIL	83.8	77.4
MAY	80.4	77.2
JUNE	80.7	77
JULY	84.1	80.2
AUGUST	86.5	82.3
SEPTEMBER	84.8	80.7
OCTOBER	81	77.5
NOVEMBER	68.2	67.6
DECEMBER	62.8	59.8

10. SUMMARY

In order to prepare the detailed project report for Positra I & II, the meteorological data at Okha port, which is the nearest IMD, is collected from IMD, Pune for the period 1967 - 1995. Based on the analysis of above data the following observations have been made.

The wind rose Diagrams show the maximum mean wind speed is 30 Kmph during the month of May to September. When Severe Storms & Depression occurs the wind speed is more than 60 Kmph which occurs mostly during in the month of May, June, October and November. So, extra precautions should be taken in these months. During the month of February the occurrence of Storm and Depression is nil. These observations

are taken from the Table 1 which is obtained from Tracks of Storms and Depressions published by IMD, Pune.

The heaviest Rainfall occurred in the month of July for the period 1967 - 1995 and the month of April is having zero rainy days. The work can be carried out almost through out the year except for the month of July and August. Number of Rainy days during the month of June, September and October is less than 10. The average of 10% of the heaviest rainfall recorded during the period 1967 - 1985 is 101.67 mm.

The visibility less than 1 KM has occurred totally for ten days during the month of March and June between 1967 - 1985.

The maximum temperature recorded on June 11th 1969, is 39.8°C and the minimum temperature recorded in February 10th 1968 is 10.9°C.

The maximum variation in temperature in 24 hours is 11⁰C.

In general, Relative Humidity is almost above 80 % during the month of March to October at 0830 hrs.

(Dr. V. SUNDAR)

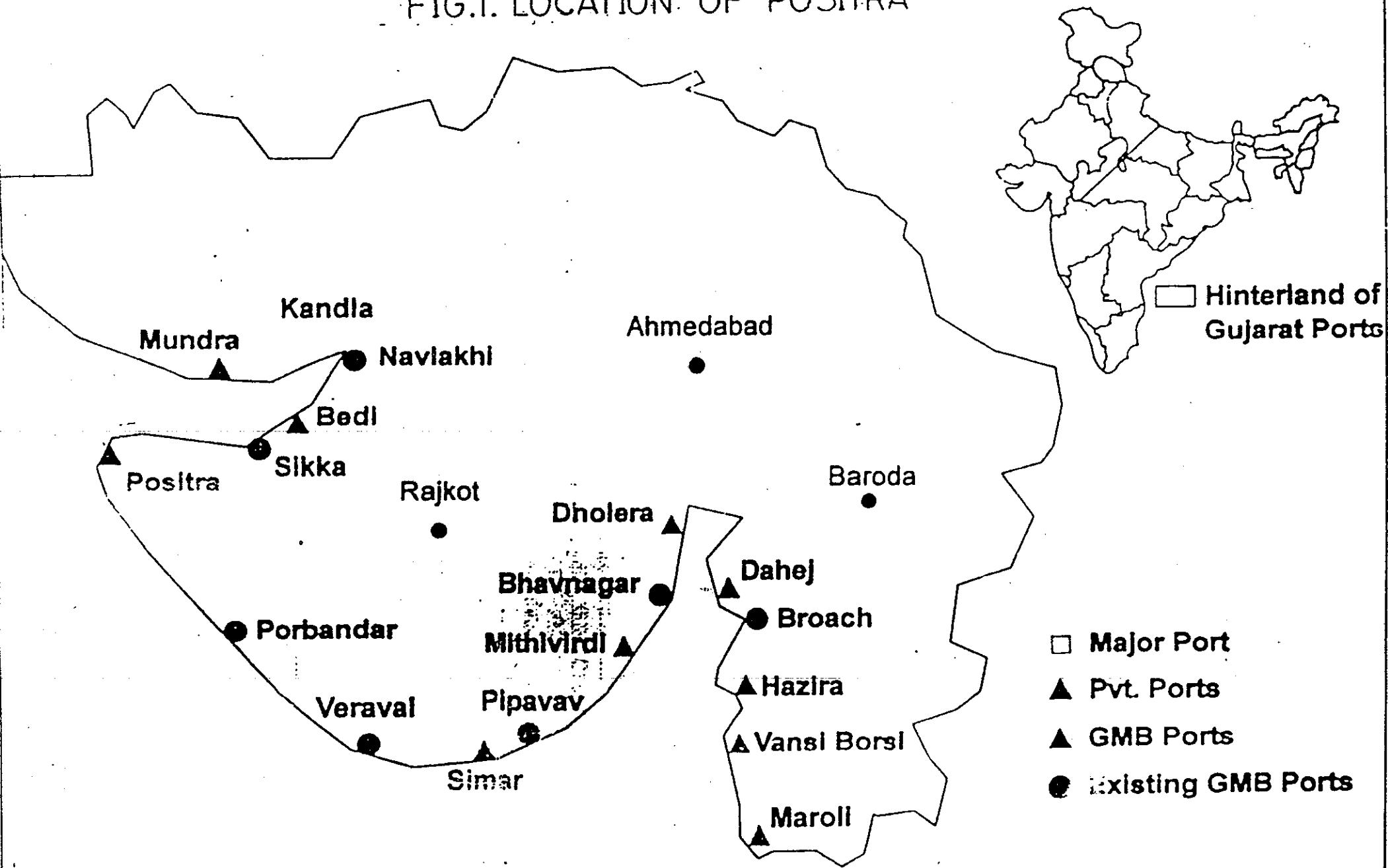
(Dr. R. SUNDARAVADIVELU)

(Dr. R. NATARAJAN)

(Dr. S.R. GANDHI)

(Dr. S. MEENAKSHISUNDARAM)

FIG.1. LOCATION OF POSITRA



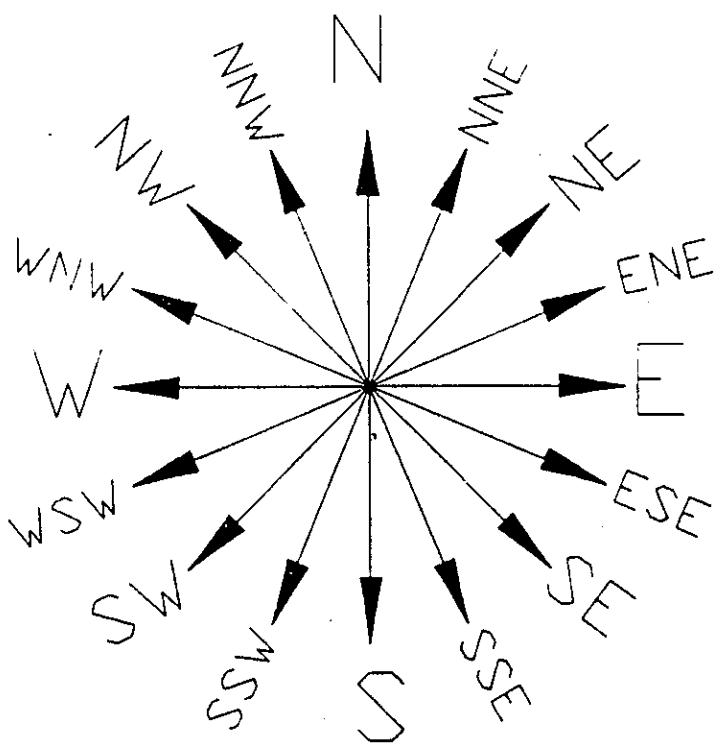


Fig.2 WIND DIRECTIONS

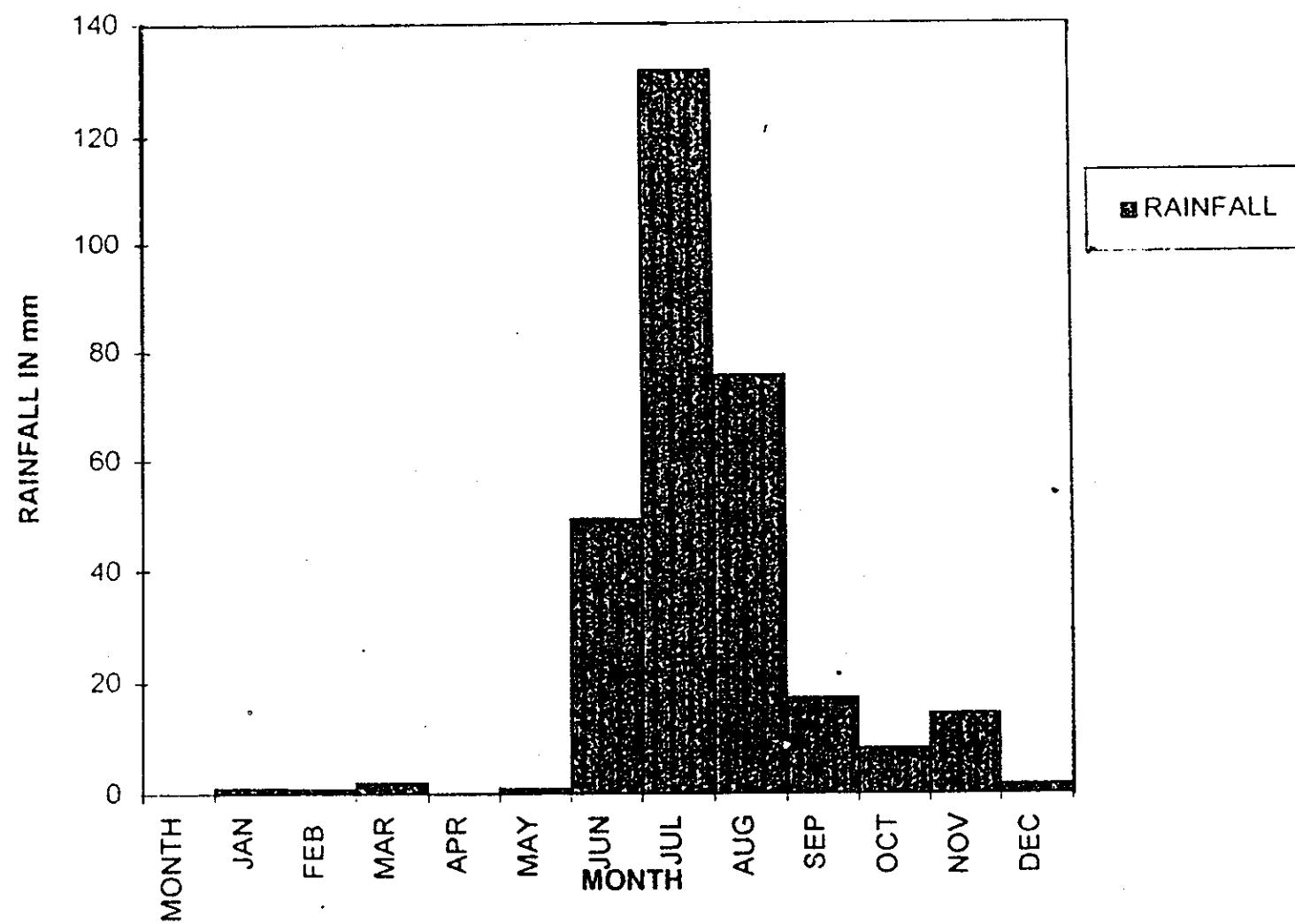


FIGURE 3 RAINFALL

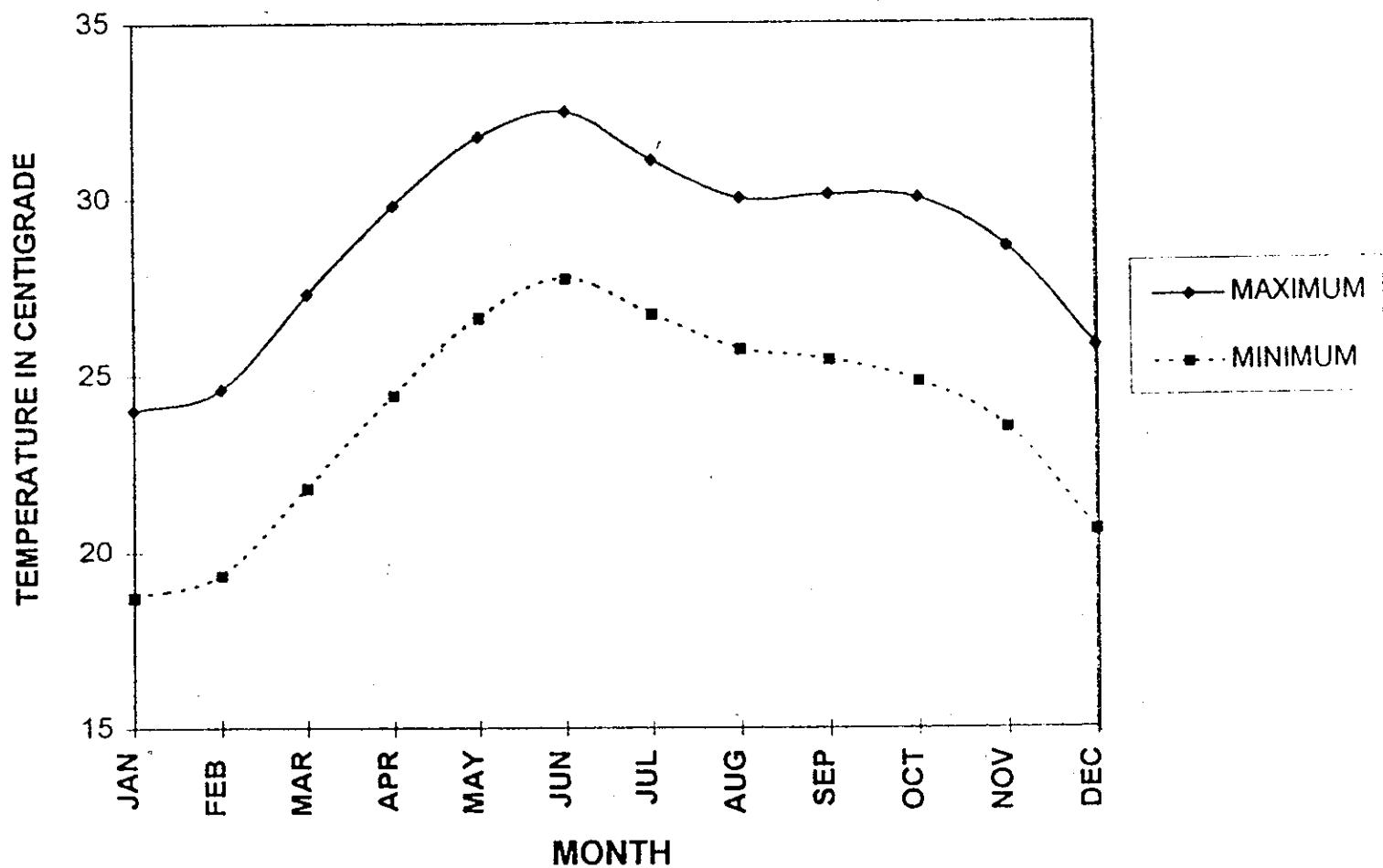


FIGURE 4 MINIMUM AND MAXIMUM TEMPERATURE

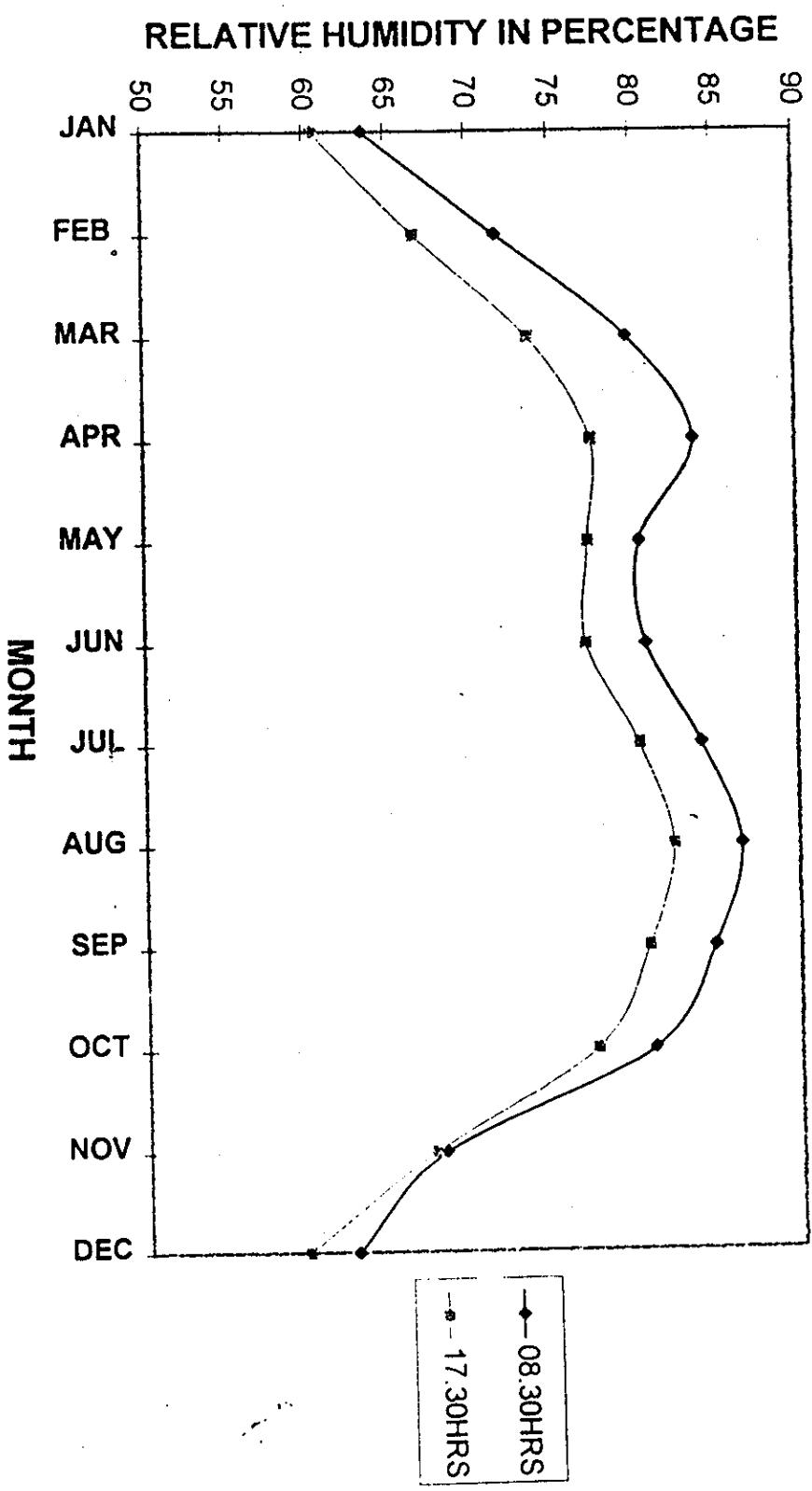
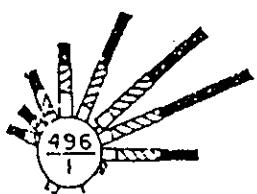


FIGURE 5 RELATIVE HUMIDITY

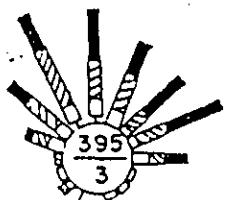
WIND ROSES

FOR: OKHA

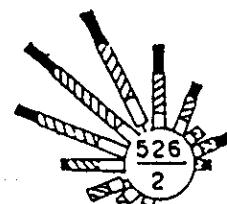
0830 HRS. I.S.T.



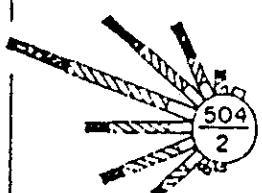
JANUARY



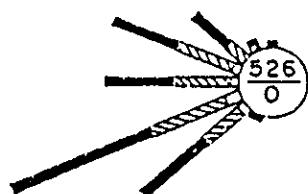
FEBRUARY



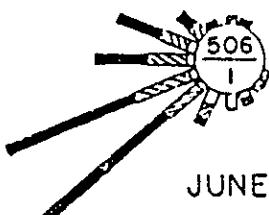
MARCH



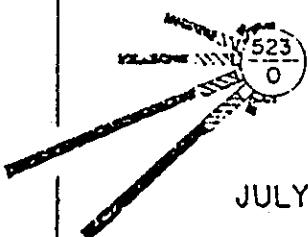
APRIL



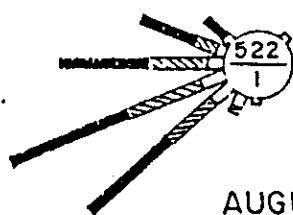
MAY



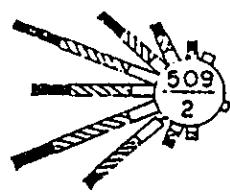
JUNE



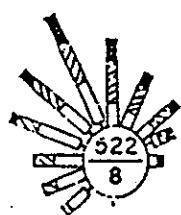
JULY



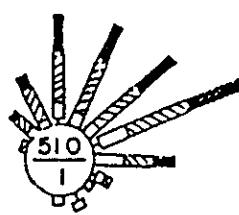
AUGUST



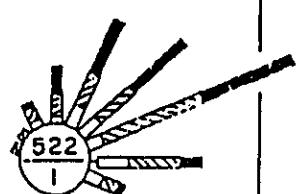
SEPTEMBER



OCTOBER

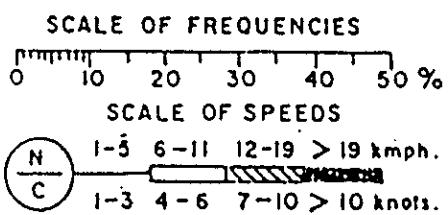


NOVEMBER



DECEMBER

FIG. 1.1



N : TOTAL NUMBER OF OBSERVATIONS.

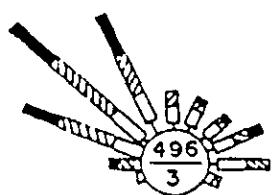
C : TOTAL NUMBER OF CALMS IN PERCENTAGE FREQUENCIES.

PERIOD: 1969 - 85

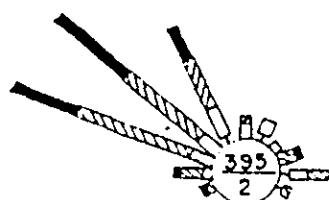
WIND ROSES

FOR OKHA

1730 HRS. I.S.T.



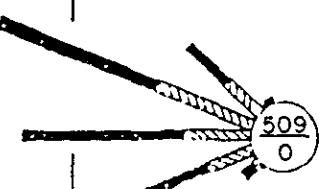
JANUARY



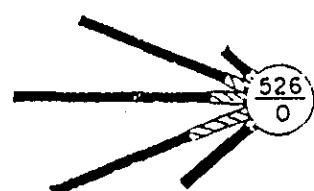
FEBRUARY



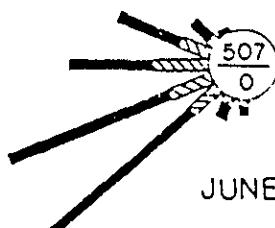
MARCH



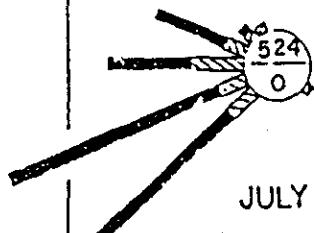
APRIL



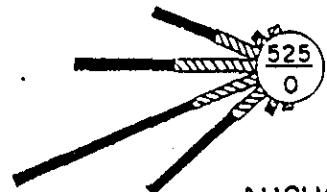
MAY



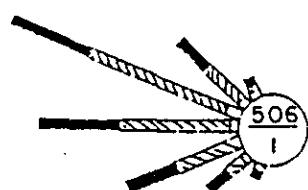
JUNE



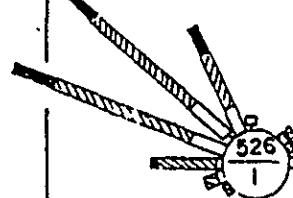
JULY



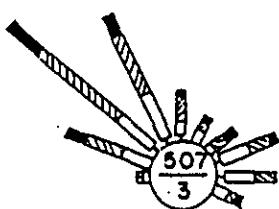
AUGUST



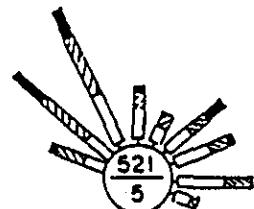
SEPTEMBER



OCTOBER



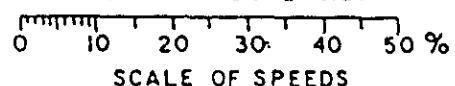
NOVEMBER



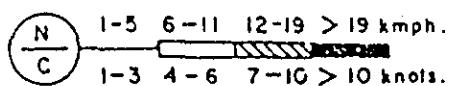
DECEMBER

FIG. 1.2

SCALE OF FREQUENCIES



SCALE OF SPEEDS



N : TOTAL NUMBER OF OBSERVATIONS.

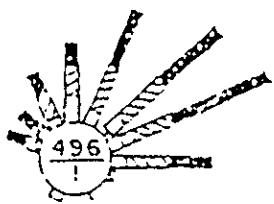
C : TOTAL NUMBER OF CALMS IN PERCENTAGE FREQUENCIES

PERIOD: 1969 - 85

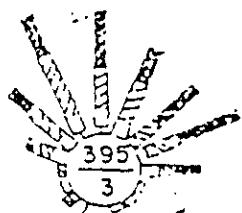
WIND ROSES

FOR: OKHA

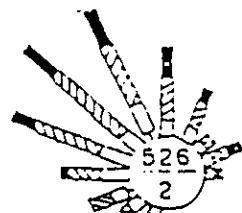
0830 HRS. I.S.T.



JANUARY

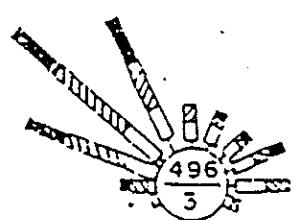


FEBRUARY

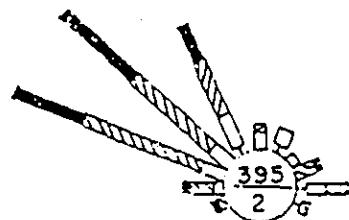


MARCH

1730 HRS. I.S.T.



JANUARY

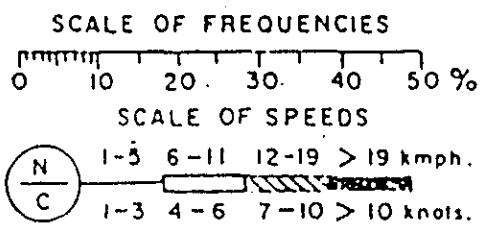


FEBRUARY



MARCH

FIG I.3



N : TOTAL NUMBER OF OBSERVATIONS.

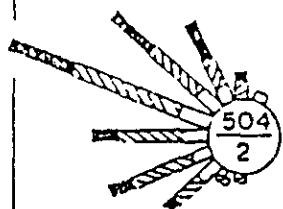
C : TOTAL NUMBER OF CALMS IN PERCENTAGE FREQUENCIES

PERIOD: 1969 - 85

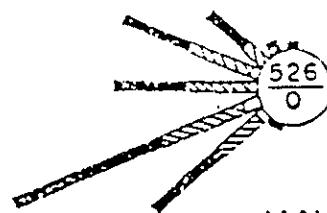
WIND ROSES

FOR OKHA

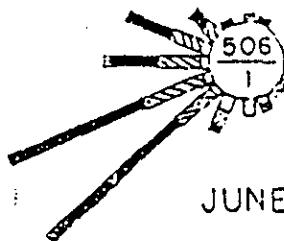
0830 HRS. I.S.T.



APRIL



MAY

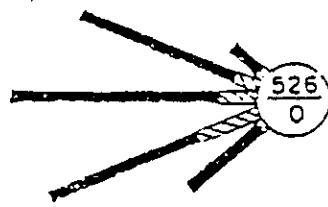


JUNE

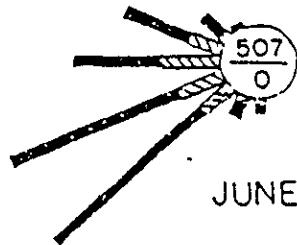
1730 HRS. I.S.T.



APRIL

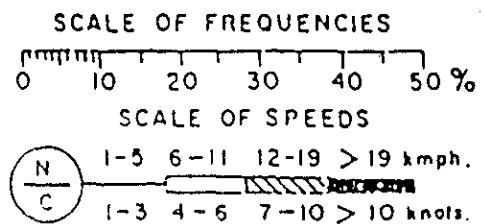


MAY



JUNE

FIG.14



N : TOTAL NUMBER OF OBSERVATIONS.

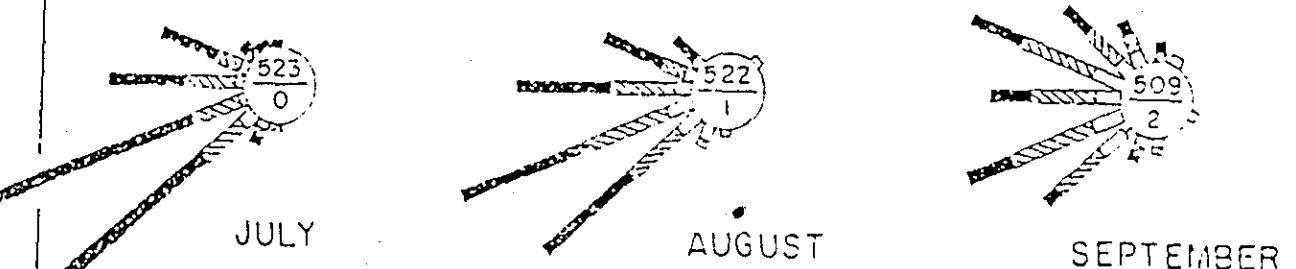
C : TOTAL NUMBER OF CALMS IN PERCENTAGE FREQUENCIES

PERIOD: 1969 - 85

WIND ROSES

FOR : OKHA

0830 HRS.I.S.T.



1730 HRS.I.S.T.

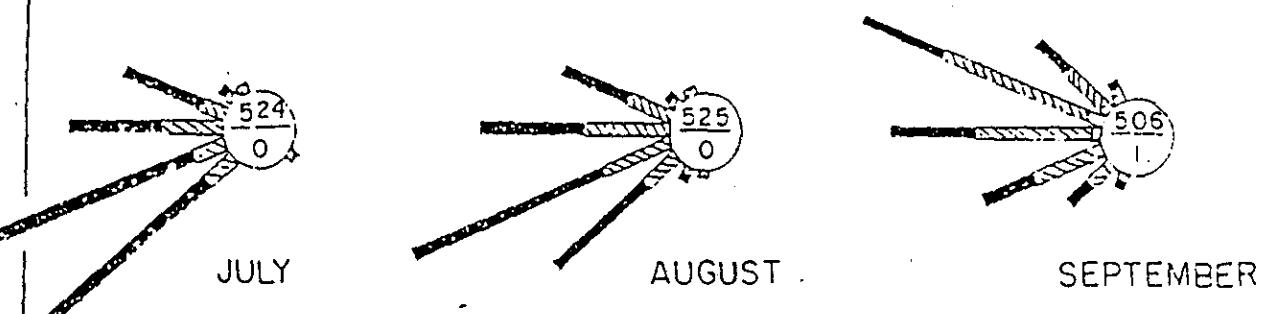
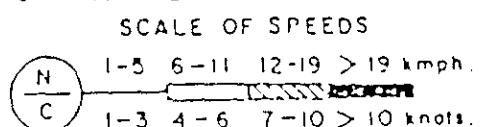
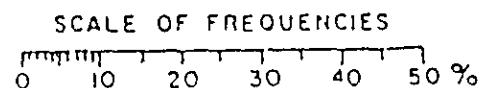


FIG. I.5



N : TOTAL NUMBER OF OBSERVATIONS.

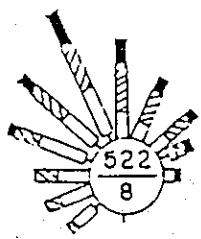
C : TOTAL NUMBER OF CALMS IN PERCENTAGE FREQUENCIES

PERIOD: 1969 - 85

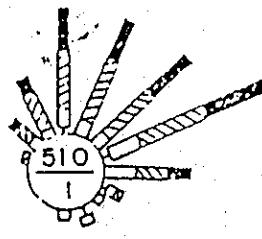
WIND ROSES

FOR: OKHA

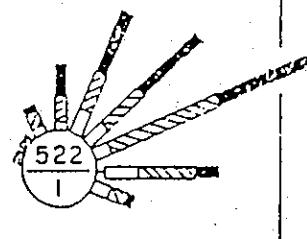
0830 HRS. I.S.T.



OCTOBER

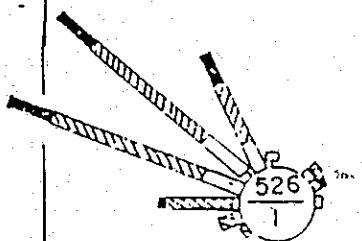


NOVEMBER

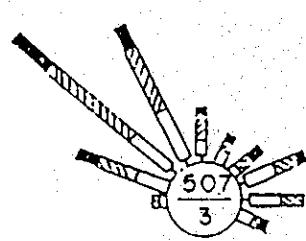


DECEMBER

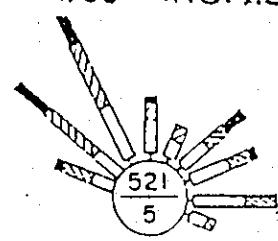
1730 HRS. I.S.T.



OCTOBER

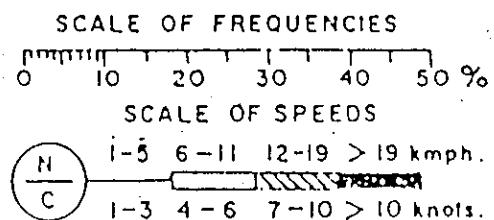


NOVEMBER



DECEMBER

FIG. 1.6



PERIOD: 1969 - 85

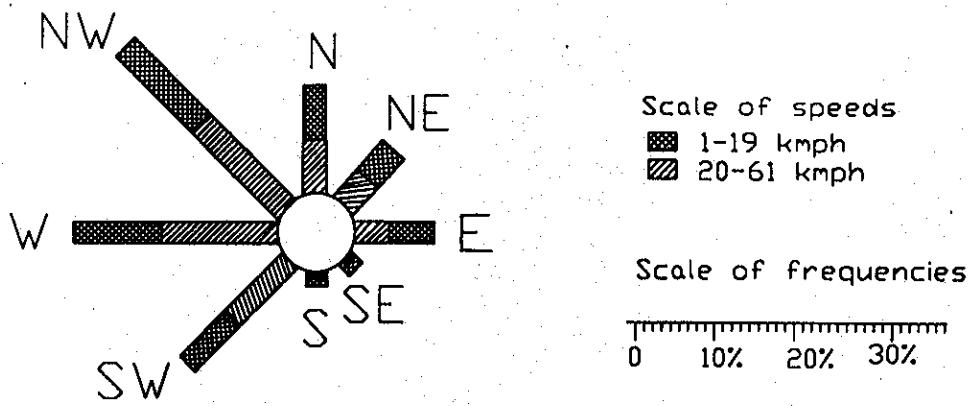


Fig. I.7 Wind rose diagram
for Okha port(annual)

ANNEXURE I

METEOROLOGICAL DATA

The following table which is obtained from I.M.D.Pune, for Okha port for the period 1967 to 1985, in Tabulated form is given below and which is to be read as follows:

Abbreviations used for Monthly Surface Data:

MN	-	Month
MMAX	-	Mean Maximum Temperature
HMAX	-	Heaviest Maximum Temperature
DT	-	Date
MMIN	-	Mean Minimum Temperature
LMIN	-	Lowest Minimum Temperature
DT	-	Date
MRF	-	Total Rainfall in the Month
HVYRF	-	Heaviest Rainfall in 24 hrs
DT	-	Date
RD	-	Number of Rainy Days
MWS	-	Mean wind speed in (Kmph)

INDEX	YEAR	MN	MMAX	HMAX	DT	MMIN	LMIN	DT	MRF	HVYRF	DT	RD	MWS
42730	1967	1	23.2	26.2	23	17.2	15.1	13	0	0		0	21.5
		2	25.2	27	21	19.2	17.1	11	0	0		0	16.7
		3	27.7	30.4	19	22.4	20.5	16	39.4	36.6	24	2	18.1
		4	29.4	31.7	27	24.1	21.7	4	0	0		0	20.5
		5	31.7	34	17	26.5	25	12	0	0		0	24.8
		6	32	34.6	14	27.1	25	26	114.4	77.4	26	7	21.1
		7	30.9	32.7	2	26	22.9	26	538.3	135.8	5	12	27.2
		8	30	31.1	31	25.6	24.2	1	127.1	76.6	23	3	21.9

9	30.3	31.1	2	25.7	23.9	18	5.8	4	17	1	20.7
10	30.1	33.4	22	24.4	22.4	22	0	0	0	0	13.9
11	28.2	30.3	5	23.3	21.3	8	0	0	0	0	13.9
12	25.3	27.5	1	19.5	16.4	30	27.8	24.2	16	1	21.5
1968	1	23.8	28.4	6	17.8	14.1	23	7	7	1	20.5
2	23.9	29.8	26	18	10.9	10	4.5	4.5	19	1	18.9
3	27.2	29.8	19	21.4	20	13	0	0	0	0	20.3
4	28.9	30.2	22	23.5	22	8	0	0	0	0	19.7
5	30.8	32.2	25	25.4	23.3	10	0	0	0	0	20.3
6	32.5	35.1	17	27.3	26	1	0.2	0.2	18	0	26.1
7	31.9	32.9	4	27	25.9	29	9	4.1	5	1	26.5
8	29.3	30.6	4	25.2	24	8	131.1	78	8	1	26.5
9	30.5	31.7	25	25.2	24	8	0.7	0.5	7	0	28.5
10	30.6	33.6	22	25.2	23.9	7	0	0	0	0	14.6
11	29.6	30.9	10	23.7	21.9	2	0	0	0	0	17
12	25.8	28.5	9	20.4	16.5	27	0	0	0	0	15.4
1969	1	24.1	26	25	18	15.2	14	0	0	0	18.3
2	24.7	27.4	20	19.1	17.1	5	0	0	0	0	18.1
3	27.5	33.2	30	21.9	19.7	10	0	0	0	0	19.1
4	30.1	31.4	21	24.3	22.3	5	0	0	0	0	19.7
5	31.9	32.9	30	24.3	22.3	5	0	0	0	0	20.6
6	33.1	39.8	30	26.5	25	8	0	0	0	0	25.2
7	31.8	33.4	11	27.5	26.5	6	0	0	0	0	22.8
8	29.5	30.6	7	14	14	26.7	24.2	22	22	8	26.4
9	29.9	31.3	3	24.4	22.5	28	0	0	0	0	23.3
10	29.5	31.3	23	23.4	21.3	12	0	0	0	0	20.9
11	29	32.5	9	23.3	20	30	13	13	30	0	13.3
12	26.8	28.8	10	21.1	18.6	28	0	0	0	0	17.6

1972

1	24.7	26.5	5	19.7	16.3	20	18	18	25	0	18.8
2	25	27.4	28	19.8	16.9	3	0	0	28	0	17.5
3	26.9	28.7	31	21.8	20.2	3	0	0	31	0	20.2
4	29.8	31.5	30	24.6	22.4	6	2	2	15	0	18.9
5	31.7	32.5	27	27	24	31	19.7	19.7	31	1	23.9
6	32.8	35.3	1	28.3	26.7	30	10.5	8.4	30	1	20.6
7	31	33	1	26.8	22.9	6	223.8	75.2	6	7	25.1
8	30.2	32	8	25.9	23.6	29	284.1	91.5	15	11	21.3
9	29.6	32	32	25.5	23.9	8	64.3	23.7	8	6	16.1
10	30.3	33.5	13	26.1	24.6	24	0	0	31	0	15.8
11	28.4	31.8	1	23	18.4	20	0	0	30	0	15.6
12	25.2	26.9	6	20	16.6	23	0	0	31	0	17.2
13	27.2	31.9	15	21.3	18.1	6	0	0	31	0	17.6
14	30.6	36.4	20	24.7	22.7	1	0	0	30	0	17.8
15	31.8	33	22	22.7	22.7	1	0	0	31	0	17.8
16	31.5	34.3	3	27.2	23.3	25	71.8	55	25	4	24.8
17	29.9	31.3	7	26	23.8	14	55	17.4	17	7	28.2
18	29.8	30.9	27	25.6	23.4	31	41.4	10.5	31	7	24.4
19	30.1	30.8	30	25.1	23.7	1	10.3	9	1	1	15.3
20	29.6	33.3	24	23.9	21.6	29	0	0	31	0	14.3
21	28	29.9	18	22.7	20.4	23	0	0	30	0	14.3
22	26.1	27.8	6	20.8	18	20	0	0	31	0	16.1
23	24.5	26.2	21	19.7	15.7	26	0	0	31	0	17.2
24	23.1	25.6	21	18	15.8	13	6.3	4.4	5	1	23.9
25	26.4	31.1	15	21	18.7	3	0	0	31	0	18.3

1970

1	24.7	26.5	5	19.7	16.3	20	18	18	25	0	18.8
2	25	27.4	28	19.8	16.9	3	0	0	28	0	17.5
3	26.9	28.7	31	21.8	20.2	3	0	0	31	0	20.2
4	29.8	31.5	30	24.6	22.4	6	2	2	15	0	18.9
5	31.7	32.5	27	27	24	31	19.7	19.7	31	1	23.9
6	32.8	35.3	1	28.3	26.7	30	10.5	8.4	30	1	20.6
7	31	33	1	26.8	22.9	6	223.8	75.2	6	7	25.1
8	30.2	32	8	25.9	23.6	29	284.1	91.5	15	11	21.3
9	29.6	32	32	25.5	23.9	8	64.3	23.7	8	6	16.1
10	30.3	33.5	13	26.1	24.6	24	0	0	31	0	15.8
11	28.4	31.8	1	23	18.4	20	0	0	30	0	15.6
12	25.2	26.9	6	20	16.6	23	0	0	31	0	17.2
13	27.2	31.9	15	21.3	18.1	6	0	0	31	0	17.6
14	30.6	36.4	20	24.7	22.7	1	0	0	31	0	17.8
15	31.8	33	22	22.7	22.7	1	0	0	31	0	17.8
16	31.5	34.3	3	27.2	23.3	25	71.8	55	25	4	24.8
17	29.9	31.3	7	26	23.8	14	55	17.4	17	7	28.2
18	29.8	30.9	27	25.6	23.4	31	41.4	10.5	31	7	24.4
19	30.1	30.8	30	25.1	23.7	1	10.3	9	1	1	15.3
20	29.6	33.3	24	23.9	21.6	29	0	0	31	0	14.3
21	28	29.9	18	22.7	20.4	23	0	0	30	0	14.3
22	26.1	27.8	6	20.8	18	20	0	0	31	0	16.1
23	24.5	26.2	21	19.7	15.7	26	0	0	31	0	17.2
24	23.1	25.6	21	18	15.8	13	6.3	4.4	5	1	23.9
25	26.4	31.1	15	21	18.7	3	0	0	31	0	18.3

1971

1	23.6	26	1	18.5	16	28	0	0	31	0	19.3
2	24.8	29.4	25	19.1	16.6	2	0	0	28	0	17.9
3	27.2	31.9	15	21.3	18.1	6	0	0	31	0	17.6
4	30.6	36.4	20	24.7	22.7	1	0	0	31	0	17.8
5	31.8	33	22	22.7	22.7	1	0	0	31	0	17.8
6	30.2	32	8	25.9	23.6	29	284.1	91.5	15	11	21.3
7	31	33	1	26.8	22.9	6	223.8	75.2	6	7	25.1
8	30.2	32	32	25.5	23.9	8	64.3	23.7	8	6	16.1
9	29.6	32	32	25.5	23.9	8	64.3	23.7	8	6	16.1
10	30.3	33.5	13	26.1	24.6	24	0	0	31	0	15.8
11	28.4	31.8	1	23	18.4	20	0	0	30	0	15.6
12	25.2	26.9	6	20	16.6	23	0	0	31	0	17.2
13	27.2	31.9	15	21.3	18.1	6	0	0	31	0	17.6
14	30.6	36.4	20	24.7	22.7	1	0	0	31	0	17.8
15	31.8	33	22	22.7	22.7	1	0	0	31	0	17.8
16	31.5	34.3	3	27.2	23.3	25	71.8	55	25	4	24.8
17	29.9	31.3	7	26	23.8	14	55	17.4	17	7	28.2
18	29.8	30.9	27	25.6	23.4	31	41.4	10.5	31	7	24.4
19	30.1	30.8	30	25.1	23.7	1	10.3	9	1	1	15.3
20	29.6	33.3	24	23.9	21.6	29	0	0	31	0	14.3
21	28	29.9	18	22.7	20.4	23	0	0	30	0	14.3
22	26.1	27.8	6	20.8	18	20	0	0	31	0	16.1
23	24.5	26.2	21	19.7	15.7	26	0	0	31	0	17.2
24	23.1	25.6	21	18	15.8	13	6.3	4.4	5	1	23.9
25	26.4	31.1	15	21	18.7	3	0	0	31	0	18.3

1974

1	23.8	25.6	6	18.8	15.5	28	0	0	31	0	15.9
2	24	28.2	19	18.5	14.6	9	0	0	28	0	20.3
3	27.8	31.8	27	22.7	20.7	2	0	0	31	0	18.1
4	29.9	31.4	16	22.7	20.7	2	0	0	30	0	21.9
5	31.7	34.9	21	25.2	23	6	0	0	30	0	23.4
6	31.8	33.6	1	27	25.6	19	0	0	31	0	23.5
7	31.8	32.9	11	28.1	27.1	30	0.6	0.3	10	0	26

1973

1	22.9	25.5	19	18.2	15.9	21	1.9	1.9	5	0	20.9
2	24.3	27.4	26	19.2	17.2	15	1.9	1.9	5	0	20.9
3	27.6	33.2	25	21.8	18.3	12	0	0	28	0	17.7
4	30.2	32.2	8	24.8	22.9	1	0	0	31	0	18.8
5	31.7	32.5	28	27.3	25.6	18	0	0	30	0	18.9
6	32.4	36.2	9	28.2	27.3	9	0	0	31	0	25.8
7	30.7	33.5	9	28.2	27.3	9	10.5	4.6	7	1	29.7
8	30.8	31	15	26.2	24.6	29	26.4	16.2	5	8	26.9
9	29.5	30.8	4	25.2	24.1	14	7.6	3.9	12	2	17.6
10	29.8	33.4	23	24.3	22.3	24	0	0	31	0	12.3
11	28.4	31.6	1	23.7	21.8	30	0	0	30	0	16.5
12	25.3	27.7	1	20.2	17.1	19	0	0	31	0	22.2

1976

1	24.4	26.1	30	19.6	16.5	19	6.5	6.2	30	1	17.1
2	25.4	27.3	22	20.5	18	18	0	0	29	0	17.1
3	27.4	31.1	16	22.6	20.3	18	0	0	31	0	19
4	29.3	30.9	24	24.5	21.4	1	0	0	31	0	19
5	31.5	37.5	25	26.8	24.9	1	0	0	30	0	23.3
6	32.6	33.8	30	28.2	27.3	2	0	0	31	0	27.6
7	31.7	34.4	4	27.3	27.3	19	155	110	23	4	27.6
8	29.7	31.4	26	23	19	0	0	0	26	0	22.5
9	30	30.9	29	25.4	23.7	1	0	0	30	0	16.9

1978

1	24.5	25.9	27	19	15.8	3	0	0	31	0	15.1
2	24.8	27.9	26	19.4	16.6	18	0	0	28	0	15.9
3	26.8	30	8	21.4	19.8	3	0	0	31	0	17.5
4	30	32.4	25	24.2	21.7	2	0	0	30	0	14.4
5	32.2	33.2	25	26.4	25	7	0	0	31	0	19.8
6	32.7	36.5	5	27.2	25.3	20	0	0	30	0	18.1
7	30.2	31.7	8	25.9	23.5	2	0	0	31	0	21.9
8	29.7	30.9	6	25.1	22.8	18	0	0	27	0	18.9
9	29.9	30.4	16	24.5	23.9	0	0	0	29	0	12.5
10	29.5	31.4	24	24.5	23.6	25	0	0	0	0	9.5
11	28.9	32.1	7	25	21.9	17	0	0	31	0	16
12	25.8	27.4	4	21.5	18.8	10	0	0	31	0	18.2

1977

1	24.1	27	24	18.8	15.6	28	0	0	31	0	17.9
2	24.8	27.4	26	20.1	17.1	6	0	0	28	0	13.5
3	29	32.7	21	22.8	20.5	4	0	0	31	0	14.4
4	30.6	32.7	26	25.3	24.1	5	0	0	30	0	19.3
5	32	33.2	30	27.1	25.6	2	0	0	31	0	23.8
6	32.7	35	13	28	26.9	30	0	0	29	0	22.6
7	30.8	32.8	25	26.7	24	8	0	0	31	0	23.6
8	30.1	31.1	30	25.8	23.8	10	0	0	30	0	20.1
9	29.6	31.1	3	24.8	21.8	3	0	0	30	0	16.6
10	30.4	31.9	21	25	23.1	25	0	0	30	0	10.7
11	30	33.1	12	24.6	22.2	19	0	0	30	0	14.2
12	27.1	29.2	1	21.7	18.5	30	0	0	31	0	14.6

1979	1	24.1	26.1	13	18.8	14.3	31	0	0	31	0	17.2
	2	23.8	26.8	19	18.8	17.1	15	0	0	28	0	17.2
	3	26.2	28.2	31	16.8	20.6	9	0	0	31	0	15.3
	4	29.5	32.8	29	23.6	21.7	11	0	0	30	0	15.6
1980	1	23.9	26.3	1	19.2	16.9	6	0	0	31	0	17.9
	2	25.2	28.3	29	20.3	16.4	5	4.9	4.9	3	1	14.3
	3	27.6	30.4	14	22.6	20.1	7	0	0	31	0	14.4
	4	30.8	33.1	21	25.3	23.4	10	0	0	30	0	13.5
	5	32.6	33.1	27	27.1	25.9	2	0	0	31	0	18.4
	6	32.9	35.7	4	27.8	24	23	432.2	190	30	8	17.8
	7	30.6	31.7	19	26.1	20.9	4	20.9	125.2	2	6	22.3
	8	30.6	33	20	25.8	24.4	29	5.9	4.5	26	1	16.5
	9	30.6	31.4	3	25.3	24	0	0	30	0	13.3	
	10	29.9	31.8	1	24.3	22.8	27	0	0	31	0	10.3
	11	28.5	30.7	6	23.4	21.5	29	0.2	0.2	18	0	13.4
	12	25.6	28.3	3	20.3	17.2	23	5.3	22	1	16.7	
1981	1	24.3	26.7	6	19.3	16.6	8	0	0	31	0	14.8
	2	25.6	28.2	28	19.8	16.4	5	0	0	28	0	13.9
	3	28	29.9	5	19.9	19.9	16	0.9	0.5	16	0	15.8
	4	30	31.7	21	22.7	22.7	6	0	0	30	0	16.9

9	31.3	32.4	24.8	23.3	23.8	29.1	29.1	27.3	30.4	31	31	31.3	17.1	16.6	12.2	13.9	13.3	13.8	13.8	13.3	1984
10	30.3	32.2	3	25.1	21.2	30	42	3.1	1.5	13	13	0	0	13.3	13.8	1	1	1	1	1984	
11	28	30.7	28.5	29	20.2	17.9	23p2181X0	0	0	30	0	0	0	13.5	13.5	12	12	11	11	1984	
12	25.4	28.5	28	26.7	25.1	20	0	0	0	0	0	0	0	15.1	15.1	16.6	16.6	16.6	16.6	1984	
1	23.3	24.8	5	17.9	13.3	20	0	0	0	31	0	0	0	15.1	15.1	16.6	16.6	16.6	16.6	1984	
2	23.8	29.1	29	17.9	15.3	21	0	0	0	29	0	0	0	17.1	17.1	18.9	18.9	18.9	18.9	1984	
3	27.3	30.4	31	21.3	15.3	21	0	0	0	29	0	0	0	16.6	16.6	18.2	18.2	18.2	18.2	1984	
4	31	34.3	24	24.9	4	4	0	0	0	31	0	0	0	12.2	12.2	13.9	13.9	13.9	13.9	1984	
5	32.3	33.3	24	24.9	23.3	4	0	0	0	30	0	0	0	12.2	12.2	13.9	13.9	13.9	13.9	1984	
6	32.9	35.9	18	26.8	26.8	3	0	0	0	31	0	0	0	18.9	18.9	20.1	20.1	20.1	20.1	1984	
7	30.7	32.6	1	26.1	22	25	29.1	12.6	19	19	1	1	1	21.4	21.4	23.5	23.5	23.5	23.5	1984	
8	28.8	29.9	2	24	22	14	67.1	50.2	14	14	2	2	2	15.6	15.6	17.3	17.3	17.3	17.3	1984	
9	28.8	31.5	7	24.7	22	14	90.8	87.5	5	5	1	1	1	15.6	15.6	17.3	17.3	17.3	17.3	1984	
10	29.2	29.2	6	24.7	22	14	67.1	50.2	14	14	2	2	2	15.6	15.6	17.3	17.3	17.3	17.3	1984	
11	28.2	31	1	22.9	21.9	16	0	0	0	31	0	0	0	9.3	9.3	11.0	11.0	11.0	11.0	1984	
12	25.9	28	1	20.7	17.6	24	0	0	0	30	0	0	0	13.5	13.5	15.2	15.2	15.2	15.2	1984	
1985	1	24	29.7	19	18.5	16.7	18	0	0	0	31	0	0	0	16.5	16.5	18.2	18.2	18.2	18.2	1985
2	25.3	27.3	27	19.9	17.9	18	0	0	0	31	0	0	0	15.5	15.5	17.2	17.2	17.2	17.2	1985	
3	28	29.5	29	22.6	20.8	18	0	0	0	28	0	0	0	14.7	14.7	16.4	16.4	16.4	16.4	1985	
4	30.1	31.6	29	22.6	20.8	18	0	0	0	31	0	0	0	15.5	15.5	17.2	17.2	17.2	17.2	1985	
5	32	35.3	29	24.5	22.3	16	0.1	0.1	0.1	21	0	0	0	15.5	15.5	17.2	17.2	17.2	17.2	1985	
6	32.4	33.3	14	27.9	25.6	3	0	0	0	29	0	0	0	17.7	17.7	18.7	18.7	18.7	18.7	1985	
7	30.4	32	9	26.1	24	2	8.7	6.8	1	1	1	1	1	17.7	17.7	18.7	18.7	18.7	18.7	1985	
8	29.6	30.7	9	26.1	24	25	49.8	9.9	19	19	0	0	0	15.9	15.9	17.6	17.6	17.6	17.6	1985	
9	30.2	30.9	30	25.2	23.6	19	136.3	79.3	2	2	5	5	5	15.9	15.9	17.6	17.6	17.6	17.6	1985	
10	29.5	32.1	5	25.1	22.2	13	32.4	21.4	21.4	20.2	12	2	2	14.5	14.5	16.2	16.2	16.2	16.2	1985	
11	28.7	31.5	5	24.5	21.5	10	21.4	18.7	7	7	2	2	2	13.9	13.9	15.6	15.6	15.6	15.6	1985	
12	25.7	28.8	2	20.3	17.5	13	0	0	0	30	0	0	0	13.9	13.9	15.6	15.6	15.6	15.6	1985	

1986	1	24.2	25.8	2	18.4	16.7	6	0	0	27	0	17
	2	25.4	31.4	15	19.2	17.4	12	0.5 ..	0.5	21	0	16
	3	27.3	30.4	27	21.9	19.6	17	2.1	2.1	22	0	16.1
	4	30.1	32	25	21.9	19.6	17	0	0	30	0	16
	5	32.3	34.6	20	26.8	24.4	22	0	0	31	0	18.9
	12	24.4	28.4	7	18.9	16	14	3.1	3.1	12	1	18.2

The following datas based on Surface data collected from I.M.D. Pune, for the period 1967 to 1985 for Okha port, which is tabulated in table form for particularly relative humidity and Visibility is as follows and its abbreviations are given below:

Year
 MN - Month,
 HR - Hour at G.M.T.
 RHNO - Relative humidity in terms of percentage with Number of Observations
 V1 - Number of days with visibility less than 1 K.M.

YEAR - 1967

MN	"HR"	"RHNO"	V1
1	3	50	0
1	12	54	0
2	3	86	1
2	12	76	0
3	3	85	0
3	12	78	0
4	3	83	0
4	12	77	0
5	3	84	0
5	12	79	0
6	3	84	0
6	12	79	0
7	3	89	0
7	12	84	0
8	3	85	0
8	12	79	0
9	3	83	0
9	12	77	0
10	3	82	0
10	12	77	0
11	3	77	1
11	12	72	0
12	3	64	0
12	12	61	0

YEAR - 1968

1	3	61
1	12	55
2	3	70
2	12	61
3	3	77
3	12	70
4	3	87

4	12	78
5	3	80
5	12	77
6	3	83
6	12	77
7	3	86
7	12	79
8	3	88
8	12	83
9	3	83
9	12	78
10	3	76
10	12	74
11	3	62
11	12	69
12	3	57
12	12	57

YEAR - 1969

1	3	6131	0
1	12	5931	0
2	3	7328	0
2	12	7028	0
3	3	8331	0
3	12	7731	0
4	3	8430	0
4	12	7830	0
5	3	8131	0
5	12	7731	0
6	3	8130	0
6	12	7830	0
7	3	8531	0
7	12	8231	0
8	3	9231	0
8	12	8931	0
9	3	8930	0
9	12	8630	0
10	3	8931	0
10	12	8931	0
11	3	7930	0
11	12	8430	0
12	3	7231	0
12	12	7131	0

YEAR - 1970

1	3	7331	0
1	12	7131	0

2	3	7028	0
2	12	7028	0
3	3	7831	0
3	12	7131	0
4	3	8430	0
4	12	7730	0
5	3	8131	0
5	12	7731	0
6	3	7930	0
6	12	7530	0
7	3	8231	0
7	12	7831	0
8	3	8531	0
8	12	8031	0
9	3	8430	0
9	12	7930	0
10	3	7831	0
10	12	7031	0
11	3	6630	0
11	12	6730	0
12	3	6131	0
12	12	5631	0

YEAR - 1971

1	3	6231	0
1	12	5831	0
2	3	7528	0
2	12	6727	0
3	3	7831	0
3	12	7031	0
4	3	8730	1
4	12	7730	0
5	3	8231	0
5	12	7931	0
6	3	8230	0
6	12	7830	0
7	3	8431	0
7	12	7931	0
8	3	8731	0
8	12	8230	0
9	3	8730	0
9	12	8130	0
10	3	8031	0
10	12	8031	0
11	3	7230	0
11	12	7330	0
12	3	6526	0
12	12	6126	0

YEAR - 1972

1	3	6831	0
1	12	6631	0
2	3	6329	0
2	12	5829	0
3	3	8631	0
3	12	8030	0
4	3	8630	0
4	12	7930	0
5	3	8231	0
5	12	7731	0
6	3	8130	0
6	12	7630	0
7	3	8331	0
7	12	7931	0
8	3	8431	0
8	12	7931	0
9	3	8730	0
9	12	8130	0
10	3	8631	1
10	12	8130	0
11	3	6730	0
11	12	6430	0
12	3	6531	0
12	12	5731	0

YEAR - 1973

1	3	6731	0
1	12	6031	0
2	3	7928	1
2	12	7828	1
3	3	7631	2
3	12	7231	2
4	3	8530	1
4	12	8130	0
5	3	8331	0
5	12	8331	0
6	3	8230	4
6	12	7830	6
7	3	8431	0
7	12	7931	0
8	3	8331	0
8	12	7931	0
9	3	8430	0
9	12	7830	0
10	3	8231	0

10	12	7431	0
11	3	6730	0
11	12	6630	0
12	3	5831	0
12	12	5630	0

YEAR - 1974

1	3	6531	0
1	12	6031	0
2	3	6328	0
2	12	5628	0
3	3	8431	0
3	12	7631	0
4	3	8230	0
4	12	7630	0
5	3	7731	0
5	12	7431	0
6	3	7829	0
6	12	7530	0
7	3	7931	0
7	12	7431	0
8	3	8230	0
8	12	7731	0
9	3	8430	0
9	12	7929	0
10	3	7631	0
10	12	7431	0
11	3	6730	0
11	12	6430	0
12	3	6931	0
12	12	6431	0

YEAR - 1975

1	3	6631	0
1	12	6431	0
2	3	6728	0
2	12	6628	0
3	3	7831	1
3	12	7231	0
4	3	8729	1
4	12	8030	0
5	3	8631	0
5	12	8431	0
6	3	8530	0
6	12	8130	0
7	3	8531	0
7	12	8131	0

5	3	7831	0
5	12	7630	0
6	3	8130	0
6	12	7830	0
7	3	8531	0
7	12	8131	0
8	3	8631	0
8	12	8131	0
9	3	8530	0
9	12	8230	0
10	3	8131	0
10	12	7931	0
11	3	6930	0
11	12	6629	0
12	3	6231	0
12	12	5331	0

YEAR - 1978

1	3	5531	0
1	12	5031	0
2	3	6628	0
2	12	6628	0
3	3	7531	0
3	12	6931	0
4	3	8730	0
4	12	7830	0
5	3	7931	0
5	12	7631	0
6	3	8129	0
6	12	7829	0
7	3	8631	0
7	12	8231	0
8	3	8831	0
8	12	8431	0
9	3	8230	0
9	12	7930	0
10	3	8131	0
10	12	7731	0
11	3	7530	0
11	12	7330	0
12	3	6131	0
12	12	5831	0

YEAR - 1979

1	3	6031	0
1	12	5831	0
2	3	7728	0

2	12	7028	0
3	3	8131	0
3	12	7531	0
4	3	8730	0
4	12	7830	0
5	3	8031	0
5	12	7431	0
6	3	8430	0
6	12	7930	0
7	3	8231	0
7	12	7831	0
8	3	8631	0
8	12	8131	0
9	3	8130	0
9	12	7830	0
10	3	7631	0
10	12	7231	0
11	3	6730	0
11	12	6930	0
12	3	6231	0
12	12	5931	0

YEAR - 1980

1	3	6231	0
1	12	5631	0
2	3	7729	0
2	12	6729	0
3	3	7531	0
3	12	6831	0
4	3	8730	0
4	12	7830	0
5	3	7831	0
5	12	7631	0
6	3	8030	0
6	12	7530	0
7	3	8331	0
7	12	8031	0
8	3	8531	0
8	12	8231	0
9	3	8830	0
9	12	8630	0
10	3	9031	0
10	12	8631	0
11	3	6329	0
11	12	6330	0
12	3	5631	0
12	12	5631	0

YEAR - 1981

1	3	6631	0
1	12	6031	0
2	3	7428	0
2	12	6828	0
3	3	7531	0
3	12	7231	0
4	3	8130	0
4	12	7730	0
5	3	7931	0
5	12	7731	0
6	3	8030	0
6	12	7729	0
7	3	8531	0
7	12	8331	0
8	3	8830	0
8	12	8331	0
9	3	8530	0
9	12	8030	0
10	3	8031	0
10	12	7831	0
11	3	6930	0
11	12	6230	0
12	3	6431	0
12	12	6131	0

YEAR - 1982

1	3	6329	0
1	12	6231	0
2	3	6927	0
2	12	6628	0
3	3	7531	0
3	12	6931	0
4	3	8130	0
4	12	7830	0
5	3	7931	0
5	12	7431	0
6	3	7430	0
6	12	7330	0
7	3	8431	0
7	12	8131	0
8	3	8331	0
8	12	7931	0
9	3	7930	0
9	12	7629	0
10	3	7830	0

10	12	7630	0
11	3	6630	0
11	12	6430	0
12	3	6431	0
12	12	6031	0

YEAR - 1983

1	3	6331	0
1	12	5931	0
2	3	6628	0
2	12	5728	0
3	3	7231	0
3	12	6731	0
4	3	7730	0
4	12	7430	0
5	3	8031	0
5	12	7631	0
6	3	8028	0
6	12	7729	0
7	3	8828	0
7	12	8431	0
8	3	8830	0
8	12	8530	0
9	3	8430	0
9	12	8128	0
10	3	7631	0
10	12	7231	0
11	3	6130	0
11	12	5730	0
12	3	5531	0
12	12	5531	0

YEAR - 1984

1	3	4	0
1	12	3	0
2	3	6527	0
2	12	6329	3
3	3	8531	0
3	12	7831	0
4	3	8228	0
4	12	7730	0
5	3	7631	0
5	12	7331	0
6	3	7529	0
6	12	7228	0
7	3	7930	0
7	12	7530	0

8	3	8729	0
8	12	8431	0
9	3	8529	0
9	12	8230	0
10	3	7731	1
10	12	7430	0
11	3	6930	0
11	12	7128	0
12	3	6630	0
12	12	6531	0

YEAR - 1985

1	3	6231	0
1	12	6331	0
2	3	7228	0
2	12	6928	0
3	3	8530	0
3	12	7731	0
4	3	7928	0
4	12	7229	0
5	3	7929	0
5	12	7631	0
6	3	7930	0
6	12	7629	0
7	3	8728	0
7	12	8527	0
8	3	9031	0
8	12	8631	0
9	3	8229	0
9	12	7830	0
10	3	8427	0
10	12	8231	0
11	3	6830	0
11	12	7129	0
12	3	5731	0
12	12	5630	0

YEAR - 1986

1	3	5630	0
1	12	6231	0
2	3	6628	0
2	12	6328	0
3	3	7930	0
3	12	7130	0
4	3	8429	0
4	12	7828	0
5	3	7826	0

5	12	7227	0
6	3	8129	0
6	12	7728	0
7	3	8131	0
7	12	7829	0
8	3	8830	0
8	12	8531	0
9	3	8529	0
9	12	8030	0
10	3	8731	0
10	12	8331	0
11	3	6929	0
11	12	7128	0
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12	12	5931	0

ANNEXURE II

DIAGRAMS SHOWING

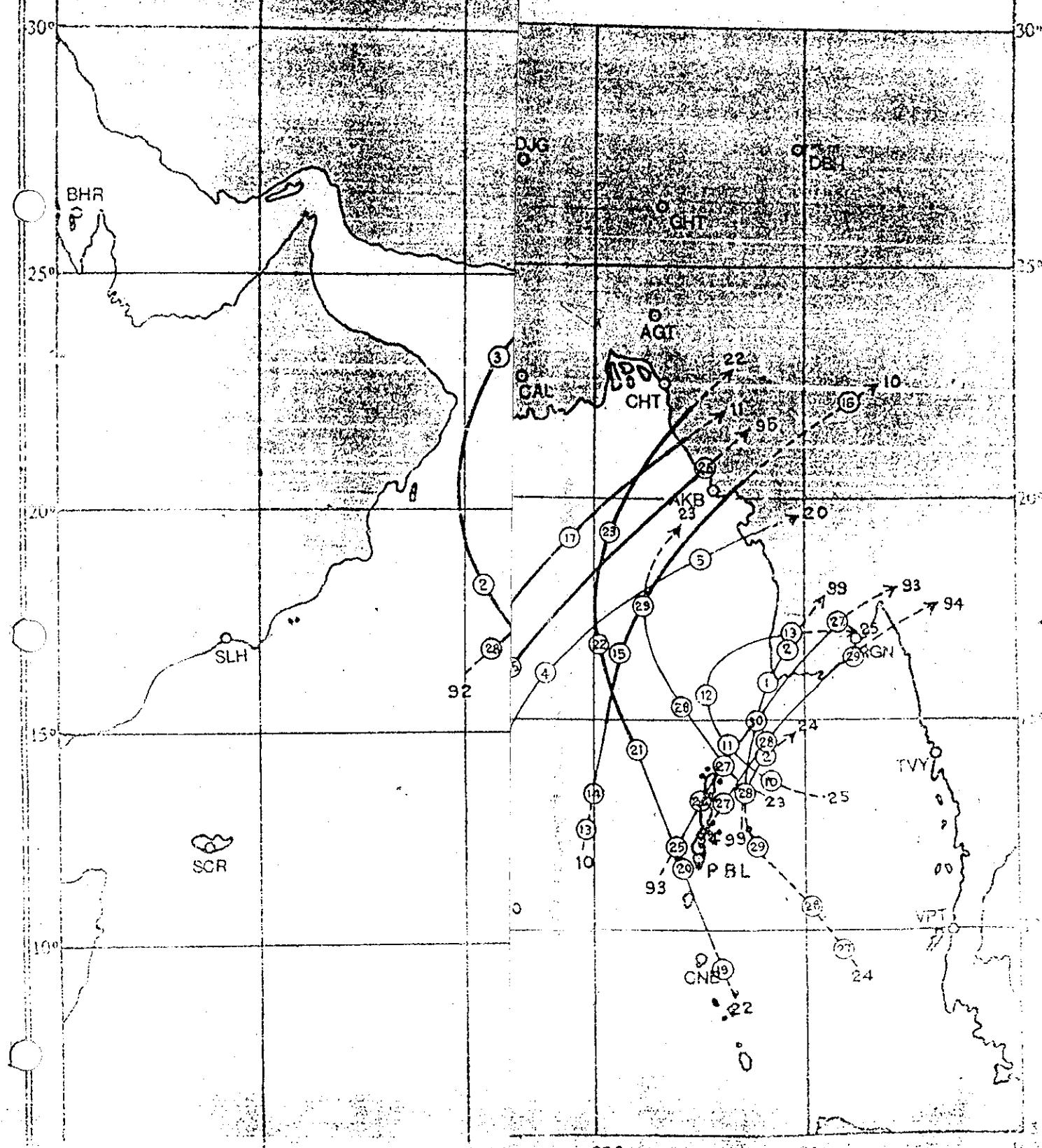
TRACKS OF STORMS / DEPRESSIONS

MAPS OF STORMS/DEPRESSIONS

MONTH APRIL

PERIOD 1891 - 1930

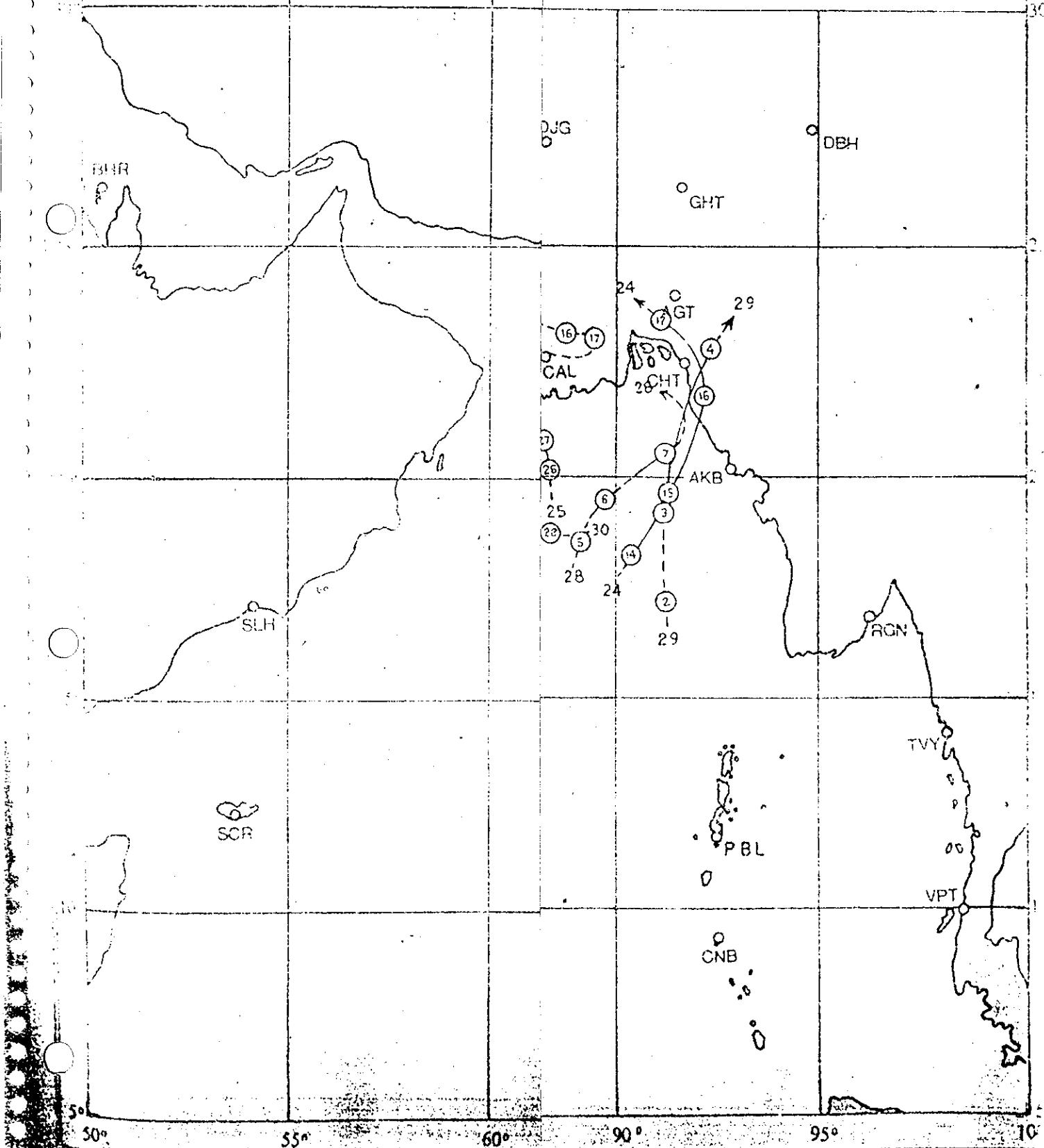
Depression — Storm, — Severe Storm

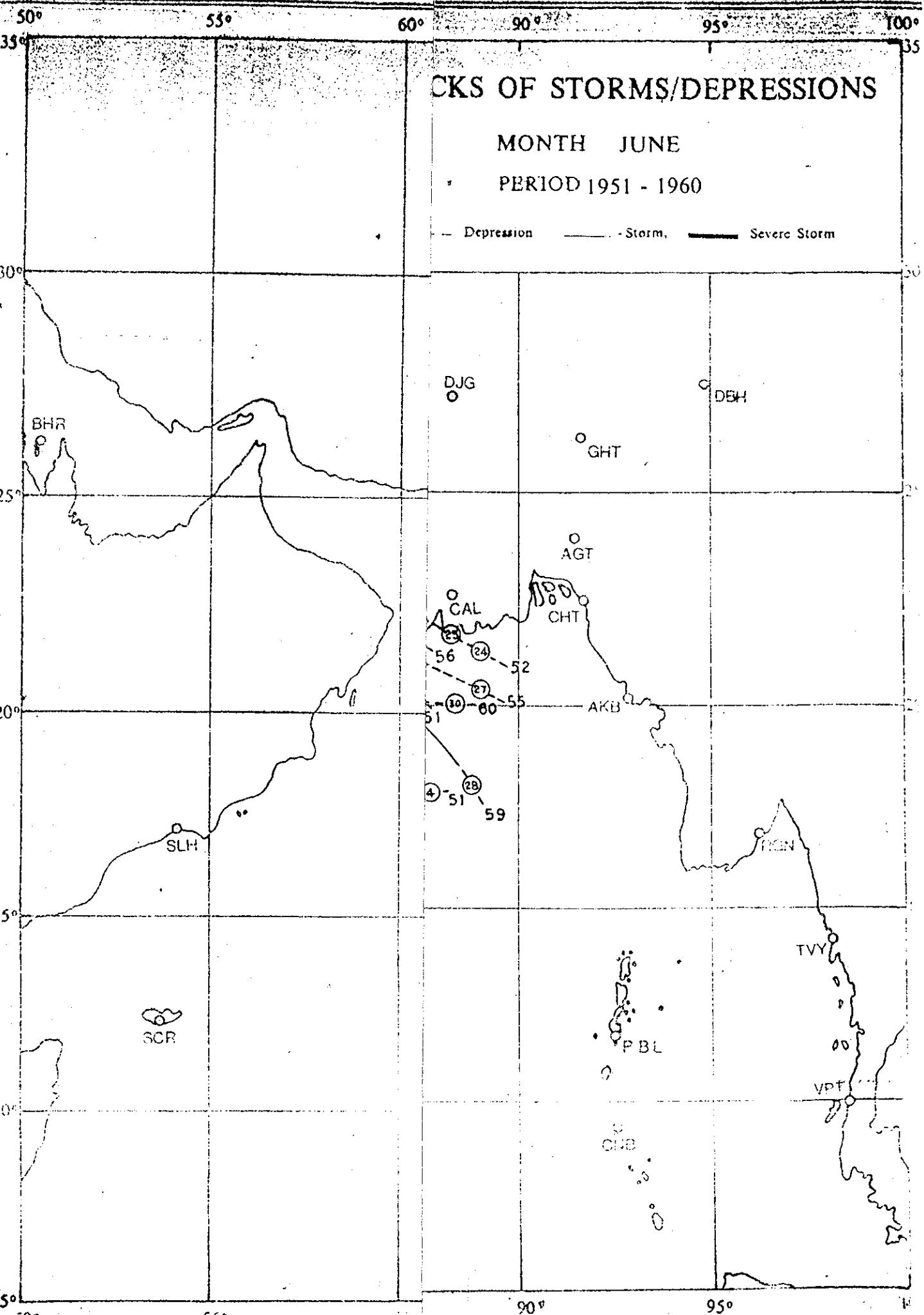


KS OF STORMS/DEPRESSIONS

MONTH JUNE

PERIOD 1921 - 1930





55° 60° 90° 95° 100°

CKS OF STORMS/DEPRESSIONS

MONTH JUNE

PERIOD 1961 - 1970

Depression ——— D. P. ——— D. T. ——— D. C.

30°

25°

20°

15°

10°

5°

DJG

DBH

GHT

29

63

68

8

14

18

7

20

8

66

12

69

15

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61

23

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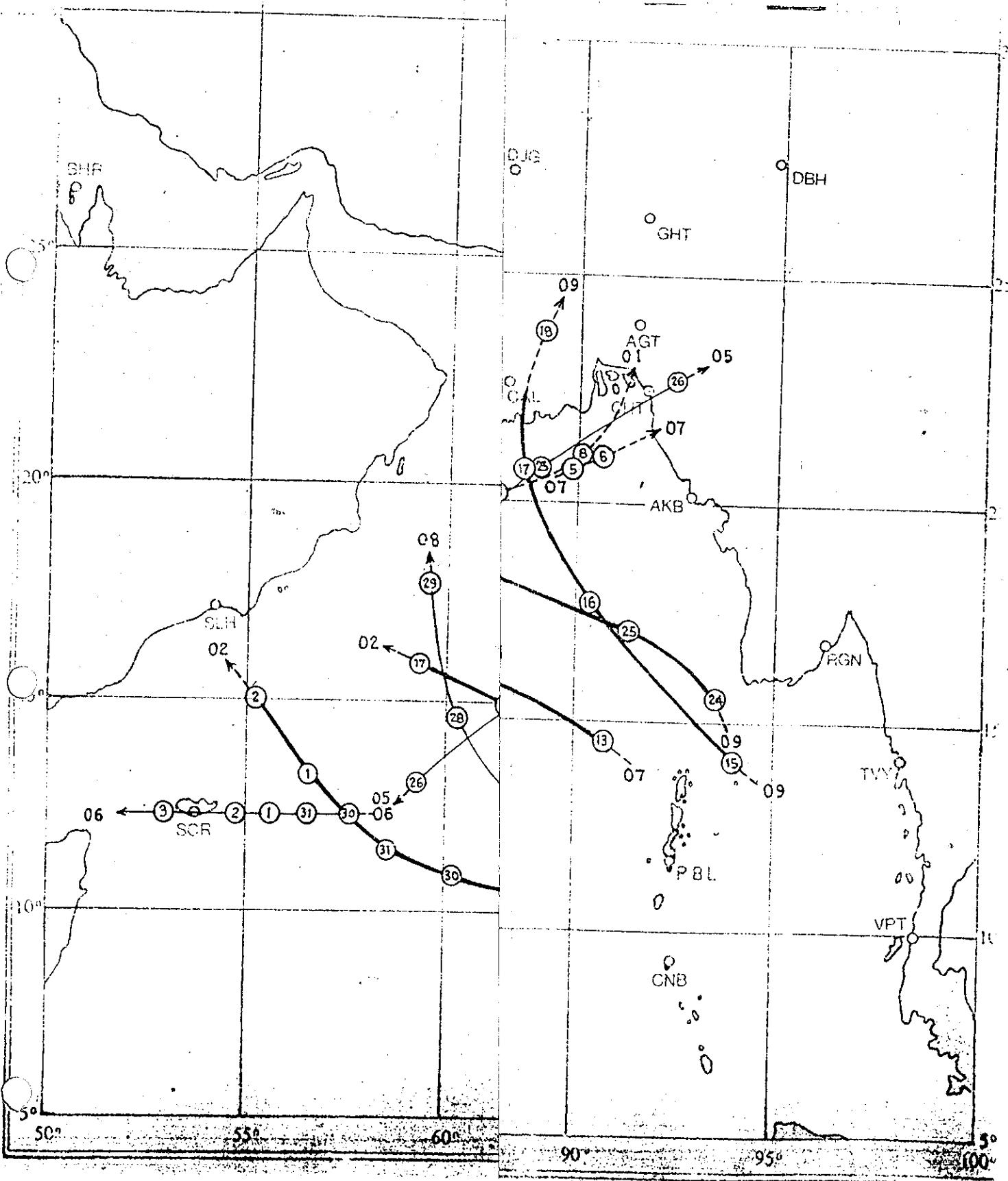
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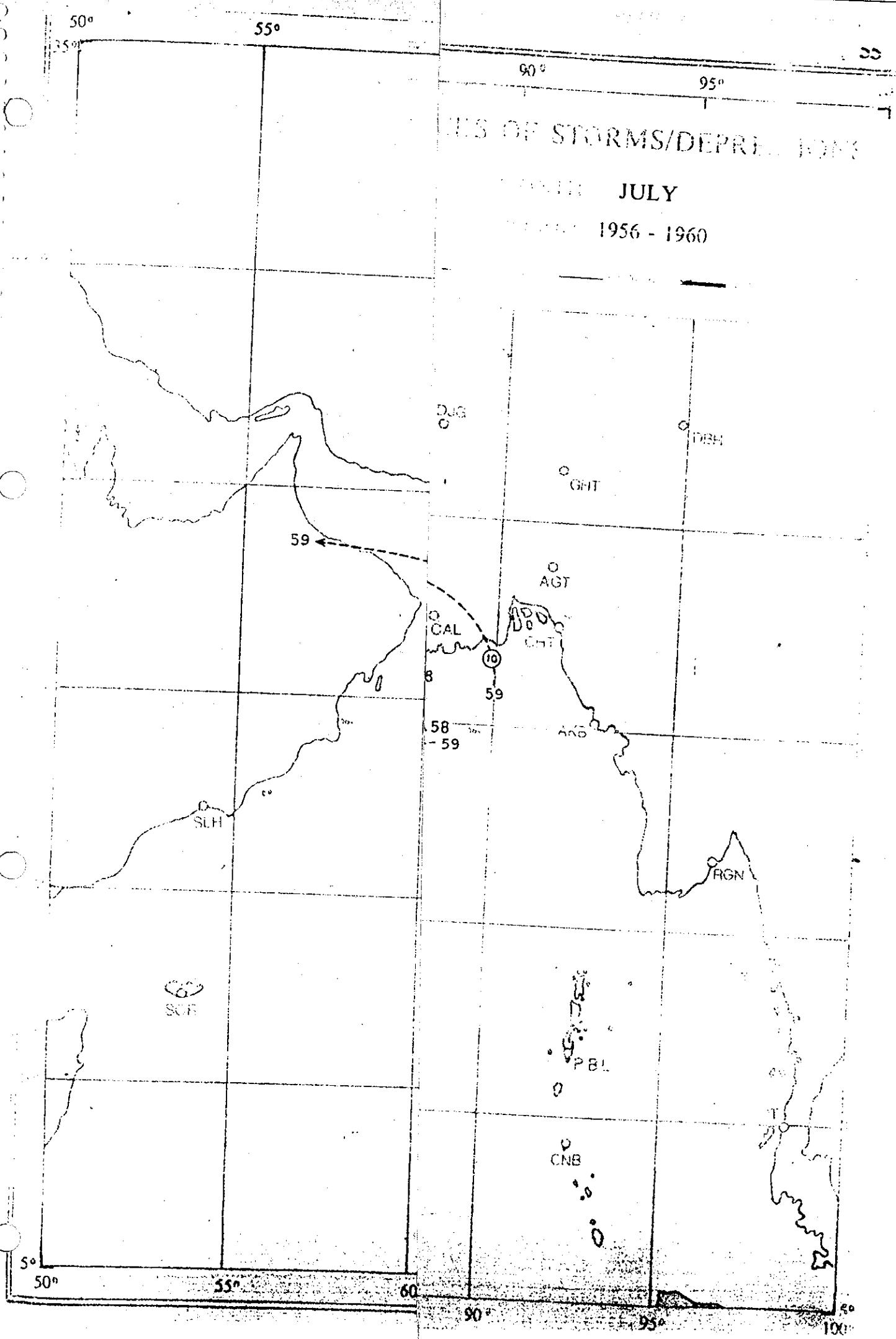
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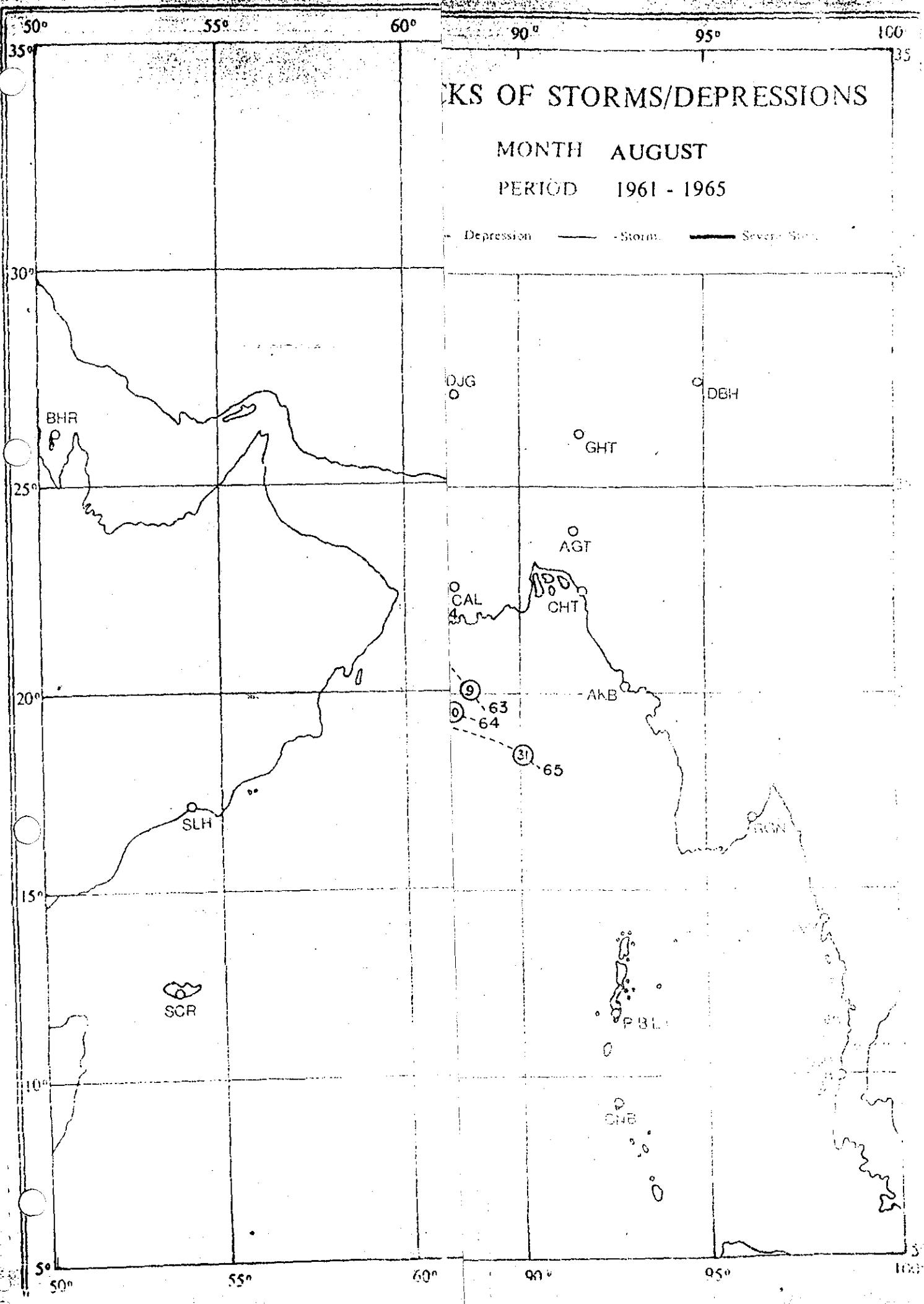
MAPS OF STORMS/DEPRESSIONS

MONTH: OCTOBER

PERIOD: 1901 - 1910



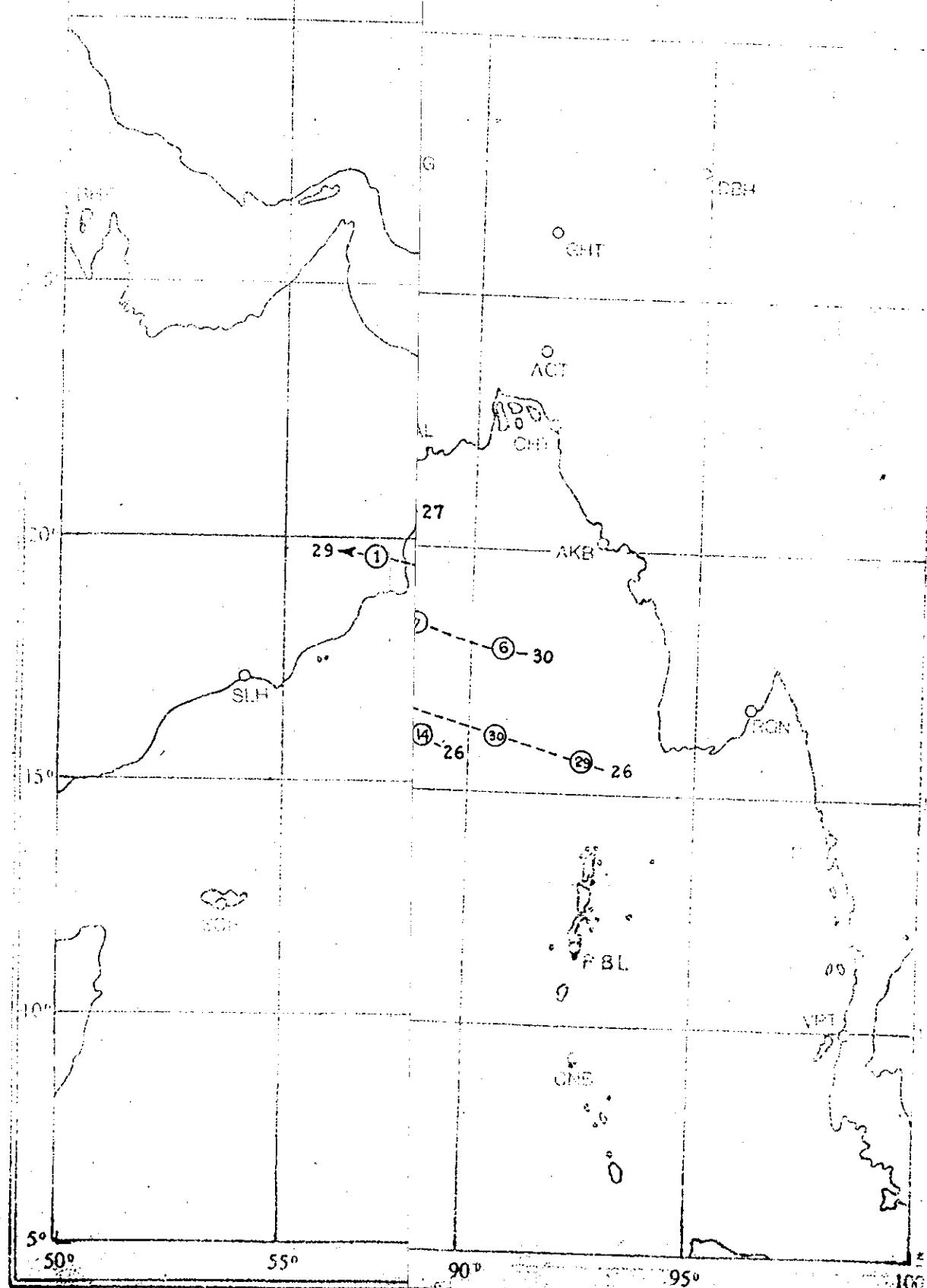




TS OF STORMS/DEPRESSIONS

VOLUME 11 SEPTEMBER

1926 - 1930

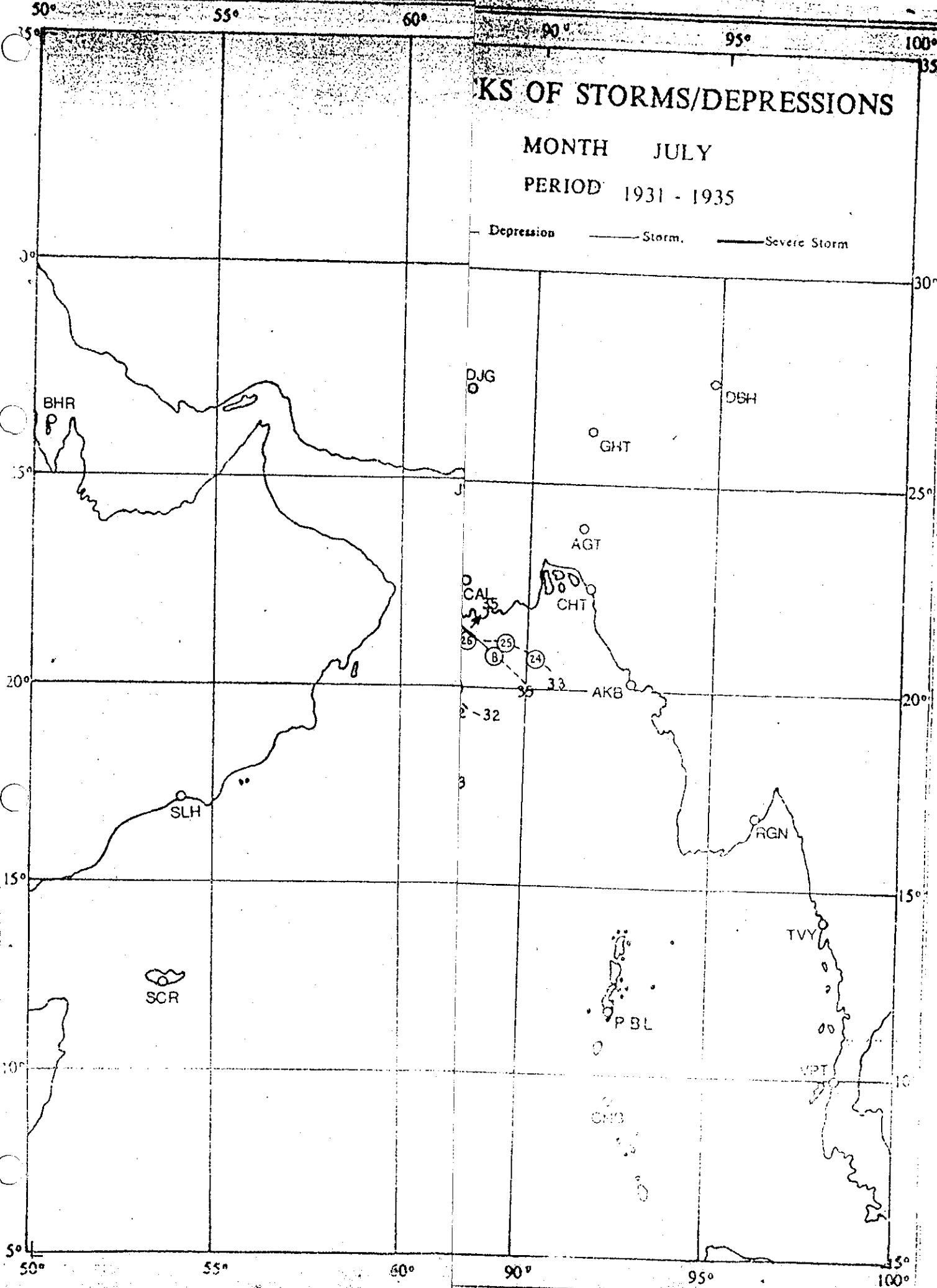


MAPS OF STORMS/DEPRESSIONS

MONTH JULY

PERIOD 1931 - 1935

Depression — Storm, — Severe Storm



50° 55° 60°

90° 95° 100°

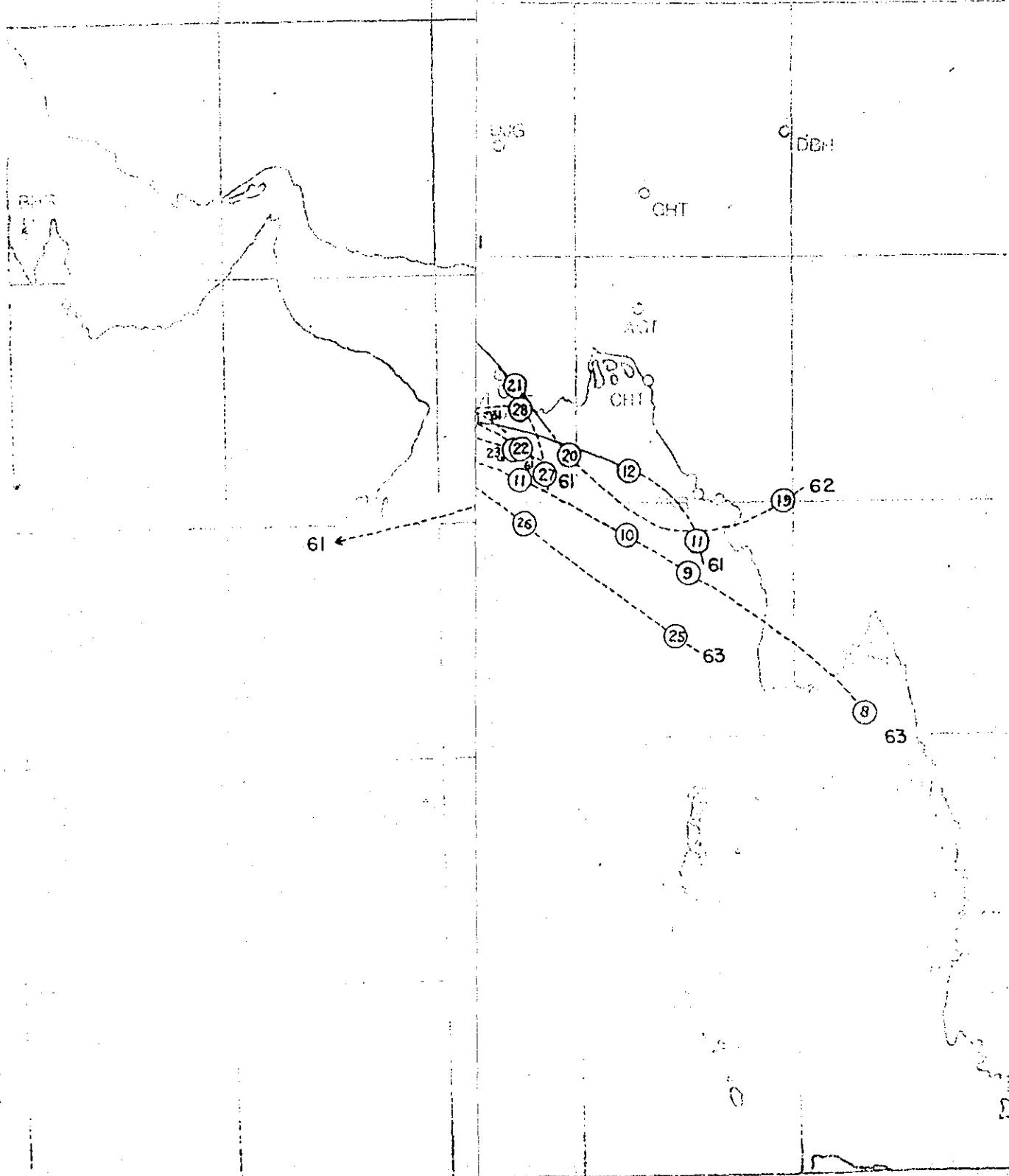
35°

BLOCKS OF STORMS/DEPRESSIONS

MONTH: SEPTEMBER

PERIOD: 1961 - 1965

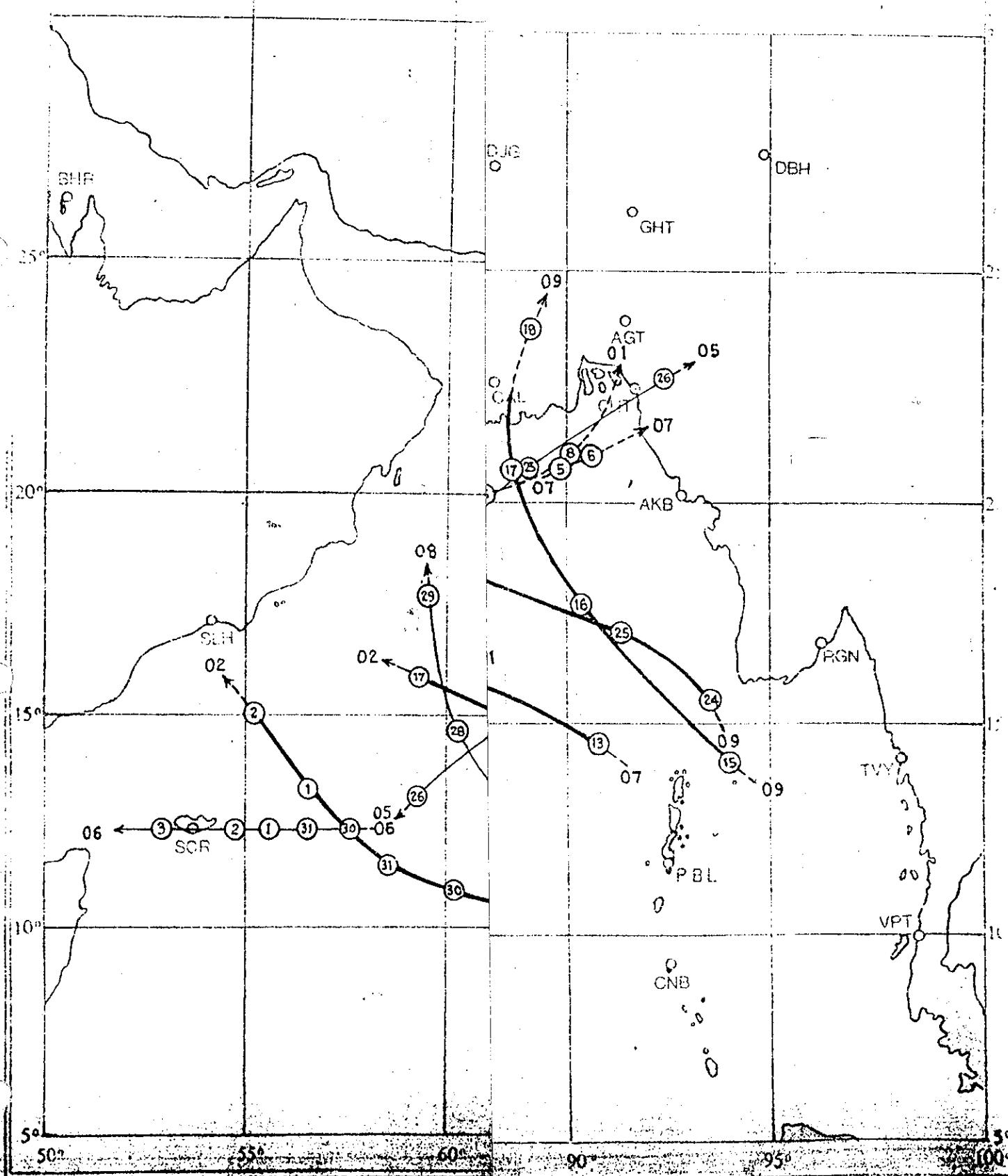
Dashed line = Depression — Solid line = System — Solid line with dots = Surface Weather

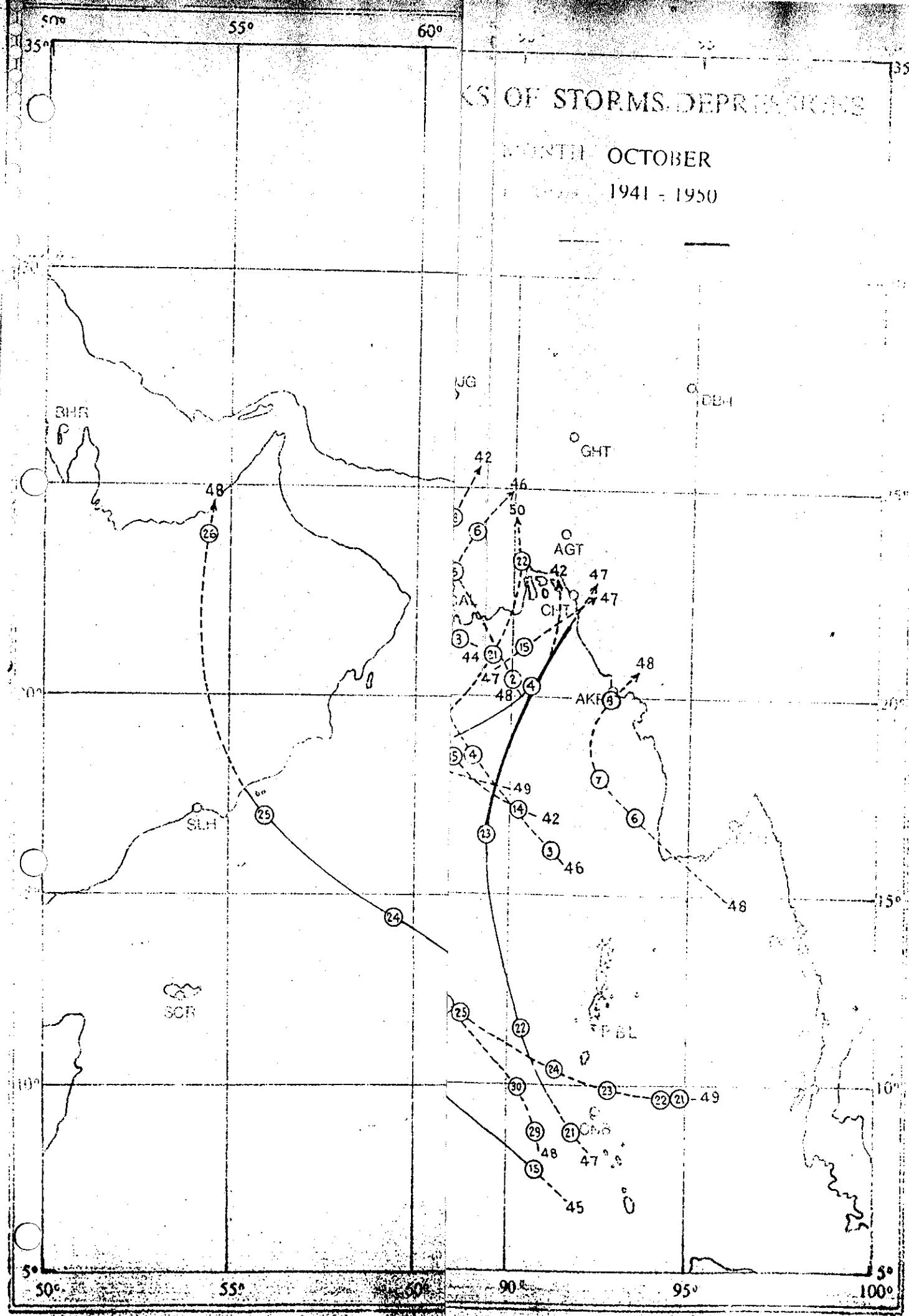


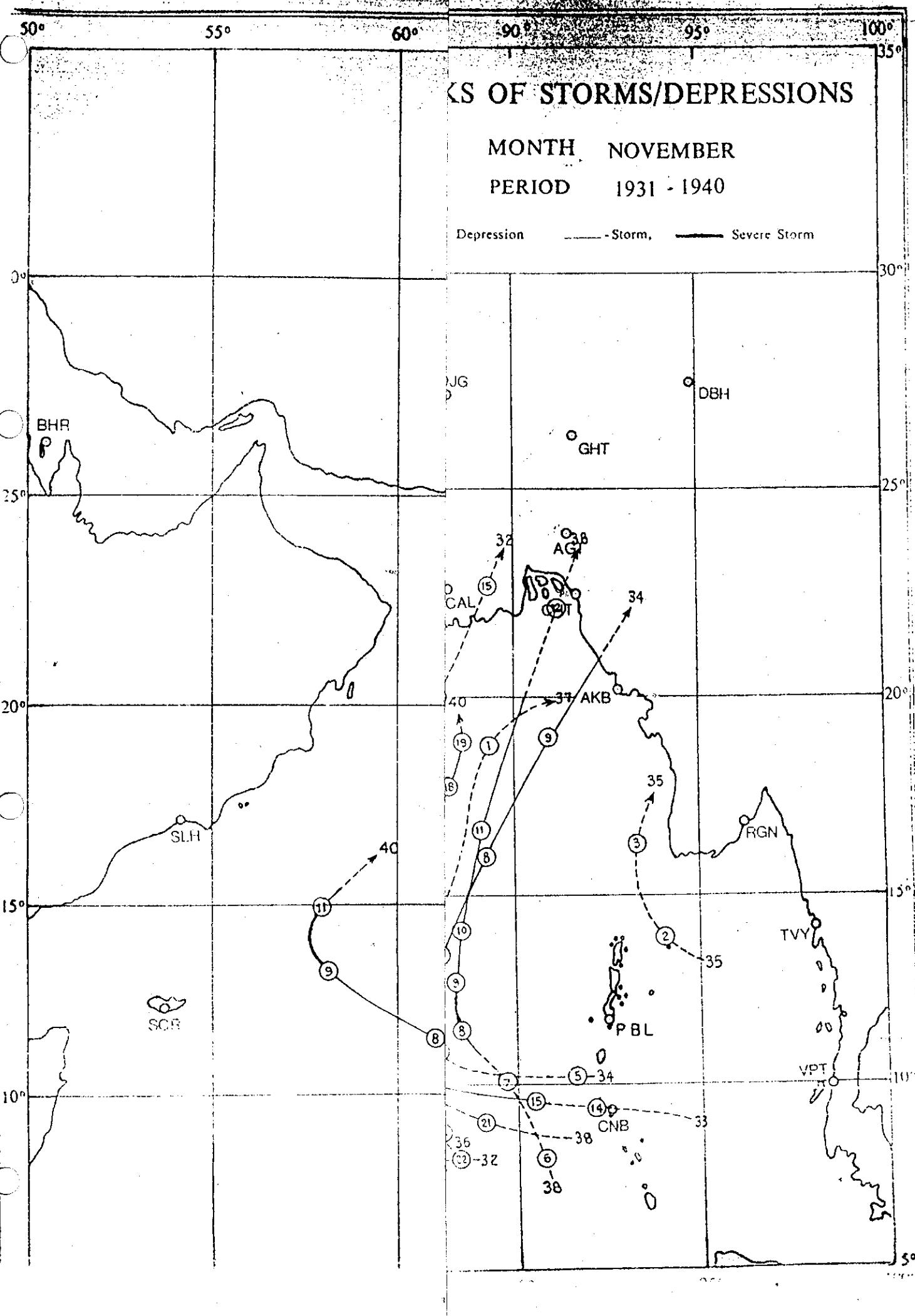
MAPS OF STORMS/DEPRESSIONS

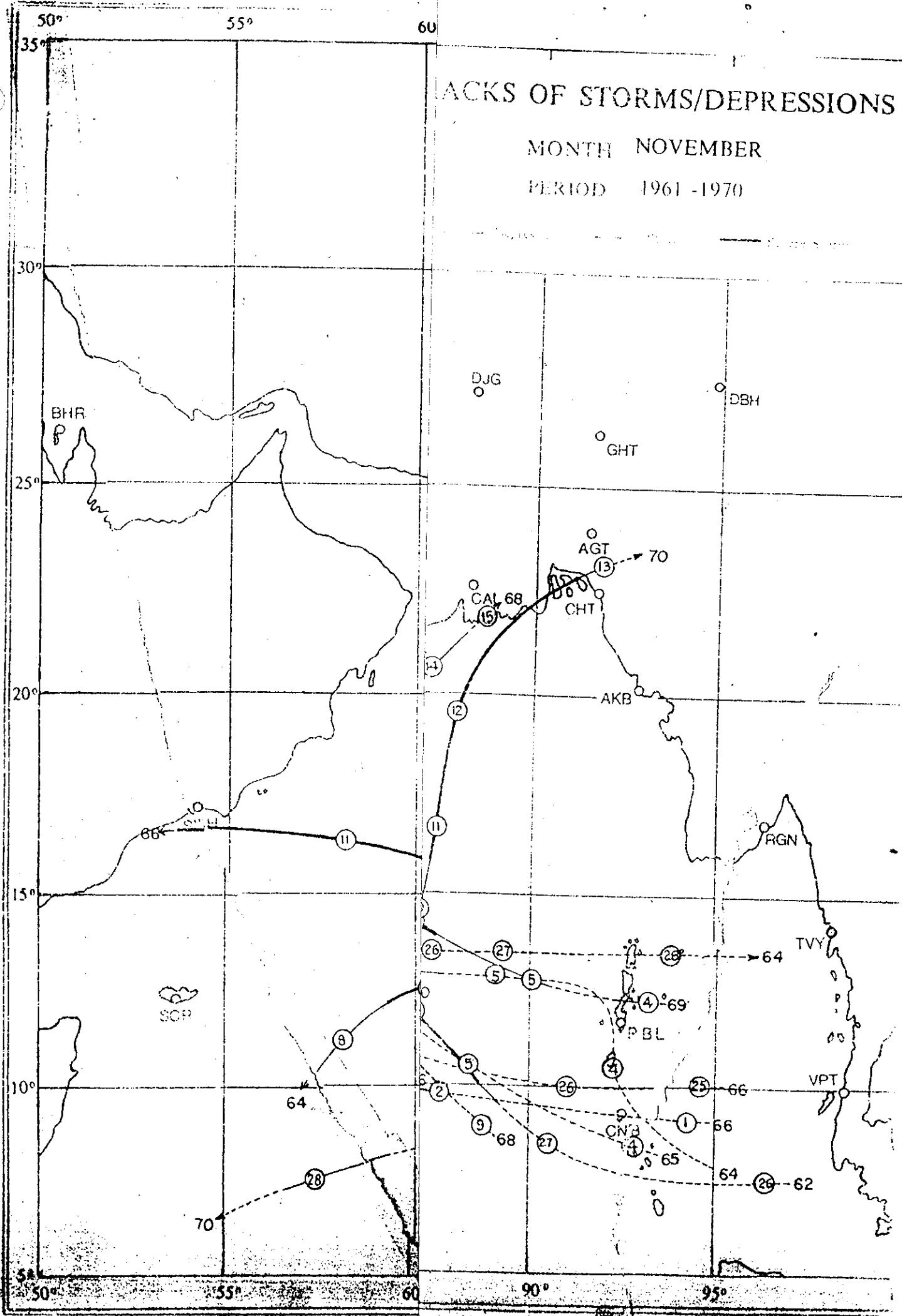
MONTH: OCTOBER

PERIOD: 1901 - 1910









APPENDIX C

**REPORT ON WIND, WAVE CHARACTERISTICS,
DESIGN WAVE AND NUMERICAL MODELLING
ON WAVE PENETRATION**

**BY
OCEAN ENGINEERING CENTRE,
I.I.T., MADRAS, CHENNAI.**

DEVELOPMENT OF PORTS IN GUJARAT

CONSULTANCY PROPOSAL FOR ENGINEERING PRE-FEASIBILITY/ DETAILED PROJECT REPORT

**Report on Wind Wave
Characteristics, Design Wave and Numerical
modeling on wave penetration**

CLIENT

FREDERIC R. HARRIS, Inc.

By

**Prof.V. SUNDAR
Dr. R. SUNDARAVADIVELU
Dr. R. NATARAJAN
Dr. S.R. GANDHI**



**OCEAN ENGG. CENTRE & CIVIL ENGG. DEPARTMENT
INDIAN INSTITUTE OF TECHNOLOGY
MADRAS - 600 036**

NOVEMBER 1996

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FIGURES

ANNEXURE A

1.0 INTRODUCTION

Gujarat Maritime Board has plans to develop various ports along the Gujarat coast as shown in Fig. 1(a). Gujarat Maritime Board has appointed Frederic R. Harris India Private Limited to prepare the detailed report for Positra Port. Frederic R. Harris Inc. have appointed IIT, Madras to perform certain tasks in connection with the development of master plan.

The port development at Positra is comprising of Positra I (location 1) and Positra II (location 2) and Positra III (location 3). Positra I is approximately located $22^{\circ}28'24''$ N and $69^{\circ}08'48''$ E. Positra II is located at $22^{\circ}25'15''$ N and $96^{\circ}11'24''$. The locations are as shown in Fig. 1(b). The bathymetry along with these locations are shown in Fig. 1(c).

The available data on the wind climate based on the meteorological data for the study area for the period 1967-1986 have been obtained, the salient results of which, have been brought out in our report submitted in August 96 to Frederic R. Harris Inc. New Delhi. A critical analysis of the above data have been made in order to pictorially represent the percentage of occurrence of wind speeds during the different months. A season wise analysis is also performed and the results are reported for the different seasons, namely, Non monsoon(Jan-May), S-W monsoon(June-Sep), N-E monsoon(Oct-Dec) and for the annual(Jan-Dec). The data compiled by Indian Meteorological Department reports the monthly wind speeds measured at 3.00 hrs and 12.00 hrs.

The wind speeds reported are the Mean Wind Speeds (MWS). The report also presents the information on the number of days within a month, the wind speed ≥ 62 kmph (W1), number of days in a month wind speed is 20-61 kmph (W2), number of days in a month wind speed is 1-19 kmph (W3) and number of days in a month calm condition prevails (W4). These data have been considered for a detailed analysis on the wind climate. The wave climate is also derived from the wind data assuming the duration of the wind is almost constant over a period of 3 hrs. The data measured by National Institute of Oceanography, Goa and the Wave Atlas prepared for the grid $15-25^{\circ}$ N and 70° E-coast have indicated that for the study area the wave period is within a small range from 5-6 seconds. The details of these analysis along with the percentage occurrence of the wave characteristics are also reported by Narasimha Rao and Sundar(1982), a

copy of which is given in Annexure A. Instead of assuming the fetch it was felt more reasonable to assume the wave period to vary from 5-6 secs, in order to forecast the wave heights. The forecasting diagram prepared by World Meteorological Organisation in 1988 has been utilised for obtaining the significant wave heights.

2. WIND SPEED

The wind speed(MWS, W1, W2, W3, W4) are stated earlier has been averaged for the duration of observation 1967-1986. Since the data available is for 20 years i.e. for a sufficiently long duration, the short term statistics derived from such data is expected to be quite reliable.

Accordingly, the averages obtained for 20 years have been derived.

The monthly variation of W1 measured at 3.00 hrs and at 12.00 hrs are reported in Fig. 2(a) and 2(b) respectively. The results suggest that the wind speed is mostly less than 62 kmph except for the months of June and August during which the number of occurrence is only one. The wind speed measured at 12.00 hrs indicate that the wind speed has been observed to be greater than 62kmph only once during the months of June, August, October and November.

The analysis of W2 measured at 3.00 hrs and 12.00 hrs shown in Fig. 3(a) and 3(b) indicate that the wind speed is between 20-61kmph, for about 400 to 500 days during the months May to August, i.e., the percentage of occurrence is approximately 5-6%.

The results on the variation of W3 measured at 3.00 hrs as shown in Fig. 4(a), show that during the month of May-August the no of days is less to the extent of 200-300. No regular trend in its variation is seen as observed for W3 taken at 12.00 hrs shown in Fig. 4(b), wherein, the number of days is seen to reduce till the month of May after which the trend shows an increase in the number of days.

The variation of W4, is presented for 3.00 hrs and 12.00 hrs in Fig. 5(a) and 5(b) Respectively. The trend in the variation for both the time of observation looks almost similar, except, for the months of February and December.

The variation of the average of monthly mean wind speed (MWS) measured at 3.00 hrs and 12.00 hrs are shown in Fig. 6(a) and 6(b) respectively. The results indicate that during the months May to July the MWS is approximately reaching to the extent of about 25kmph, which is observed to be the highest in a year. The results obtained for the observation taken for 3.00 hrs generally exhibits a slightly higher value compared to the observations made at 12.00 hrs.

3.0 WAVE HEIGHT

3.1 From wind data:

The monthly average wind speed obtained for the 20 yrs data and assuming that the wave period ranging from 5-6 sec, the significant wave height was derived based on the wave forecasting methodology proposed by World Meteorological Organisation(WMO) in 1988. The wave period has to be fixed since the fetch is not known. Similarly, the duration of the wind is assumed to be 3.00 hrs. The above assumptions are quite reasonable as stated earlier in this report. The significant wave height(H_s) defined as the average of the highest one - third of the wave heights is obtained and the monthly means for the wind speeds measured at 3.00 hrs shown in Fig. 7(a).and that for the measurements taken at 12.00 hrs as shown in Fig. 7(b).The trend in the variation of H_s is similar to the variation of mean wind speed as can be seen in the previous plots. The significant wave height is found to vary from 2-4 m. The maximum significant wave height is of the order of 4 m, occurring during the month May-July for the data measured at 12.00 hrs and occurring in the month of July for the data measured at 3.00 hrs.

In the absence of data, it is advantageous to make certain assumptions for the derivation of the wave statistics. Literature states that the maximum wave height is 1.6-2.0 times the significant wave height. In the present study a factor of 1.8 has been adopted for the calculation of maximum wave heights. The variation of the monthly mean of maximum wave heights computed from the wind data observed at 3.00 hrs and that for measured at 12.00 hrs is shown in Fig. 8(a) and 8(b) respectively. The plots indicate that the maximum varies from about 3.5-7.5 m. The mean maximum wave height is observed to be about 7.5m in the month of July. However, the wave heights observed for the data taken at 12.00 hrs indicate that the mean

monthly maximum wave height is maximum during the months May, June, July to the extent of 7.5m. The variation of the maximum wave heights as derived above and that reported by Narasimha Rao and Sundar (1982) is given in Table 1, which indicates that the maximum wave heights in all the three months May, June, July which is of the order of about 7.5m.

The mean monthly maximum wave heights has been considered for the extreme value analysis in order to obtain the design wave heights.

Table 1. Maximum wave heights for the study area

Months	Hmax from wind speed at 3.00 hrs	Hmax from wind speed at 12.00 hrs	Hmax from the report [Narasimha Rao and Sundar (1982)]
January	5.4	4.14	3.0
February	5.04	4.68	2.5
March	4.32	5.76	2.5
April	4.77	6.3	3.0
May	5.85	7.2	4.0
June	6.12	7.2	7.5
July	7.2	7.38	7.5
August	5.94	6.3	7.0
September	4.32	5.4	4.0
October	3.42	4.23	4.5
November	4.68	4.14	3.5
December	5.4	3.6	3.0

3.2 Short Term Statistics:

The percentage of occurrence of different class intervals of wave heights have been obtained. For the seasonwise variation please see Annexure A. Fig. 9(a).shows the percentage of occurrence of wave heights considering the data from the visually observed data compiled for

the year 1968-1973. It is seen that the wave height of about 1-1.5m is the most frequently occurring. It also reveals that nearly 60% of the time wave height is less than 1.5m. The percentage of occurrence of wave heights less than or equal to 3m is approximately 95%. The cumulative percentage of occurrence of wave height is as shown in Fig. 9(b). It is felt that the above figures may certainly be helpful in decision making for the operational conditions. It is to be stated that this plot is for the offshore location.

4.0 WAVE PERIOD:

The percentage of occurrence of wave period and cumulative percentage of occurrence is shown in Fig. 10(a) and 10(b). It is observed that the wave periods range 5-6 secs are the most frequently occurring one and this accounts for nearly 60% of the duration

5.0 DESIGN WAVE HEIGHT

For the calculation of design wave heights from the available maximum wave heights for the 20 year duration as shown in Table 2, Log Pearson Type III distribution method is used. In this method the statistical moments are computed by using logarithms of the wave heights instead of the natural numbers. Since, the wave heights cannot be negative and therefore cannot conform to the normal distribution, their logarithms are more nearly normally distributed than the wave heights expressed in natural numbers.

Table 2. Computed yearly maximum wave heights

Year	Maximum wave height Hmax(m)
1967	8.1
1968	8.1
1969	8.1
1970	7.38
1971	8.1
1972	8.1
1973	8.1
1974	8.1
1975	7.38
1976	8.1
1977	7.56
1978	7.38
1979	7.38
1980	6.66
1981	6.84
1982	6.12
1983	6.3
1984	6.66
1985	6.66
1986	6.12

As per the available and computed 20 years data of maximum wave heights, the design wave heights for three return periods 25 ,50 and 100 years are as shown in Table 3.

Table 3. Results of Log Pearson type III distribution method

Return period (years)	Log of Mean wave heights	Standard deviation	Coefficient of skewness	Skewness curve factor	Design wave height (m)
25	.86985	.0447	-.52697	1.556	8.6
50	.86985	.0447	-.52697	1.762	8.8
100	.86985	.0447	-.52697	1.935	9.0

From the Log Pearson type III distribution method the design wave height for a structure whose life time is 100 years is 9m.

6.0 WAVE CHARACTERISTICS REPORTED BY NIO, GOA.

The recent study on the wave characteristics carried out by NIO, Goa during the period December 1993 to January 1994, for the study area of Positra in the Gulf of Kachchh as indicated in the following. The significant wave height during the S-W monsoon (June-Sept) varies from 1.5m-3m, during N-E monsoon (Oct-Jan) and non-monsoon (Feb-May) from 0.5m-1.5m. The wave periods varies from 5-8 sec during S-W monsoon, and 5-6 sec during the rest of the year. The deep water waves predominantly approach from 230° - 240° with respect to north, during S-W monsoon, 350° - 30° during N-E monsoon and 300° during fair weather period. Salient features from NIO measurements are given in Table 4.

Table 4. Salient results from NIO measurements from Dec 93- Jan 94

Season	Wave height (m)	Period (sec)	Wave direction w.r.t North
S-W Monsoon (June-Sept)	1.5 to 3.0	5.0 to 8.0	230° to 240°
N-E Monsoon (Oct-Jan)	0.5 to 1.5	5.0 to 6.0	350° to 30°
Fair Weather (Feb-May)	0.5 to 1.5	5.0 to 6.0	300°

Considering Table 4. and Table 2(of Annexure A), the input wave characteristics for running the numerical model have been arrived as shown in Table 5.

Table 5. Wave characteristics for numerical model

Monsoon	Wave Height(m)	Wave Period(s)	Wave Direction with respect to North	Number of Plots
SouthWest	7.5	7	240°	1
NorthEast	4.5	5	67.5°	1
		5	30°	1
Non-monsoon	4	6	300°	1

7.0 NUMERICAL MODEL

The objective of the study is to investigate, the wave climate modifications in and around Positra, Boria reef, Paga Reef and in the approaches to the above locations. Accordingly, the hydrographic chart No. 203, for the Gulf of Kachchh region was considered for numerical

modelling. The stretch $69^{\circ} 5' E$ to $69^{\circ} 30' E$ and $22^{\circ} 15' N$ to $22^{\circ} 32' N$ was blown up to arrive at the depth contours. The study area consists of the stretch running around 45kms east to west extending from about Gururshoal on the west to Chank Tapu in the east and about 32kms running north-south, from Gurur shoal in the north to Lalpur in the south. The total area considered for numerical modelling is 1440km^2 . The entire area was discretized in fine intervals of 385.2m. For each grid of size $385.2\text{m} \times 385.2\text{m}$ the depths were obtained from the hydrographic charts on the four corners. The basic input for running the above numerical model are the co-ordinates of the corners of the grid, and the water depths in metres in each of the grid. The other input data includes the wave period, the wave height and the wave direction. Computations were done for south - west monsoon, north - east monsoon and for non-monsoon seasons. The numerical model predicts the wave heights corresponding to the co-ordinates taken.

The numerical model uses mild slope equation and finite difference method is used for the computations. The program includes combined diffraction and refraction. In order to include wave transformation within the surf zone energy dissipation term by Dally et. al (1984) is also incorporated. The numerical model was verified with Berkhoff et. al (1982)wave tank experimental results which consists of an elliptical shoal superimposed on a plane beach. The numerical model has been earlier applied for the prediction of the wave heights near the Pipavav port in Gujarat. This model has been applied for the development of a port in Tamilnadu. The salient results obtained for the present study area are herein reported.

The wave height distribution in and around the jetty locations for the south west monsoon is shown in Fig. 11(a). The results indicate that the wave heights near all the three proposed jetty locations is mostly to the extent of about 0.60m for a deep water wave height of 7.5m.

The results on the wave height distribution for the north east monsoon are shown in Figures 11(b) and 11(c) respectively. In the former plot, location 1 experiences waves of height upto a maximum of 2.0m whereas, at location 2 the wave height is about 0.5m and at location 3 the waves are occasionally to a height of about 1.0m. In the latter plot, both the locations 2 and

3 are observed to be calm with waves of height upto about 0.5m while, location 1 experiences occasional higher waves of height upto about 2.0m .

The plot for the wave height distribution during non monsoon is shown in Fig. 11(D). The results indicate that all the three locations experiences mostly waves of height about 0.4m. However, at location 3, the waves are occasionally to the extent of about 1.0m. Based on the present study the order of priority with relevance to the tranquility point of view would be location 3, location 2 and location 1.

8.0 REFERENCES

1. Berkhoff, J. C . W. , Booy, N. , and Radder A. C . 1982. "Verification of Numerical Wave propagation models for simple harmonic linear water waves " , Coastal Engineering , Vol. 6 , pp 225 - 279.
2. Dally , W. R., Dean, R. G., and Dalrymple, R. A. 1984. " Modelling Wave transformation in the surf zone. " , Miscellaneous paper CERC - 84 - 8, US Army Engineer Waterways Experiment Station, Vicksburg, Miss.
3. T. V . S . Narasimha Rao and V . Sundar . , 1982." Estimation of Wave Power potential along the Indian Coastal line" , Proc. Energy, Vol. y, No. 10, pp. 839 - 845.

9.0 SUMMARY

A detailed analysis of the variation of wind speeds reveals that during the months May-August the wind speeds are relatively higher compared to the other months. The mean monthly wind speeds during the months May-August is about 25kmph.

The monthly mean significant wave height varies from 2-4m and is observed to be maximum during the months of May-July to the extent of about 4m.

The monthly mean maximum wave height is of the order of 7.5m during the 3 months May, June and July.

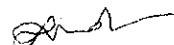
From the visually observed data compiled for the year 1968-1973, it is seen that the most frequently occurring wave height is about 1-1.5m and the most frequently occurring wave period range 5-6 secs.

The design wave height for a structure whose life time is 100 years is obtained as 9m using the Log Pearson type III distribution method.

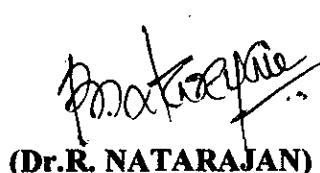
Though all the three locations are ideal for port development, based on the wave penetration tests, the order of priority in finalising the jetty locations for port development considering the tranquility conditions will be location 3, location 2 and finally location 1.



(Prof.V. SUNDAR)



(Dr.R. SUNDARAVADIVELU)


~~Dr. R. Natarajan~~

(Dr.R. NATARAJAN)


~~Dr. S.R. Gandhi~~

(Dr.S.R. GANDHI)

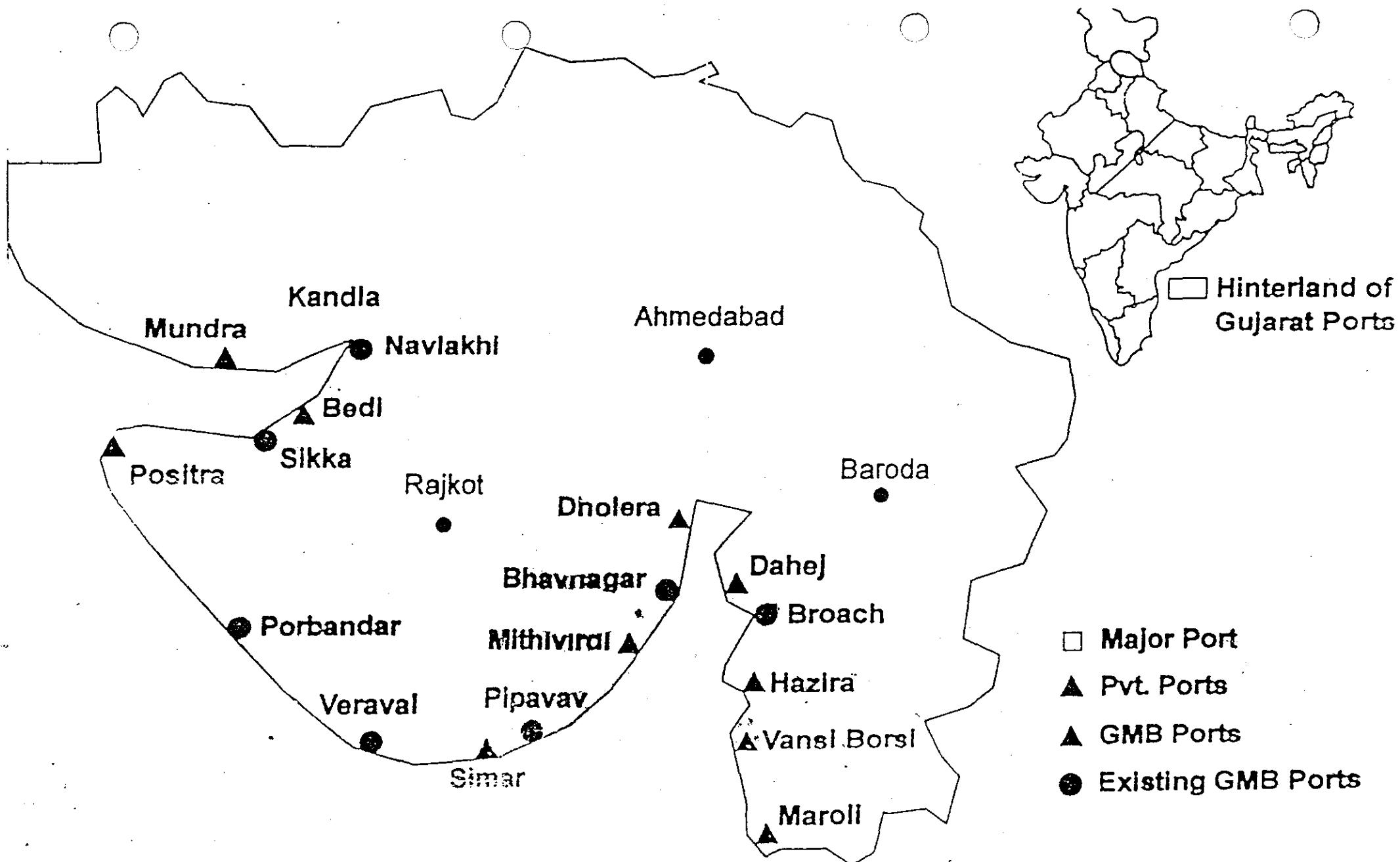
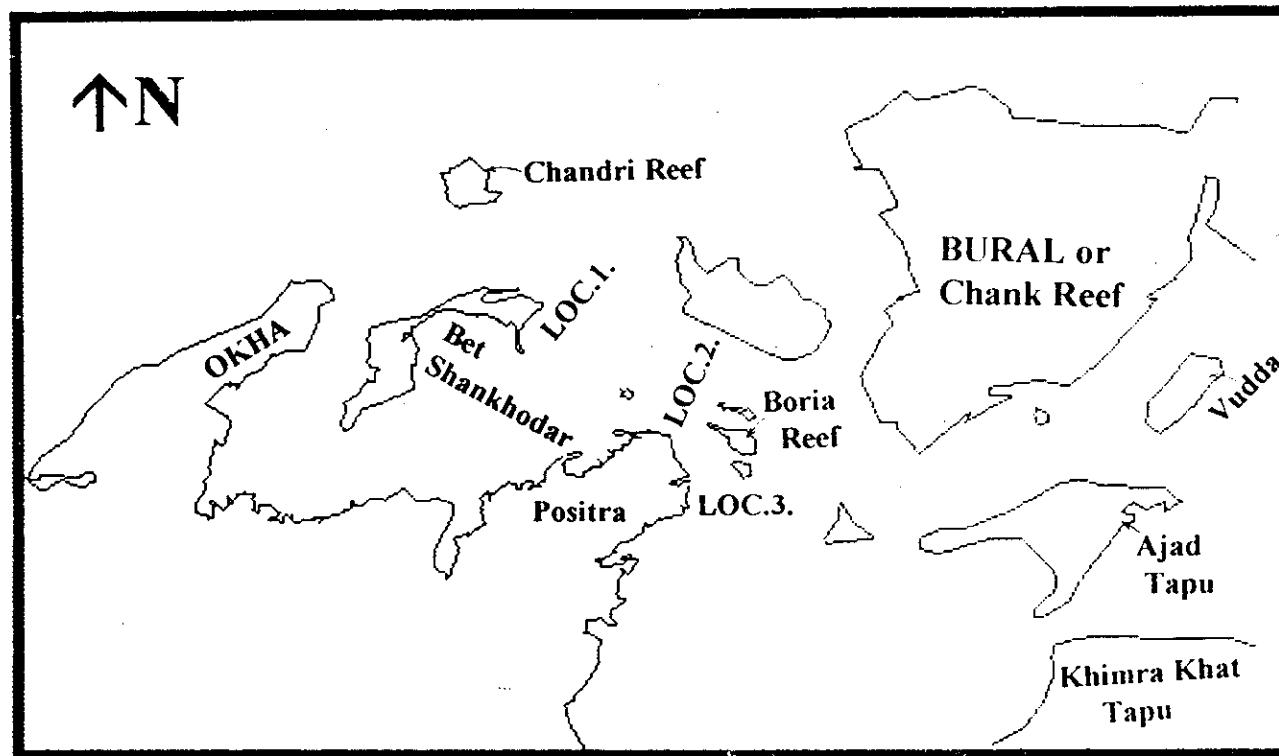


FIG. 1 (a). LOCATION OF PORTS ALONG GUJARAT COAST



LOC → LOCATION

FIG. 1 (b) . LOCATION OF POSITRA

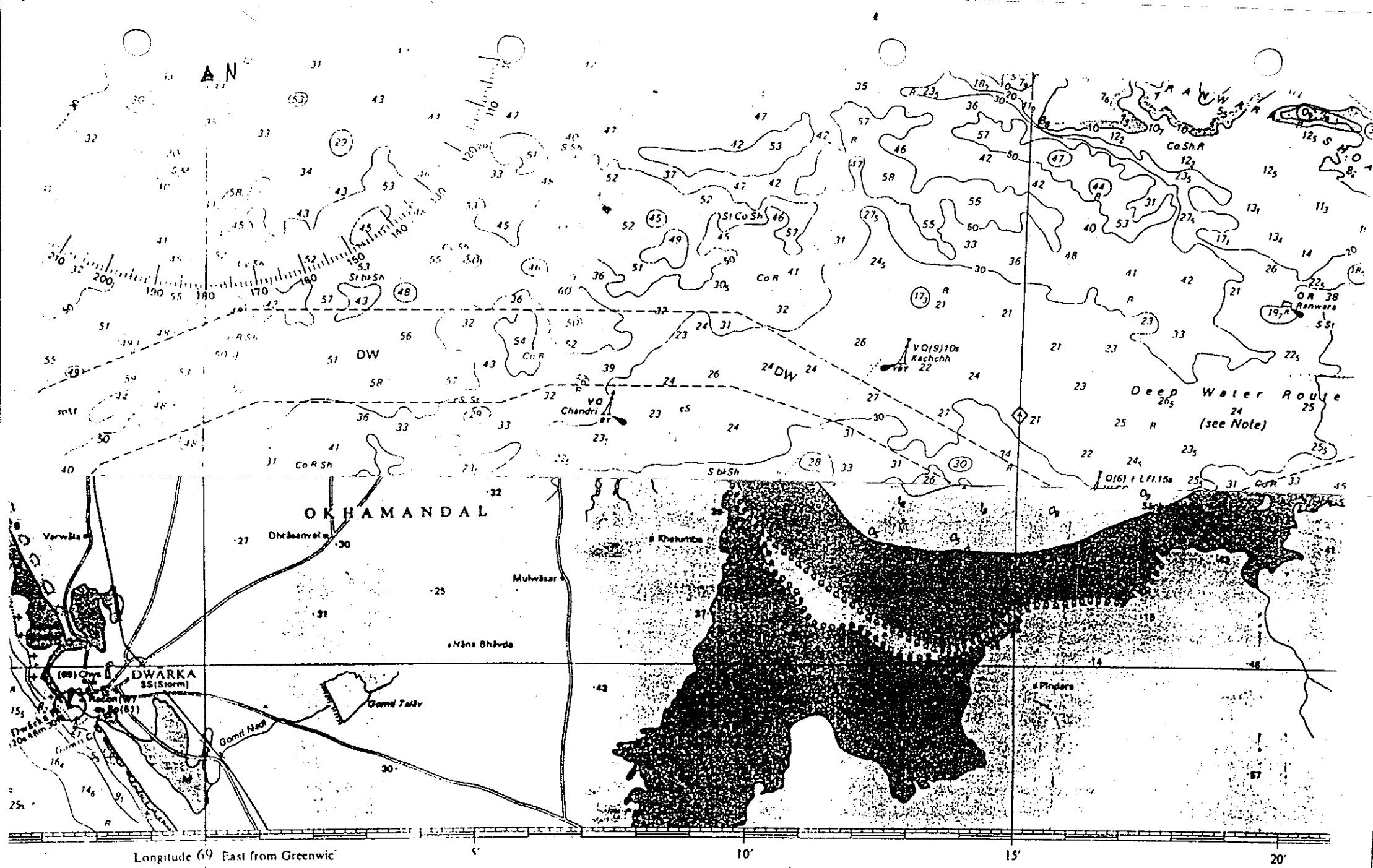


FIG. 1 (c). HYDROGRAPHIC CHART SHOWING LOCATIONS OF
POSITRA

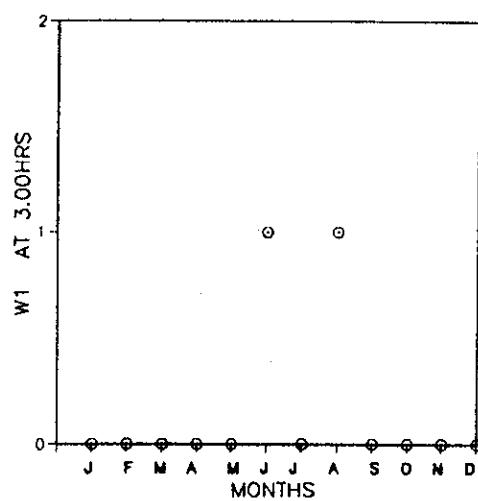


FIG.2(a). W1(number of days for which wind speed=62 kmph and above)
based on 20 years data

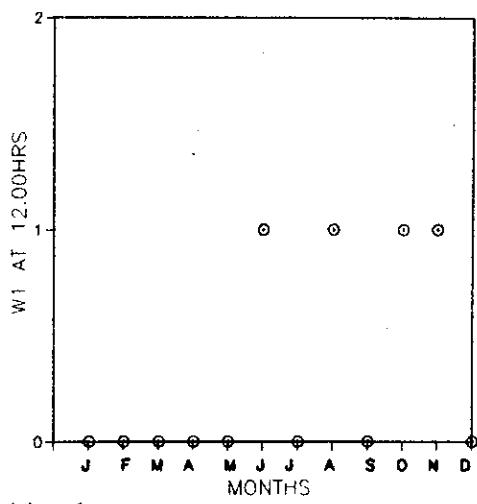


Fig.2(b).W1(number of days for which wind speed=62 kmph and above)
based on 20 years data

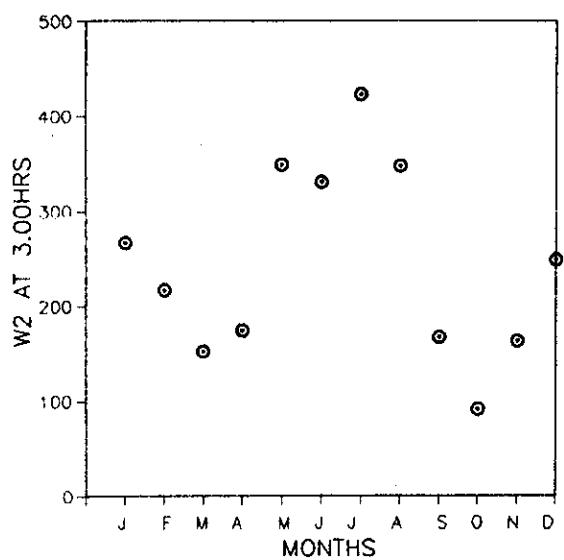


Fig.3(a).W2(number of days for which wind speed=20-61 kmph)
based on 20 years data

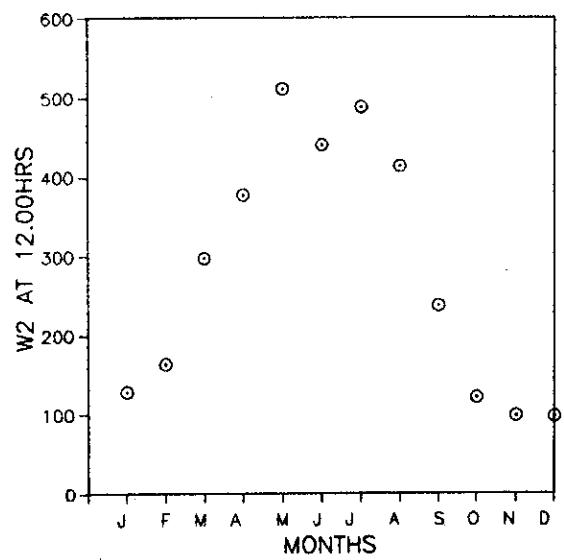


Fig.3(b).W2(number of days for which wind speed=20-61 kmph)
based on 20 years data

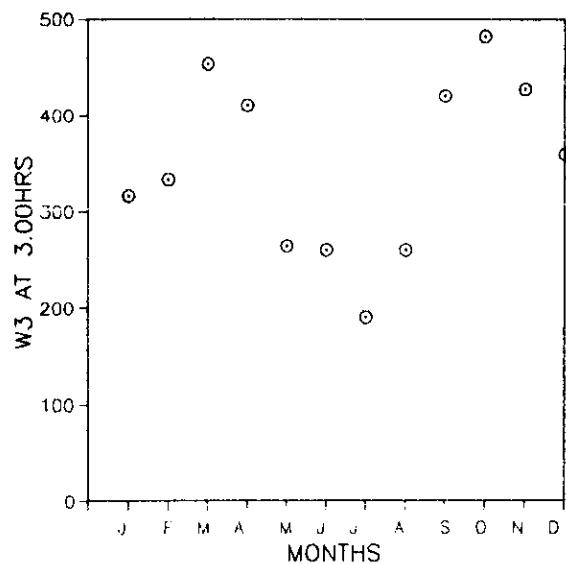


Fig.4(a).W3(number of days for which wind speed=1-19 kmph)
based on 20 years data

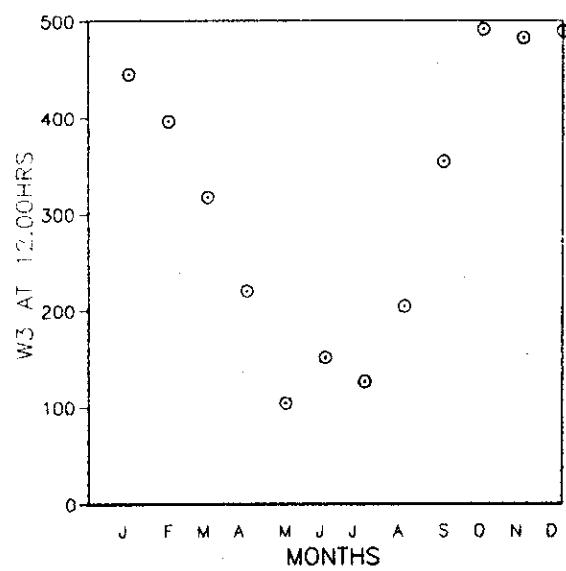


Fig.4(b).W3(number of days for which wind speed=1-19 kmph)
based on 20 years data

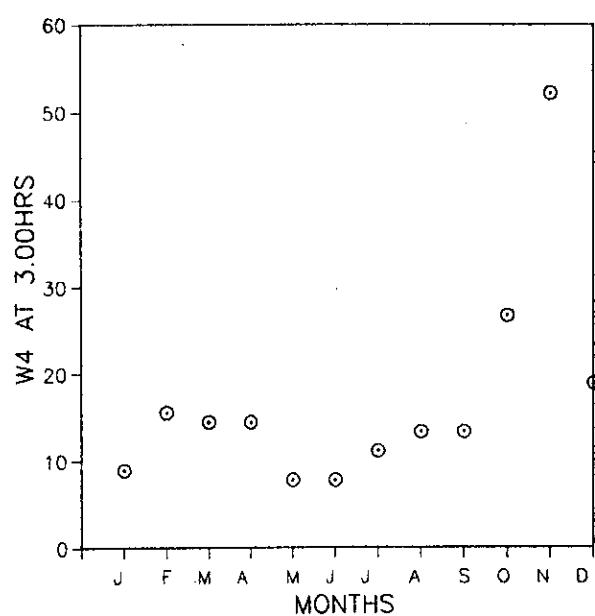


Fig.5(a).W4(number of days when calm condition prevails)
based on 20 years data

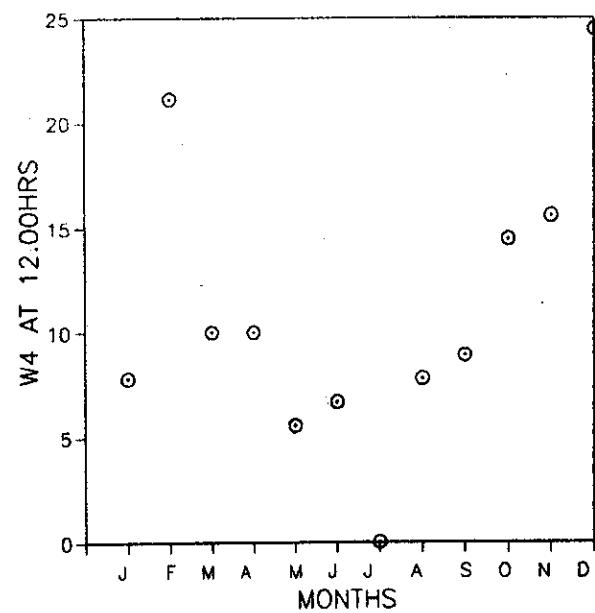


Fig.5(b).W4(number of days when calm condition prevails)
based on 20 years data

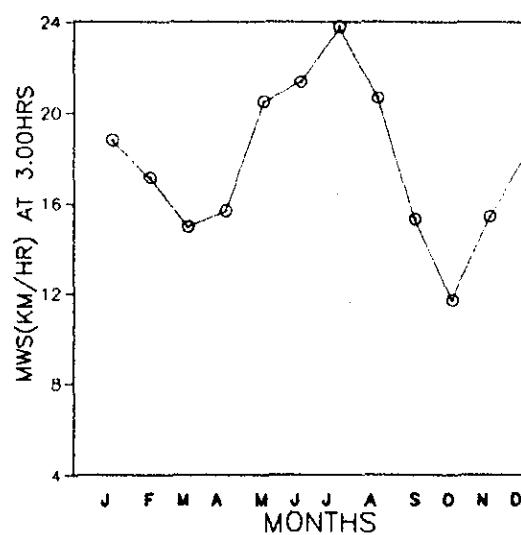


Fig.6(a).Average of monthly mean(based on 20 years data) of MWS

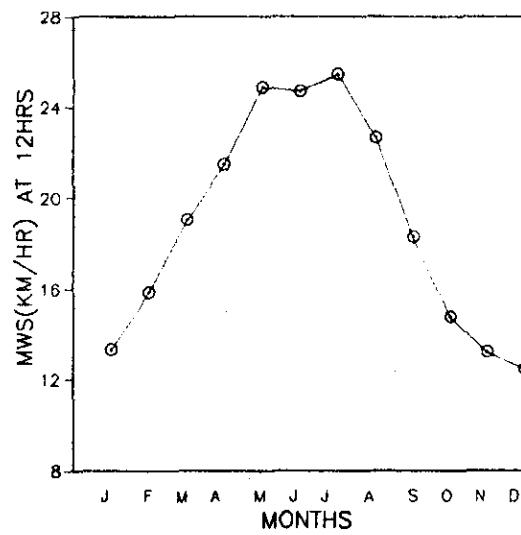


Fig.6(b).Average of monthly mean(based on 20 yrs data) of MWS

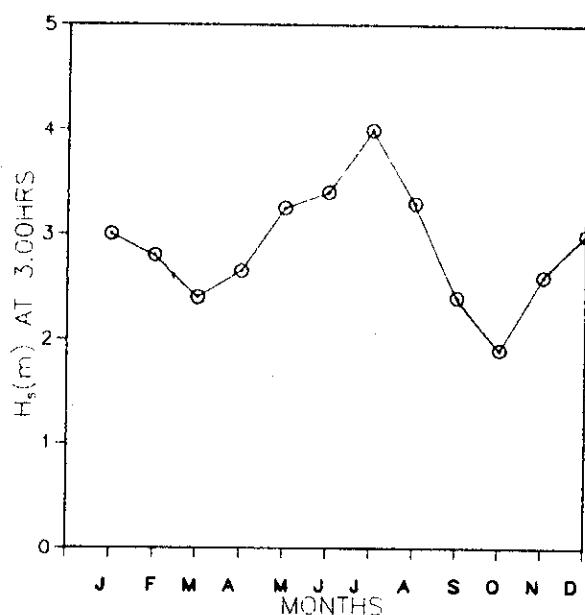


Fig.7(a).Significant wave heights based on the average of monthly mean wind speeds(MWS) of 20 years data

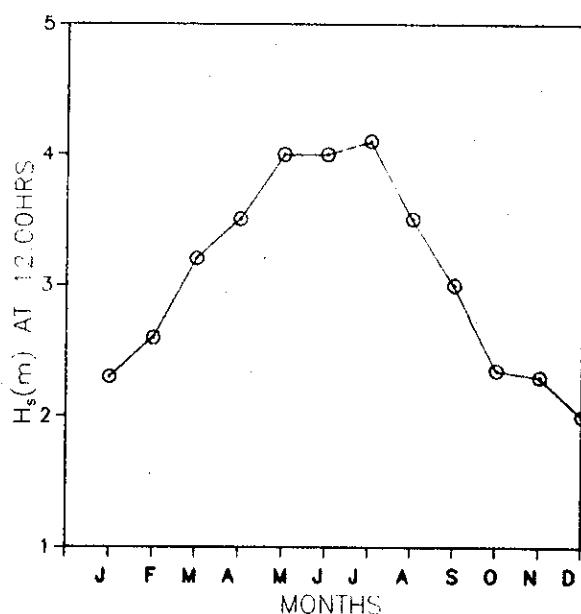


Fig.7(b).Significant wave heights based on the average of monthly mean wind speeds(MWS) of 20 years data



VI. FIELD VANE SHEAR TEST

UC : UNCONFINED COMP.

PP: POCKET PENETROMETER

TEST

TU TRIAXIAL TEST UNDRAINED

NR : NO RECOVERY

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

3.1 LAB VANE SHEAR TEST

UC : UNCONFINED COMP.

PP POCKET PENETROMETER

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TU TRIAXIAL TEST UNDRAINED

NR : NO RECOVERY.

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

4. FIELD VANE SHEAR TEST

UC : UNCONFINED COMP.

PP. POCKET PENETROMETER

TEST

TU TRIAXIAL TEST UNDRAINED

NR : NO RECOVERY

PREPARED BY : COAST

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT	SHEAR STRENGTH	DEPTH	DEPTH*		TIME		CORING			PENETRATION No of Bore						N - VALUE	SAMPLE	TYPE	SAMPLE No.	SAMPLES	DEPTH IN METERS	BORE HOLE NO. MB-7			Sheet 1 of 3						
Water Content	Liquid Limit	Dry Bulk	V.L. PP UC TU	KN/CUM	FROM	TO	DATE	FROM	TO	CR %	SCR %	RDD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm								CO ORDINATES	59°10'05.47"E 22°25'54.80"N OFF POSITRA Rotary REDUCED LEVEL DIA. OF BORE HOLE	Date: 30th Mar. 97 to 2nd Apr. 97 BY JACK-UP BARGE Core dia. 55 mm						
20	40	80	80	100	15	20	25	25	50	75	100	125																					
*All depths are in metres below bed level																																	
0.00		0.00	0.30		18.15	18.30													D5	0.0						Very soft, dark grey, marine silty CLAY							
2.00		1.80	1.90		18.42	18.00													V8	1.80													
3.00		3.30	3.70		19.15	19.35	NR												UDS	3.3													
4.00		4.80	5.20		20.30	20.40							1	0	0	0	2	2	SPT	4.8													
5.00		5.30	5.31	31-Mar	02.25	02.45							1.5/25						>100	SPT	5.3						Light yellow, fine grained, fractures are extremely closely to very closely spaced slightly weathered LIMESTONE.						
6.00		5.30	6.30		03.00	04.30	58%	58%	14%																								
7.00		6.30	7.30		1 Apr	23.00	00.30	36%	36%	18%																							
8.00		7.30	8.80		01.00	02.20	34%	34%	NII																								
9.00		8.80	10.30		02.45	03.15	NR																										
10.00		10.30	10.42		03.35	03.50							12/50						>100	SPT	10.3												
VS FIELD VANE SHEAR TEST		UC: UNCONFINED COMP		TEST		PP: POCKET PENETROMETER		TEST		TU: TRIAXIAL TEST UNDRAINED		NR: NO RECOVERY		PREPARED BY: COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.																			CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT.		SHEAR STRENGTH		SAMPLE RUN NO.	DEPTH FROM TO	TIME FROM TO	CORING	PENETRATION/ No of Blows							N - VALUE	SAMPLE TYPE	SAMPLE No.	SAMPLES	DEPTH IN METERS	BORE HOLE NO. MB-8		Sheet 2 of 3	
										CR %	SCR %	RQD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm		CO ORDINATES	69 09' 51.21" E	22 26' 40.24" N	OFF POSITRA	Date: 2nd April 97 to 3rd April 97		
Plastic Limit	Water Content	Liquid Limit	Dry Bulk	V L	P P	UC	TU									SITE METHOD	BY JACK-UP BARGE	Reduced Level	2.1M Below chart datum	Core Dia 55MM					
20	40	60	80	100	16	20	28	200	400	600	800	1000													
*All depths are in metres below bed level																									
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© 2007 SUPERIOR SOURCE TEST

UC : UNCONFINED COMPR

98. ROCKET PENETROMETER

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TU TRIAXIAL TEST UNDRAINED

NR : NO RECOVERY

FIELD VANE SHEAR TEST

UC UNCONFINED COMP.

→ POCKET PENETROMETER

TEST

J TRIAxIAL TEST UNDRAINED

NR : NO RECOVERY

PREPARED BY : COAST

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

• FIELD VANE SHEAR TEST

UC UNCONFINED COMP

3. BOCHETT BENTHOMETER

EST

1. SWELL TEST UNGRAINED

NB : NO RECOVERY

ANSWERING QUESTIONS

THE UNCONFINED COMPACTION TEST

THE POCKET BENEFTROMETER

TEST

4.2.1.1.1.3. UNDERPAVED

NR : NO RECOVERY

✓ 8. FLEXOVANE SHEAR TEST

UC : UNCONFINED COMP.

20. MOCHET RHEOSTOMETER

11

2013 RELEASE UNDER E.O. 14176

NR : NO RECOVERY

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT	SHEAR STRENGTH		DEPTH SAMPLE RUN NO. TIME Coring	PENETRATION No of blows 15cm 7.5cm 7.0cm 7.5cm 7.5cm	BORE HOLE NO. MB- 11		Sheet 3 of 3			
Water Content %	Liquid Limit	Dry Bulk	V.L P.P U.C T.U	KN/CUM			CR %	SCR %	RQD %	N - VALUE	SAMPLE No.	TYPE
20	40	60	80	100	15	20	25	25	50	75	100	125
20.00												
21.00	14	18.80	21.00			04.00 04.30 NR						
22.00						04.45 05.00						
23.00	15	21.00	23.00			07.00 08.00 NR						
24.00												
25.00	16	23.00	25.00			09.00 10.00 NR						
26.00												
27.00												
28.00												
29.00												
30.00												
VS : FIELD VANE SHEAR TEST		UC : UNCONFINED COMP.		TEST		TEST		TEST		TEST		
PP : POCKET PENETROMETER		NR : NO RECOVERY		TEST		TEST		TEST		TEST		
TU : TRIAXIAL TEST UNDRAINED		PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.		CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.								

*All depths are in metres below bed level

Symbol	DESCRIPTION
	Light yellow, fine grained, completely weathered, LIMESTONE with considerable amount of sandy silt.
	END OF BOREHOLE

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT		SHEAR STRENGTH		DEPTH METERS	SAMPLE RUN NO.	DEPTH*		DATE	TIME		Coring			Penetration/ No of Blows					BORE HOLE NO. MB- 13							
								FROM	TO		FROM	TO	CR %	SCR %	RQD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm								
Water Content %		Liquid Limit		Dry Bulk				VL	PP		UC	TU																
20	40	60	80	100	15	20	25	25	50	75	100	125																
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4. ENFELD LANE SHEAR TEST

UC : UNCONFINED COMP.

SOCKET BAROMETER

TEST

www.4you4you.com

NR : NO RECOVERY

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT.	SHEAR STRENGTH		SAMPLE DEPTH: RUN NO. FROM TO DATE FROM TO ICING	TIME CR % SCR % RQD %	PENETRATION 15cm 7.5cm 7.5cm 7.5cm 7.5cm	No. of shear N + VALUE SAMPLE TYPE SAMPLE No. SAMPLES DEPTH IN METERS	BORE HOLE NO. MB-13		Sheet 2 of 3						
Plastic Limit	Water Content %	KN/CuM	V.L. P.P. U.C. T.U.	DEPTH*					CO ORDINATES 69 11' 24.87" E 22 26' 52.28" N OFF POSITRA Rotary REDUCED LEVEL DIA. OF BORE HOLE	Date: 18th Mar. 97 to 21st Mar. 97 BY JACK-UP BARGE 7.5 M below chart datum 100 MM Core dia. 55 mm							
40	40	80	80	100	15	20	25	30	35	40	45						
*All depths are in metres below bed level																	
11.00		10.50	10.75		06 50	07 00			15	18	2/25	>100 SPT	10.6		Light yellowish brown, fine grained, completely weathered LIMESTONE with trace of silt.		
12.00	10	10.50	12.00		07 30	08 00	NR		10	20	18	19	20	77	SPT	12.0	
13.00		12.00	12.45		08 30	08 40			11	10	13	22	8/25	>100	SPT	13.5	
14.00		13.50	13.92		10 15	10 30			7/35							16.0	
15.00	12	13.50	16.00		14 30	15 30	NR		7	5	4	7	18	34	SPT	16.5	
16.00		16.00	16.07		15 30	16 00			16	4/25						18.0	
17.00		16.00	16.50		16 30	17 30	NR		10/60							19.5	
18.00	14	16.50	18.00		18 30	18 40											
19.00		18.00	18.18	20-Mar	00 30	01 00	NR										
20.00	15	18.00	19.50		06 00	06 30	NR										
		19.50	19.60		07 00	07 10											
V.L. LAB VANE SHEAR TEST		UC : UNCONFINED COMP.															
PP. POCKET PENETROMETER		TEST															
TU. TRIAXIAL TEST UNDRAINED		NR : NO RECOVERY															
PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.													CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.				

4.5 FIELD VANE SHEAR TEST

UC : UNCONFINED COMP.

PP POCKET PENETROMETER

ST

TU TRIAxIAL TEST UNDRAINED

NR . NO RECOVERY

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

1 LAB VANE SHEAR TEST

UC . UNCONFINED COMP.

PP POCKET PENETROMETER

TEST

TRIAXIAL TEST UNDRAINED

LAB VANE SHEAR TEST

UC : UNCONFINED COMP.

POCKET PENETROMETER

TEST

TRIAXIAL TEST UNDRAINED

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CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT.	SHEAR STRENGTH	DEPTH SAMPLE RUN NO. FROM TO DATE TIME CORKING CR % SCR % RQD % 15cm 7.5cm 7.5cm 7.5cm 7.5cm	No. of Blows PENETRATION 15cm 7.5cm 7.5cm 7.5cm 7.5cm	N + VALUE SAMPLING TYPE No. SAMPLES DEPTH IN METERS	BORE HOLE NO. MB-15		Sheet 3 of 3					
			KN/CuM				V.L P.P U.C T.U							
Water Content % Liquid Line		Liquid Line	Dry Bulk											
20	40	60	80	100	15 20 25 28 30 80 75 100 125									
*All depths are in metres below bed level														
21.00				20.60 20.88	08 66 09 10		22	3/25		>100	SPT	20.5		
22.00		11		20.60 22.00	09 40 11 65	NR	21	19	18	18	14	65	SPT	20.0
23.00				20.00 22.45	12 15 12 40		29	23	7.6/31			>100	SPT	23.5
24.00		12	22.00	23.60	13 30 15 00	NR	32	30	4.6/20			>100	SPT	25.0
25.00				23.60 23.80	15 30 15 45									
26.00		13	23.50	25.00	16 35 18 00	NR						>100	SPT	
27.00				25.00 25.27	18 30 18 00									
28.00														
29.00														
30.00														
END OF BOREHOLE														
Symbol DESCRIPTION														
Dark to light greyish yellow, fine grained, completely weathered LIMESTONE.														
UC : UNCONFINED COMP.														
TEST														
NR : NO RECOVERY														
P. POCKET PENETROMETER														
U. TRIAXIAL TEST UNDRAINED														
LAB VANE SHEAR TEST														
PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.														
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.														
Date: 14th Mar. 97 to 16th Mar. 97 BY JACK-UP BARGE Core dia. 55 mm														

• LAB VANE SHEAR TEST

UC : UNCONFINED COMP.

P. POCKET PENETROMETER

TEST

TRIAxIAL TEST UNDRAINED

NO RECOVERY

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

LAB VANE SHEAR TEST UC : UNCONFINED COMP.

UC : UNCONFINED COMP.

POCKET PENETROMETER

三

TRIAXIAL TEST UNDRAINED

NR : NO RECOVERY

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

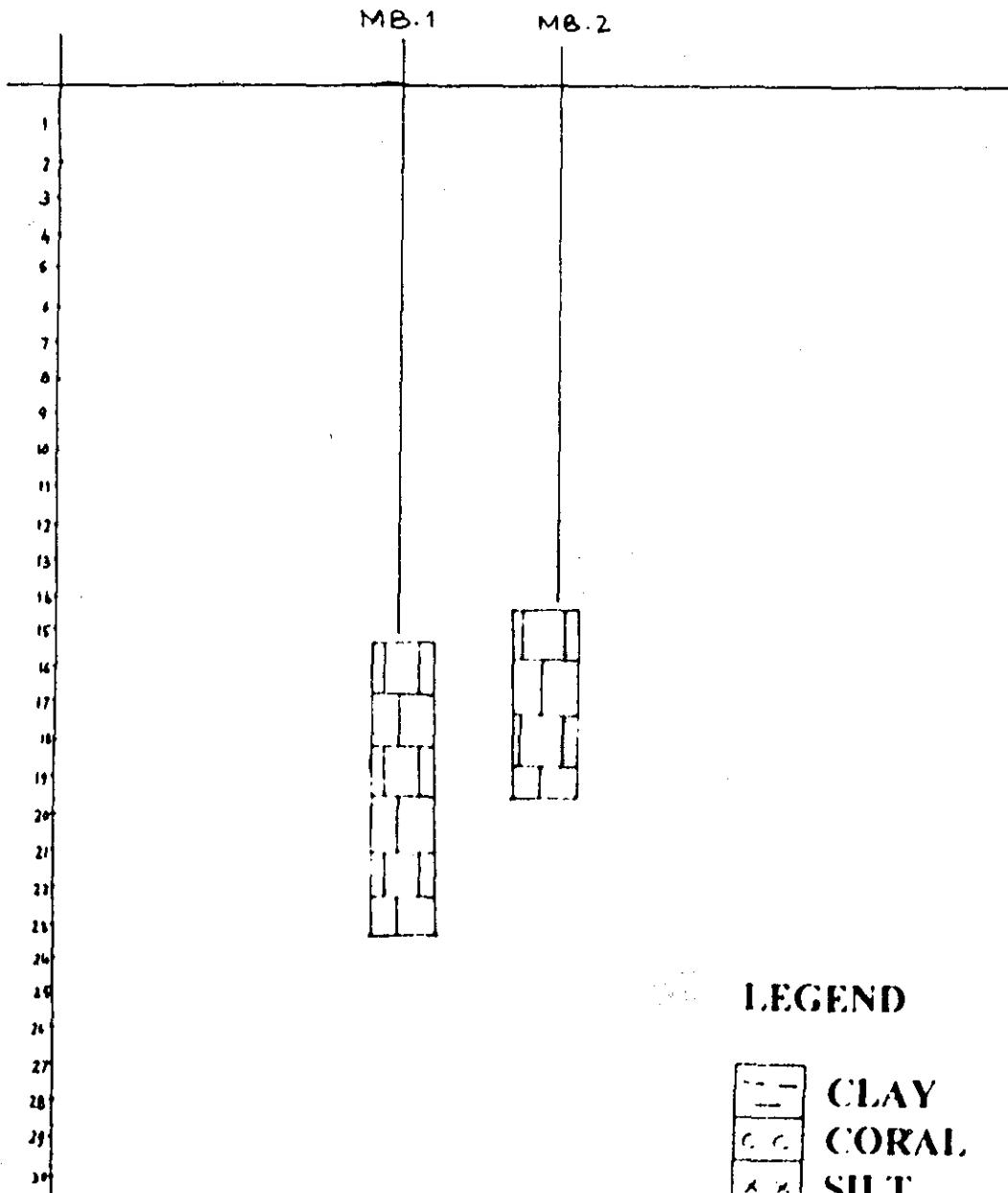
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

ATTERBERG LIMIT		UNIT WT	SHEAR STRENGTH	DEPTH SAMPLE RUN NO.	DEPTH FROM TO	DATE	TIME FROM TO	CORING	PENETRATION	No. of BORES	N - VALUE	TYPE SAMPLE	SAMPLE No.	SAMPLES	DEPTH IN METERS	BORE HOLE NO. MB-16		'Sheet 3 of 3'												
Water Limit	Conc. Limit	Liquid Limit	Dry Bulk								15	20	25	30	40	50	60	70	80	90	100	120	Date: 12th Mar. 97 to 14th Mar. 97							
Paste Line	✓	✓	✓								✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	✓	Core dia. 55 mm							
"All depths are in metres below bed level"																														
20.00																														
21.00																														
22.00																														
23.00																														
24.00																														
25.00																														
26.00																														
27.00																														
28.00																														
29.00																														
30.00																														
A. LAB VANE SHEAR TEST												UC UNCONFINED COMP																		
PP POCKET PENETROMETER												TEST																		
TU TRIAXIAL TEST UNDRAINED												NR - NO RECOVERY																		
PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.																							CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.							

ANNEXURE - 4

**GEOTECHNICAL INVESTIGATION OFF POSITRA
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.**

CHANNEL BOREHOLE

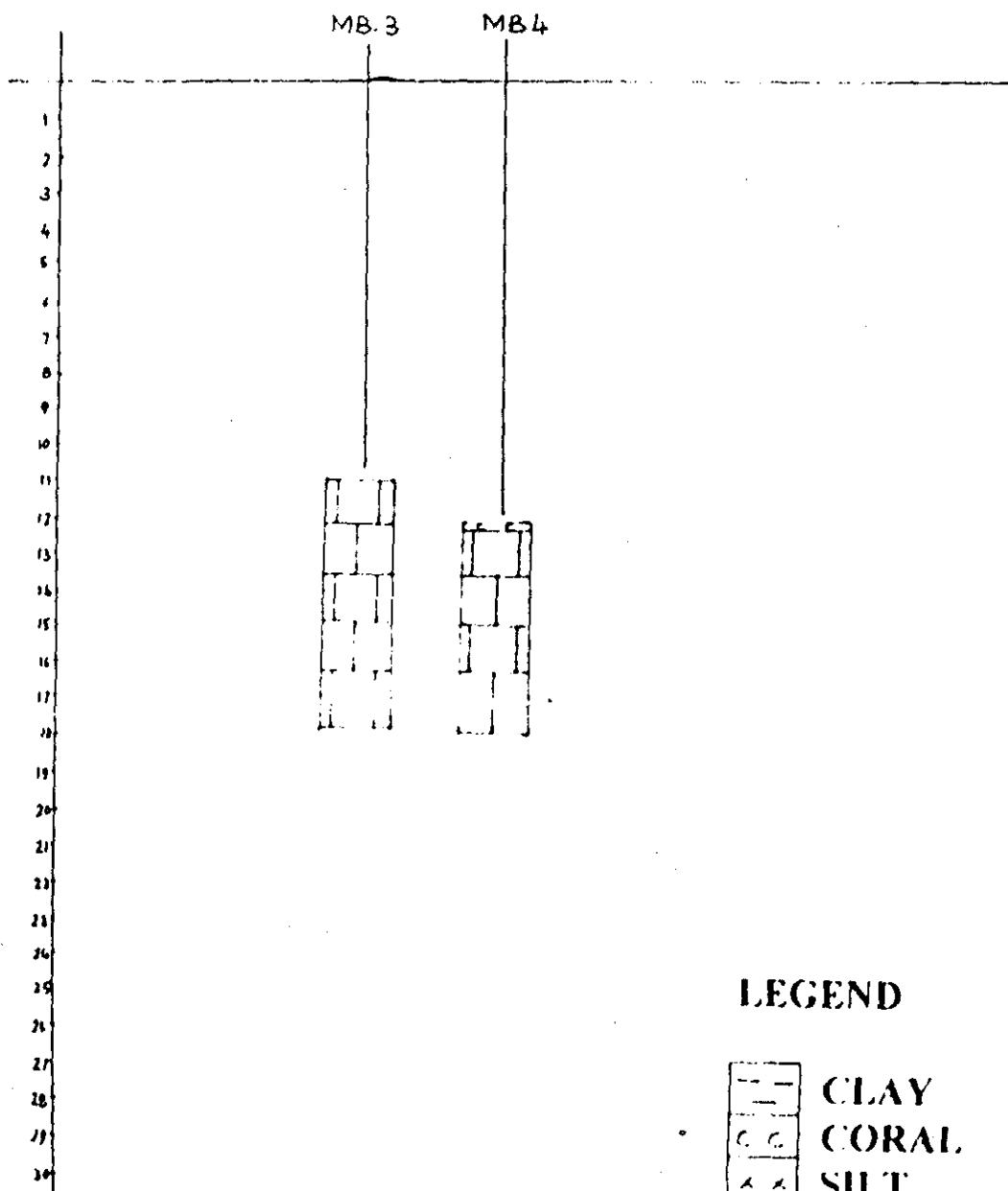


SUB SOIL PROFILE

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

**GEOTECHNICAL INVESTIGATION OFF POSITRA
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.**

CHANNEL BOREHOLE



LEGEND

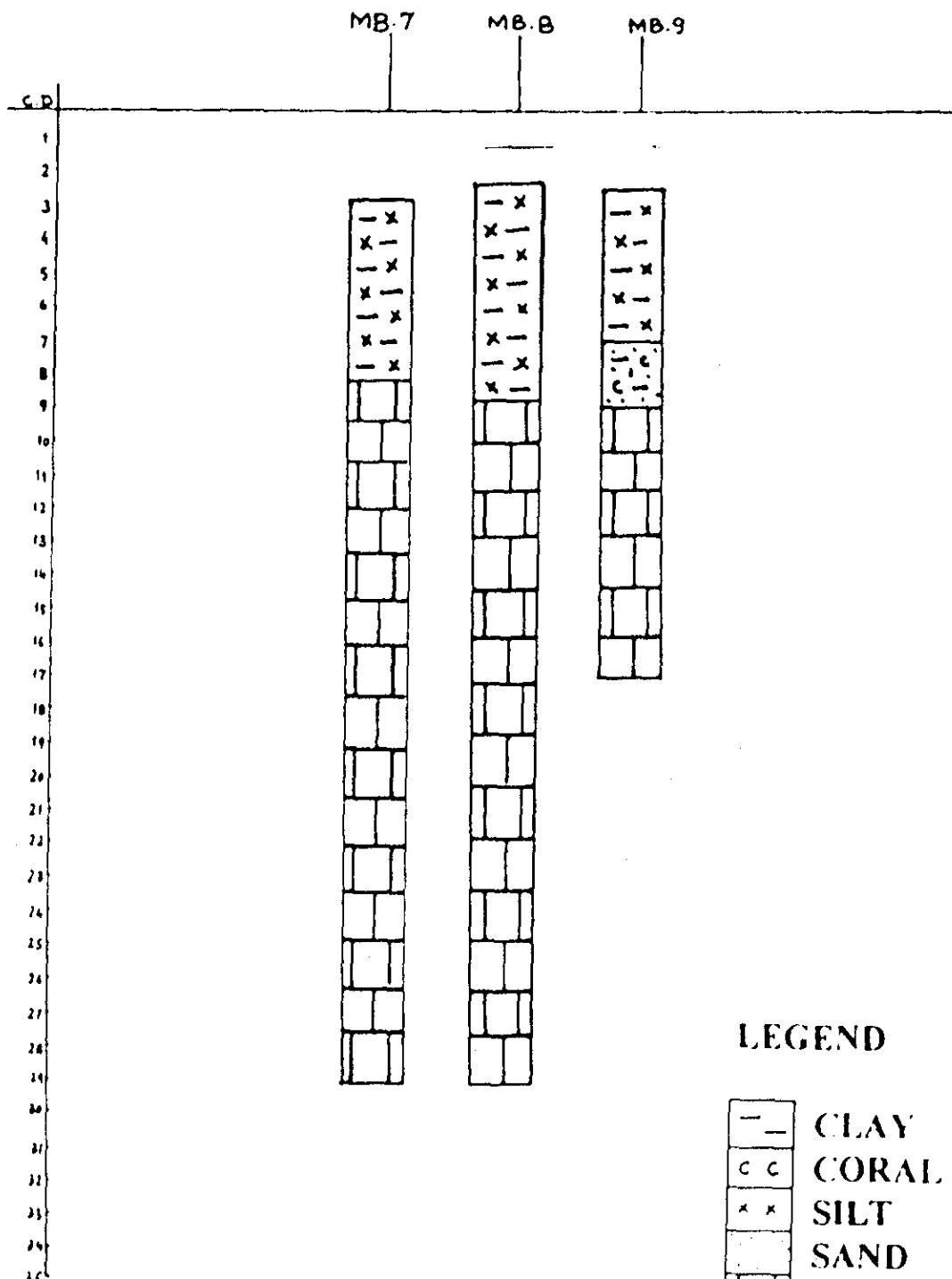
—	CLAY
○○	CORAL
××	SILT
—	SAND
■■■	LIMESTONE

SUB SOIL PROFILE

GEOTECHNICAL INVESTIGATION OFF POSITRA
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

SUB SOIL PROFILE

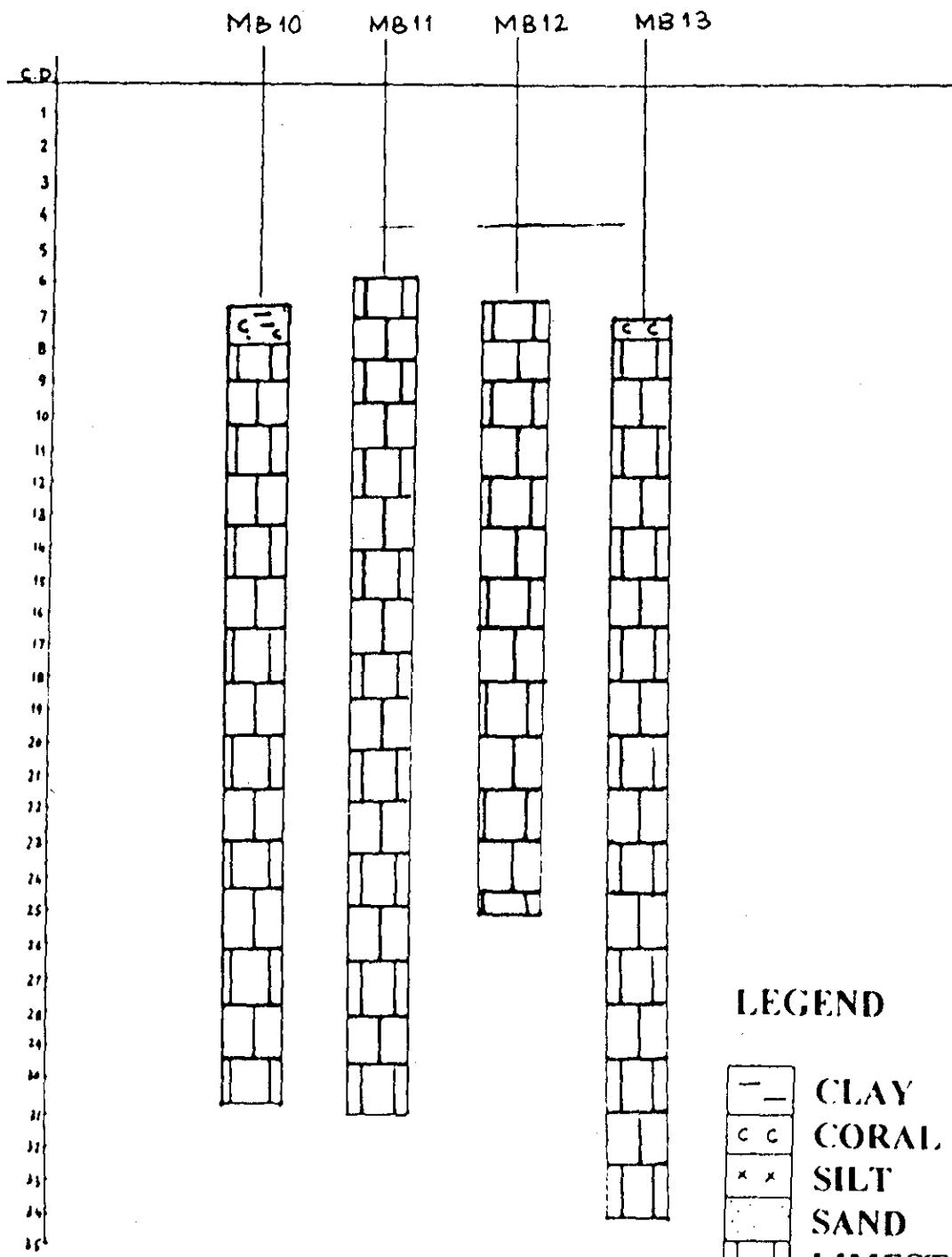
LOCATION - POSITRA II



GEOTECHNICAL INVESTIGATION OFF POSITRA
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

SUB SOIL PROFILE

LOCATION - POSITRA II

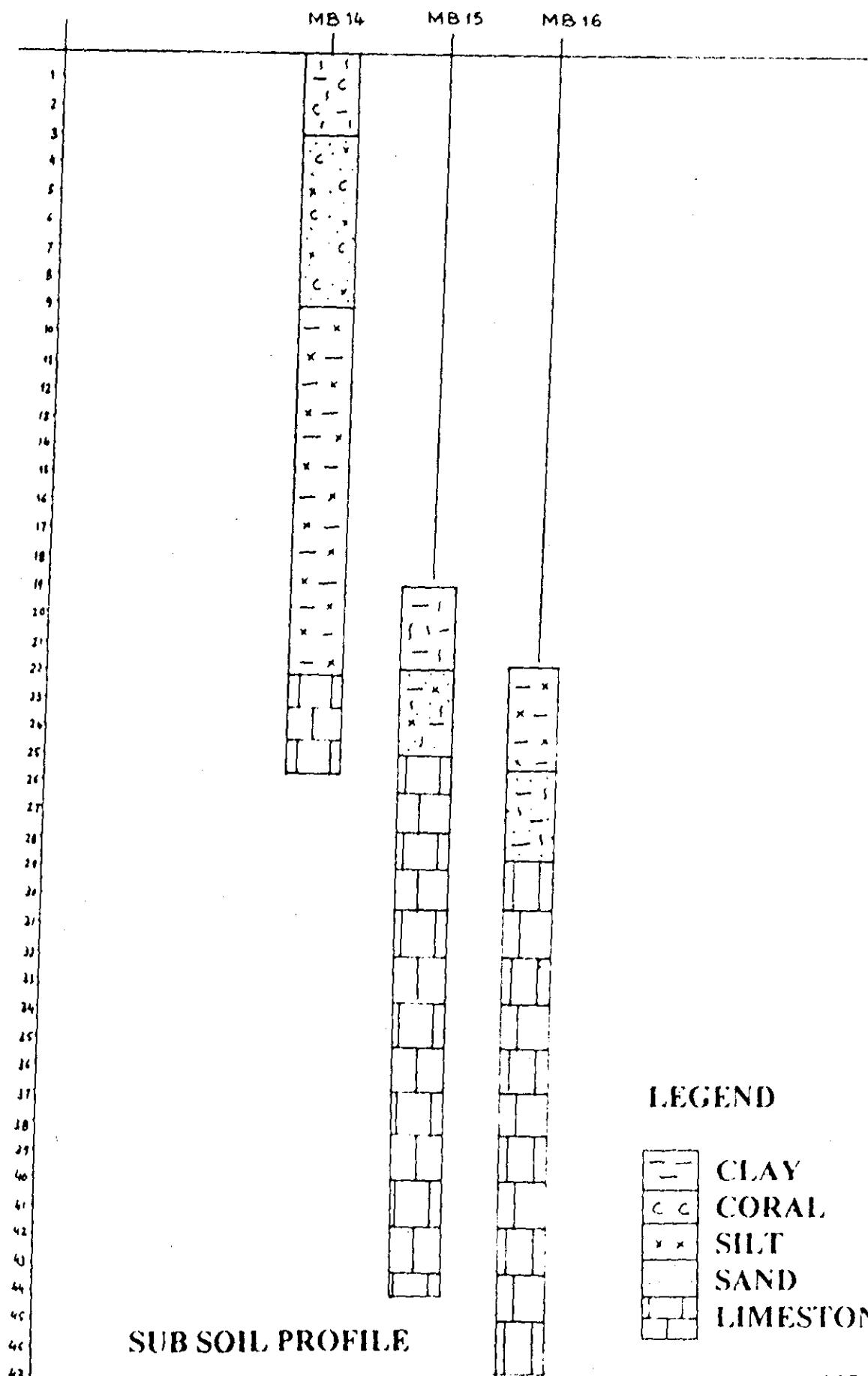


LEGEND

—	CLAY
cc	CORAL
xx	SILT
..	SAND
	LIMESTONE

GEOTECHNICAL INVESTIGATION OFF POSITRA
CLIENT : FREDERIC R. HARRIS (INDIA) PVT. LTD.

LOCATION - POSITRA III



ANNEXURE - 5

TE: POSITRA

SOIL TEST DATA SHEET

E/ E/ E/	DEPTH m	SAMPLE TYPE UD/D	DENSITY		NATURAL MOISTURE CONTENT	MECHANICAL ANALYSIS				CONSISTENCY LIMITS			SOIL CLASSI- FICATION (BS)	SHEAR STRENGTH TEST			CONSOLIDATION TEST		SPECIFIC GRAVITY	OTHER TESTS (SEE LEGEND)	REMARKS
			WET gm/cc	DRY gm/cc		GRAVEL %	SAND %	SILT %	CLAY %	LIQUID %	PLASTIC %	PLAS- TICITY INDEX %		TYPE	COHE- SION (KPa)	ϕ Deg.	COMP. INDEX (Lab.)	INITIAL VOIDS RATIO e_0			
3	5.50	D	-	-	-	20	20	60	41	16	25	CIS	-	-	-	-	-	-	-	-	-
4	3.50	D	-	-	-	1	6	93	57	20	37	CH	-	-	-	-	-	-	-	-	-
7	0.00	D	-	-	-	22	78	71	23	48	CV	-	-	-	-	-	-	-	-	-	-
	14.00	D	-	-	-	6	94	81	26	55	CV	-	-	-	-	-	-	-	-	-	-
	23.00	D	-	-	-	3	57	40	28	17	11	CLS	-	-	-	-	-	-	-	-	-
8	0.00	D	-	-	-	42	58	45	18	27	CIS	-	-	-	-	-	-	-	-	-	-
	14.50	D	-	-	-	7	32	61	34	17	17	CLS	-	-	-	-	-	-	-	-	-
	23.50	D	-	-	-	3	14	83	38	15	23	CI	-	-	-	-	-	-	-	-	-
9	3.00	D	-	-	-	6	42	52	39	21	18	CIS	-	-	-	-	-	-	-	-	-
	12.50	D	-	-	-	34	51	15	-	-	-	SWM	-	-	-	-	-	-	-	-	-
10	0.00	D	-	-	-	46	42	12	-	-	-	SWM	-	-	-	-	-	-	-	-	-
	14.60	D	-	-	-	1	79	20	-	-	-	SML	-	-	-	-	-	-	-	-	-
,	22.10	D	-	-	-	6	53	41	32	14	18	CLS	-	-	-	-	-	-	-	-	-
12	9.10	D	-	-	-	1	19	80	34	15	19	CL	-	-	-	-	-	-	-	-	-

ITEM : CHEMICAL ANALYSIS TEST
 CAMP : COMPACTION TEST
 D : DIRECT SHEAR TEST
 P : PERMEABILITY TEST
 F : FREE SWELL TEST

Tuu : TRIAXIAL TEST UNCONSOLIDATED UNDRAINED
 Tcu : TRIAXIAL TEST CONSOLIDATED UNDRAINED
 Ted : TRIAXIAL TEST CONSOLIDATED DRAINED
 NP : NON PLASTIC
 SL : SHRINKAGE LIMIT TEST

SP : SWELLING PRESSURE OR SWELLING POTENTIAL TEST
 RM : ON REMOULDED SOIL
 VL : LABORATORY VANE SHEAR TEST
 UC : UNCONFINED COMPRESSION TEST

DRG. NO.: 8522/74

AFCONS

TE: POSITRA

SOIL TEST DATA SHEET

EM : CHEMICAL ANALYSIS TEST
MP : COMPACTION TEST
D : DIRECT SHEAR TEST
P : PERMEABILITY TEST
F : FREE SWELL TEST

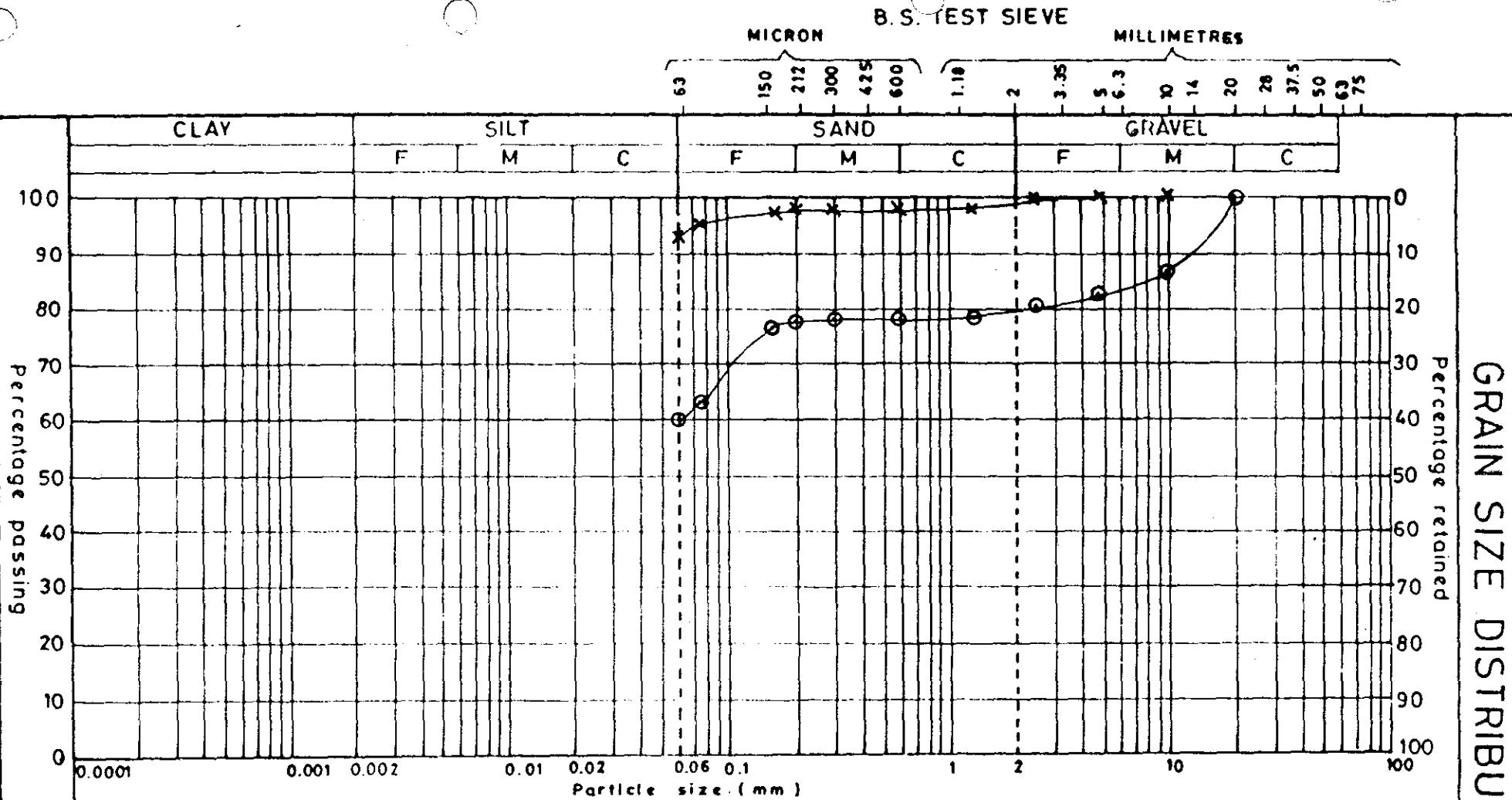
Tuu : TRIAXIAL TEST UNCONSOLIDATED UNDRAINED
Tcu : TRIAXIAL TEST CONSOLIDATED UNDRAINED
Tcd : TRIAXIAL TEST CONSOLIDATED DRAINED
NP : NON PLASTIC
SL : SHRINKAGE LIMIT TEST

SP : SWELLING PRESSURE OR SWELLING
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DRG. NO.: 8522 / 74

AFCONS

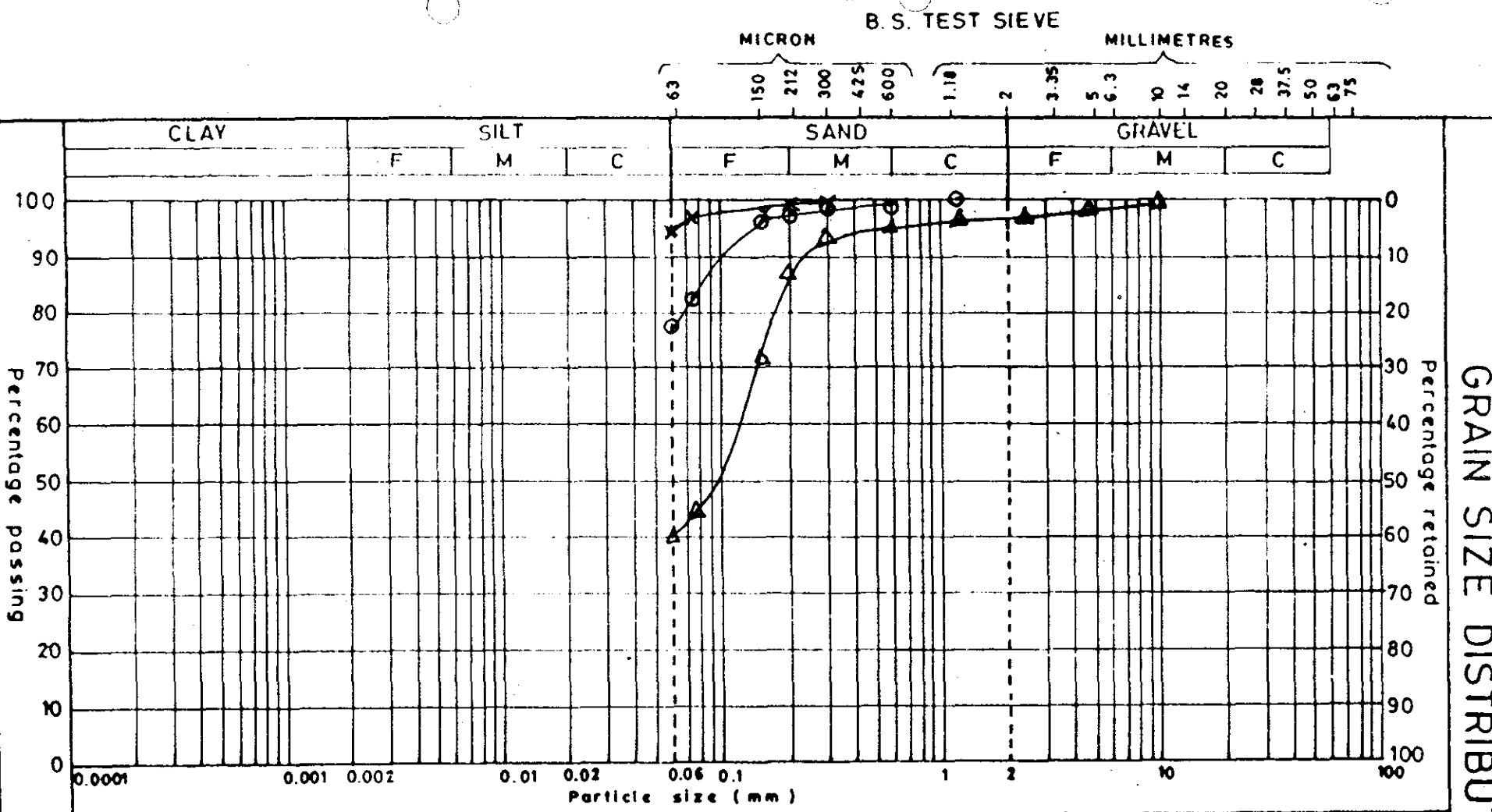
GRAIN SIZE DISTRIBUTION



SITE : POSITRA

Symbol	BOREHOLE No.	Depth m	Classification (B.S.)	Grav. %	Sand %	Silt %	Clay %	$\phi 10\%$ mm	$\phi 30\%$ mm	$\phi 60\%$ mm	Cu	Cc	Remarks
○ - ○	MB-3	5.50	CIS	20	20	60	-	-	-	-	-	-	D
× - ×	MB-4	3.50	CH	1	6	93	-	-	-	-	-	-	D

GRAIN SIZE DISTRIBUTION

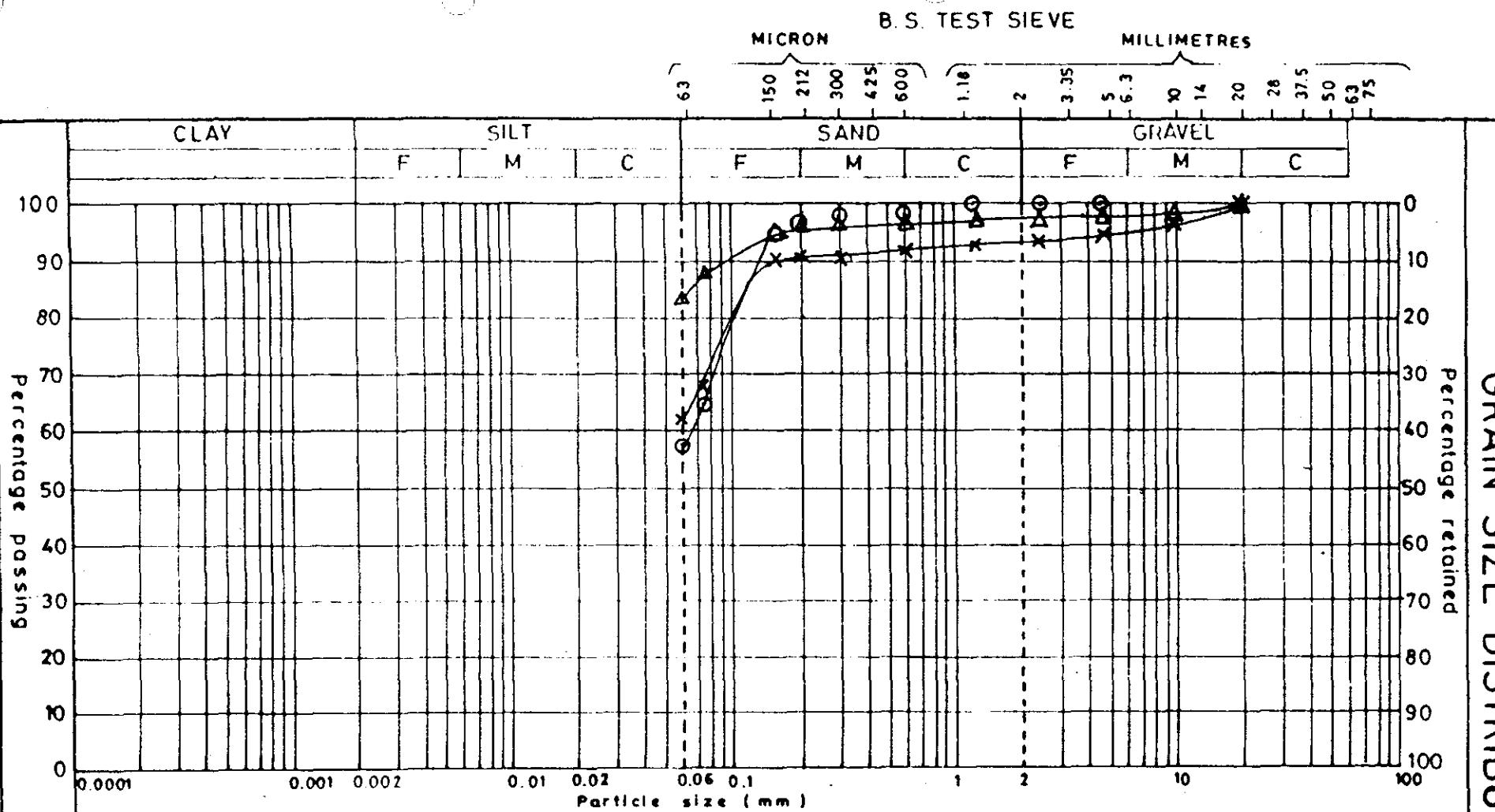


SITE : POSITRA

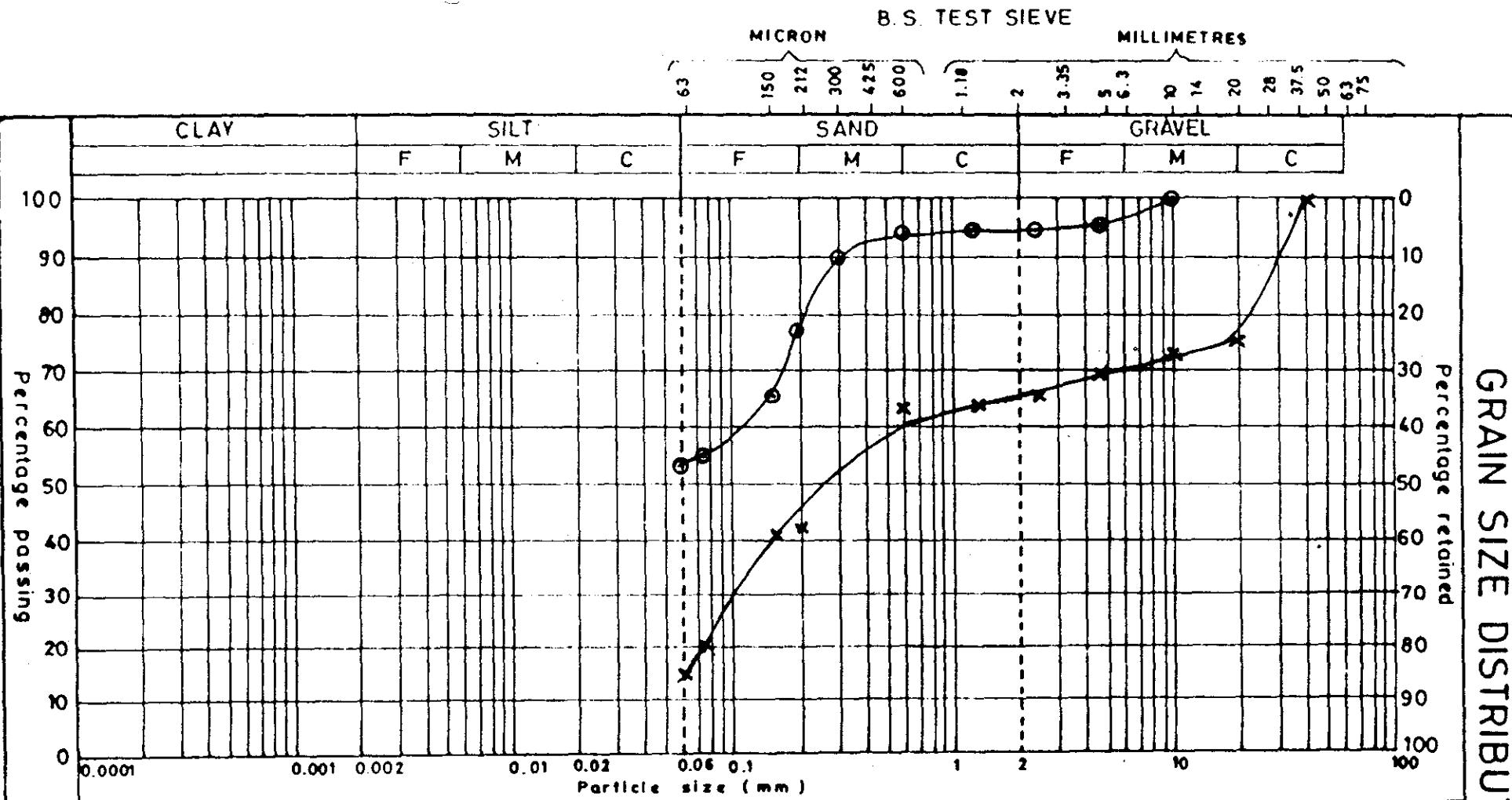
AFCONS COMPANY DATE : 15/4/97 DRG. NO. 8522/74

GRAIN SIZE DISTRIBUTION

SITE: POSITRA



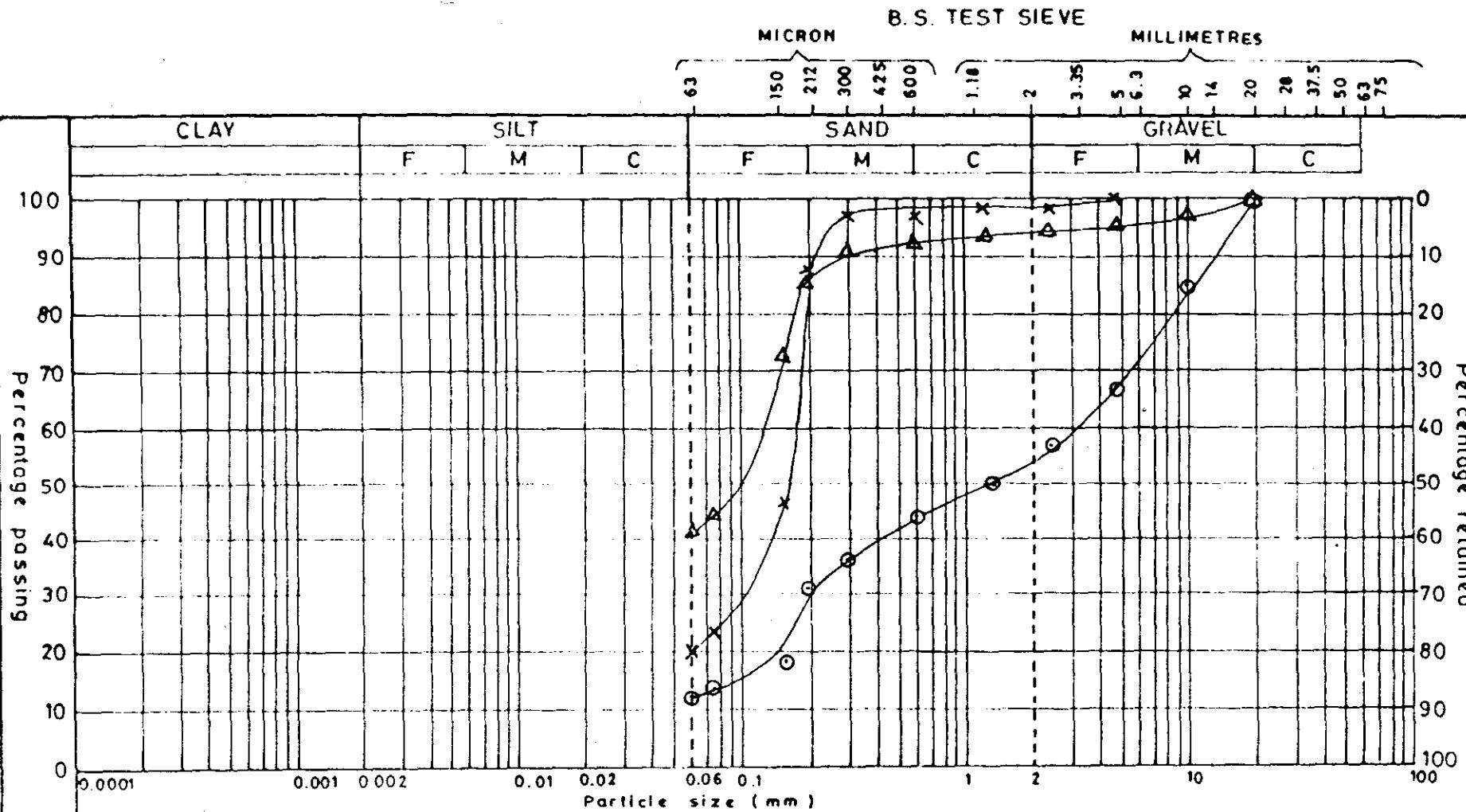
GRAIN SIZE DISTRIBUTION



SITE : POSITRA

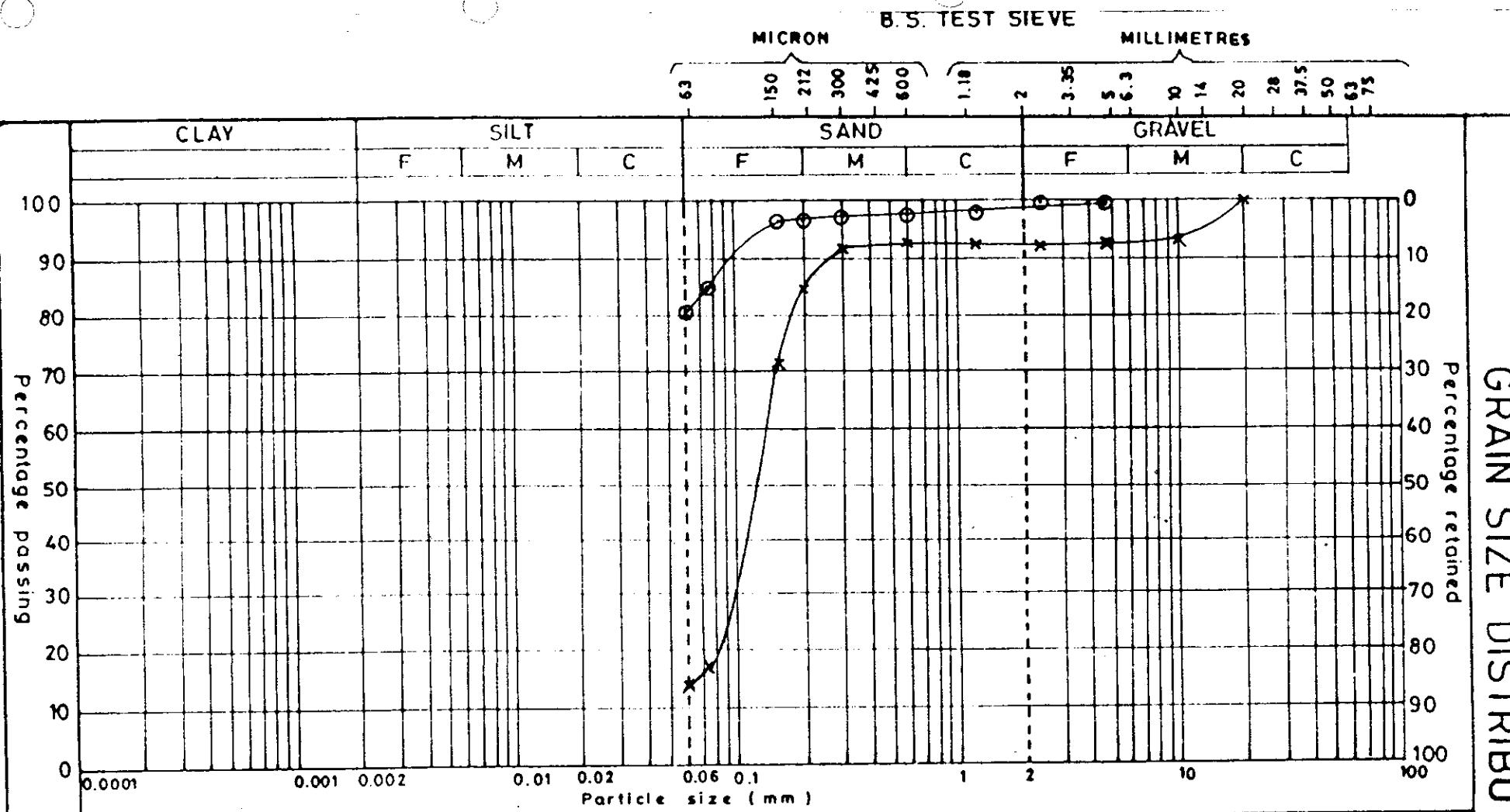
Symbol	BOREHOLE No.	Depth m	Classification (B.S.)	Grav. %	Sand %	Sh. %	Clay %	$\phi_{10\%}$ mm	$\phi_{30\%}$ mm	$\phi_{60\%}$ mm	Cu	Cc	Remarks
○○	MB - 9	3.00	CIS	6	42	52	-	-	-	-	-	-	D
××		12.50	SWM	34	51	15	-	-	-	-	-	-	D

GRAIN SIZE DISTRIBUTION

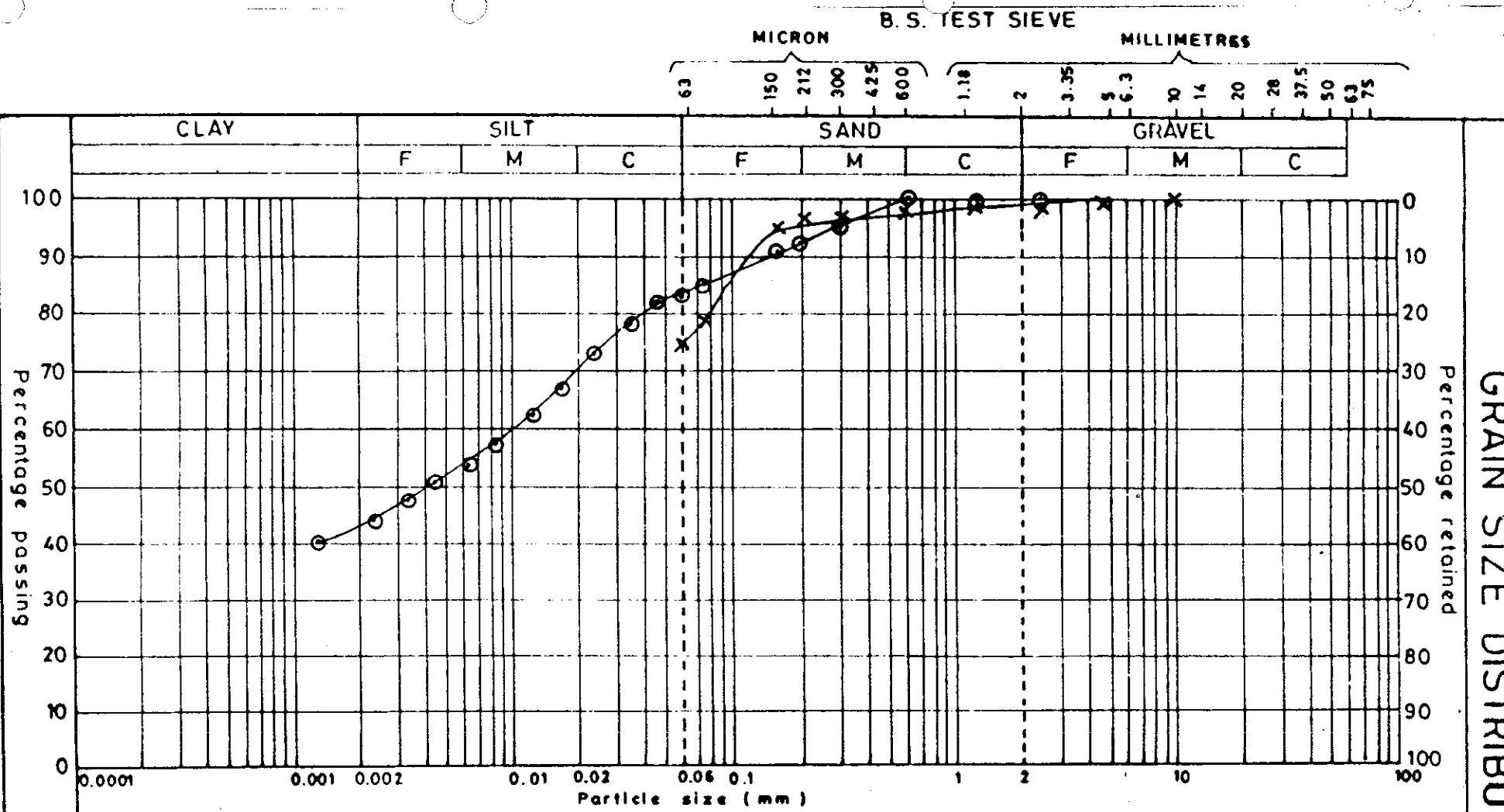


GRAIN SIZE DISTRIBUTION

SITE: POSITRA



GRAIN SIZE DISTRIBUTION



TRIAXIAL COMPRESSION TEST

SITE **POSITRA**

TYPE OF TEST **UU**

RATE OF STRAIN **1.25 mm/min.**

SPECIMEN MEASUREMENTS **$\sigma = 38 \text{ mm}$**
 $L = 26 \text{ mm}$

DATE **17-4-97**

BORE HOLE NO **MB-14**

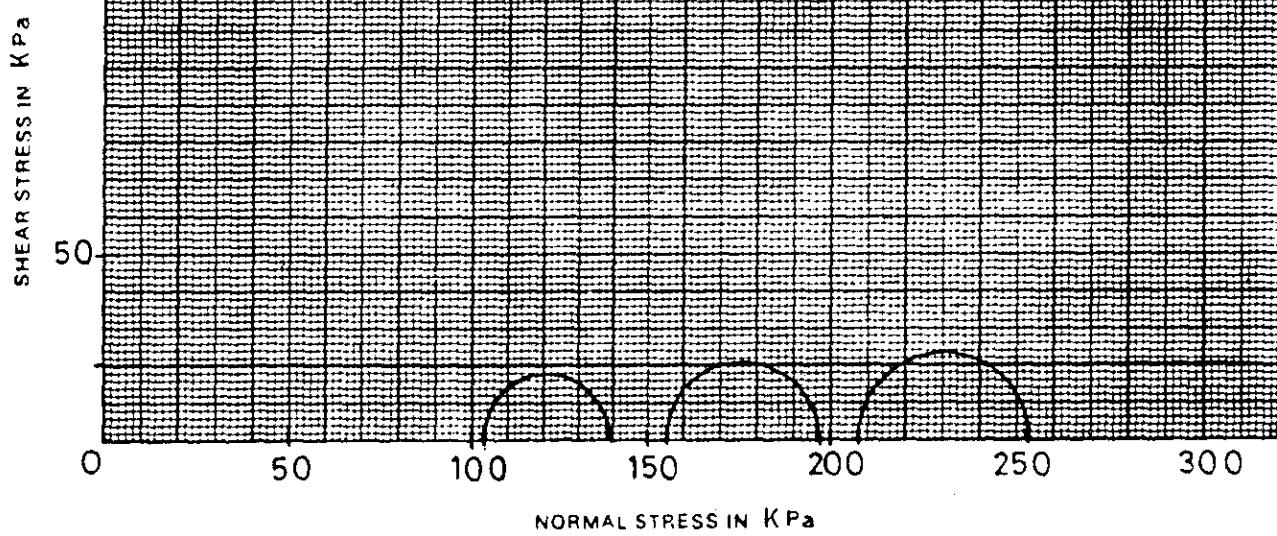
SAMPLE DEPTH **10.50 / 10.90 m**

VISUAL DESCRIPTION

Soft grey CLAY.

BULK DENSITY: **1.57 gm/cc**
 MOISTURE CONTENT: **66 %** } AVERAGE OF 3 SPECIMEN

SR. NO.	CELL PRESSURE IN KPa	DEVIATOR STRESS AT FAILURE IN KPa	PORE PRESSURE AT FAILURE IN KPa	STRAIN AT FAILURE IN %
1	104	37.4	-	7
2	156	41.6	-	11
3	208	46.8	-	12



COHESION INTERCEPT **$C = 21 \text{ KPa}$**

ANGLE OF SHEARING RESISTANCE **$\phi = 0$**

AFCONS

8522/7
DRG. NO.

UNCONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST

SITE: POSITRA

BOREHOLE NO. MB-14 DEPTH: 10.50 / 10.90 m

PECIMEN NO.:

1

CELL PRESSURE (KPa)

(104)

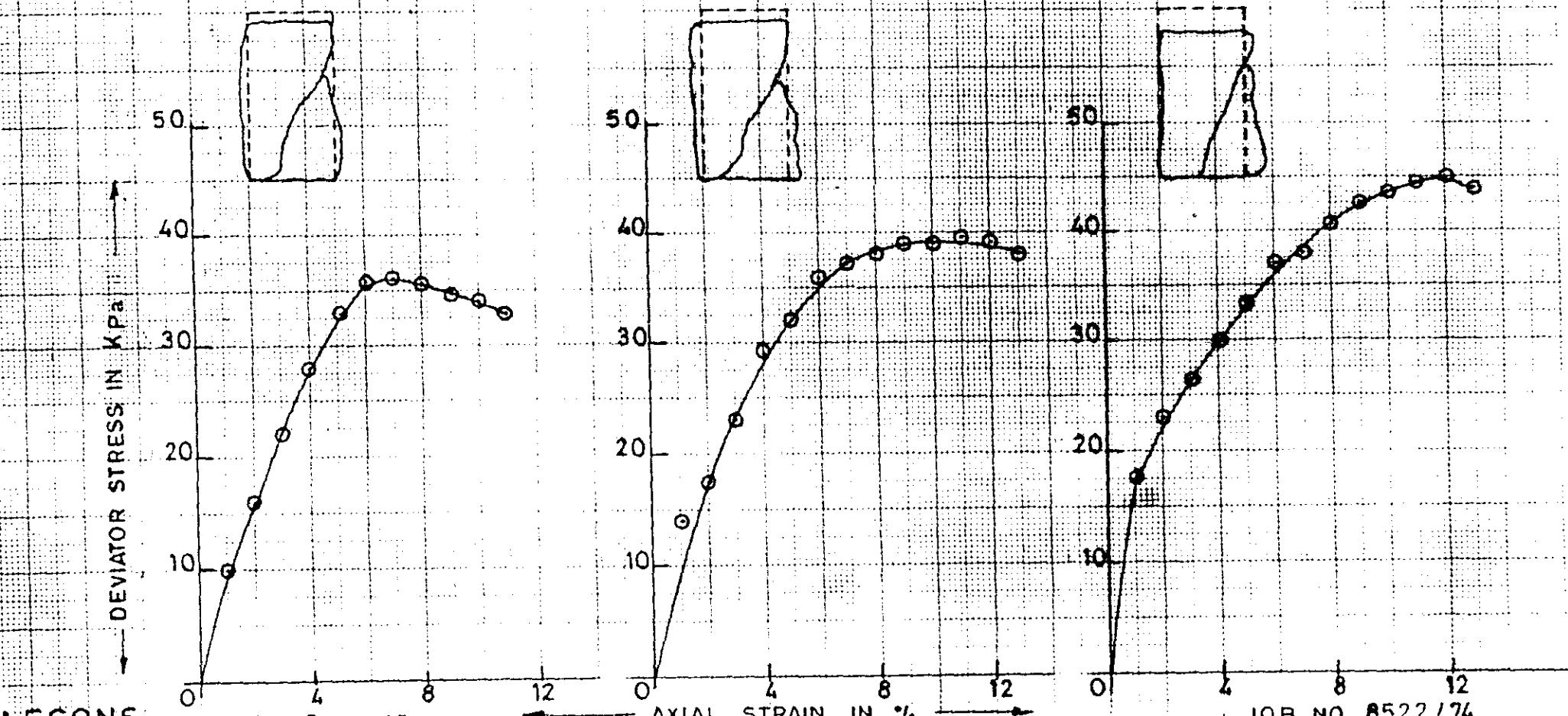
2

(156)

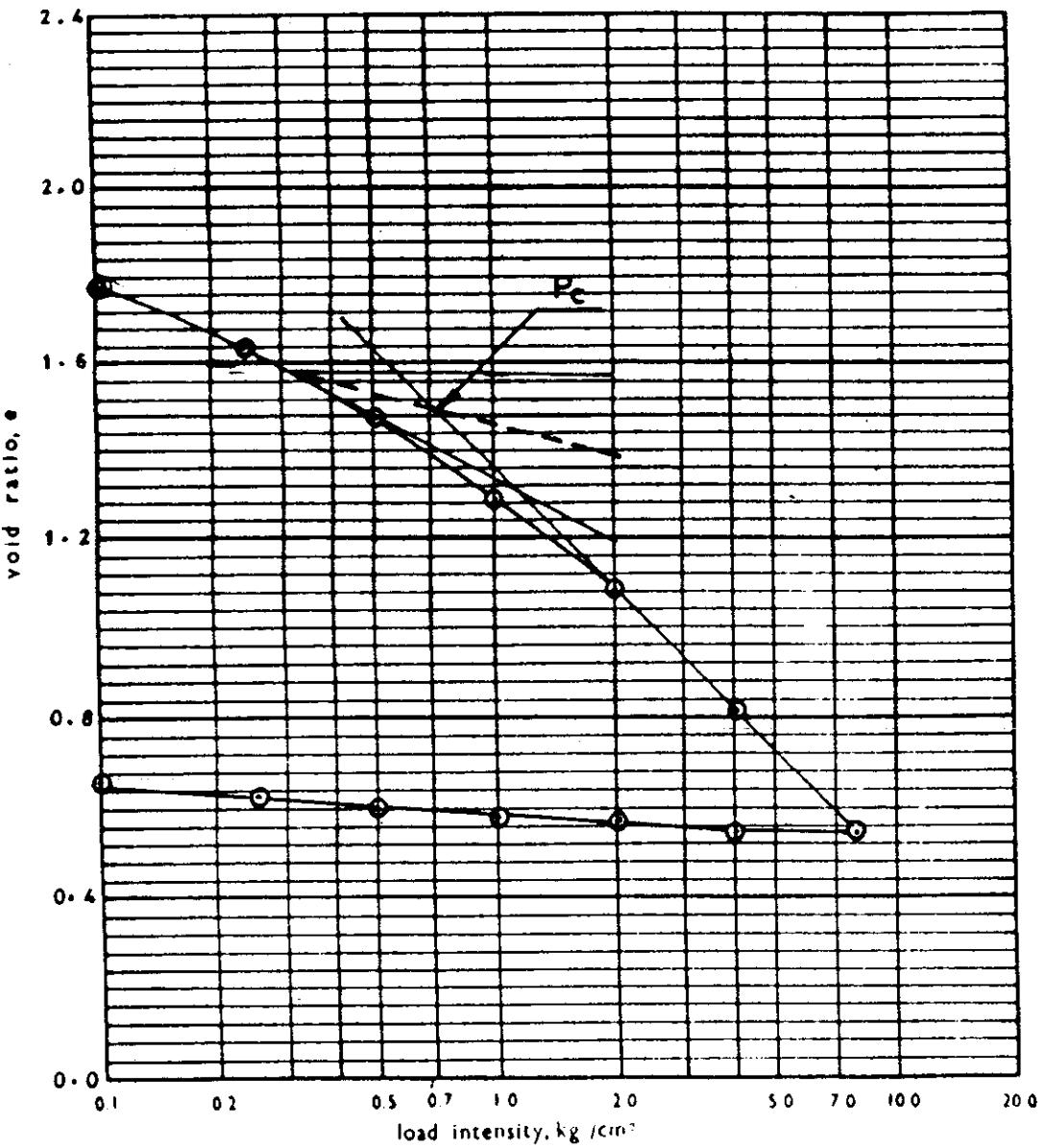
3

(208)

SKETCH OF SPECIMEN AFTER FAILURE:



SITE:- POSITRA



CONSOLIDATION TEST DATA

BORE HOLE No.MB 14 DEPTH:10.50 m. TO 10.90 m.

$$(C_c)_{\text{lab}} = 0.90, \bar{P}_c = 0.73 \text{ kg}/\text{cm}^2, G_s = 2.64$$

Prior To Test	At The End of Test
$\gamma = 1.57 \text{ g}/\text{cm}^3$	$\gamma_w = 1.99 \text{ g}/\text{cm}^3$
$\gamma_d = 0.95 \text{ g}/\text{cm}^3$	$\gamma_d = 1.59$
$w = 65 \%$	$W = 25$
$e_0 = 1.778$	$e_0 = 0.662$
$S_r = 97 \%$	$S_r = 100 \%$

TIME RATE SETTLEMENT DATA

LOAD INCREMENT IN kg/cm^2	COEFFICIENT OF CONSOLIDATION $C_v, \text{m}^2/\text{year}$	COEFFICIENT OF VOLUME COMPRESSIBILITY $m_v, \text{cm}^2/\text{kg}$
0.10/0.25	1.50	33.80×10^{-2}
0.25/0.50	1.20	24.60×10^{-2}
0.50/1.00	0.80	15.00×10^{-2}
1.00/2.00	0.60	8.70×10^{-2}
2.00/4.00	0.50	6.40×10^{-2}
4.00/8.00	0.30	3.70×10^{-2}

TE : POSITRA

ROCK TEST DATA SHEET

RE S.	CORE PIECE NO.	DEPTH m	DENSITY		WATER CONTENT %	POROSITY %	WATER ABSORB- PTION %	SPECIFIC GRAVITY	UNIAXIAL COMPRESSIVE STRENGTH						POINT LOAD STRENGTH				OTHER TESTS SEE ADDL. SHEET	
			BULK gm/cc	DRY gm/cc					DIA- METER cm	HEIGHT cm	D:H	UNIAXIAL COMPRESSIVE STRENGTH MPa	MODULUS OF ELASTICITY Kg/cm ²	POISSON'S RATIO	CONDITION OF TEST	DIA- METER mm	LENGTH mm	CORRECTED STRENGTH INDEX IS (50) MPa	CONDITION OF TEST	
3-1	3	0.5	-	2.25	-	-	-	-	-	-	-	-	-	-	53	78	2.99	U	-	
	6	1.0	-	2.13	-	-	-	-	5.3	6.9	1:1.30	6.4	-	-	U	-	-	-	-	-
3-2	1	0.0	-	2.40	-	-	-	-	5.4	6.3	1:1.17	30.2	-	-	U	-	-	-	-	-
	7	2.3	-	2.30	-	-	-	-	-	-	-	-	-	-	52	75	2.31	U	-	
	11	3.6	-	2.50	-	-	-	-	-	-	-	-	-	-	54	75	3.27	U	-	
3-7	-	5.60/ 5.75	-	2.10	-	-	-	-	5.4	10.6	1:1.96	21.8	-	-	U	-	-	-	-	-
	-	8.55/ 8.60	-	2.19	-	-	-	-	-	-	-	-	-	-	52	40	1.54	U	-	
	-	18.45/ 18.50	-	2.19	-	-	-	-	-	-	-	-	-	-	53	60	1.12	U	-	
3-8	-	25.00/ 25.07	-	2.09	-	-	-	-	-	-	-	-	-	-	53	90	0.75	U	-	
	-	26.00/ 26.15	-	2.25	-	-	-	-	5.3	10.4	1:1.96	6.8	-	-	U	-	-	-	-	-
3-9	-	15.45	-	2.70	-	-	-	-	-	-	-	-	-	-	53	77	3.36	U	-	

OTES: 1. UNIAXIAL COMPRESSIVE STRENGTH CORRECTED FOR
D:H = 1:2 (As per ASTM : D 2938)

2. * INDICATES THE SAMPLE FAILED ALONG JOINTS.

3. Δ - - - WHILE PREPARATION.

4. ▲ - - - CRUMBLED IN WATER.

S = SOAKED (FOR 24 Hrs. in water)

U = UNSOAKED

D = OVEN DRY

RLL = POINT LOAD LUMP STRENGTH

TSB = TENSILE STRENGTH (BRAZILIAN)

DTS = DIRECT TENSILE STRENGTH

TXL = TRIAXIAL COMPRESSION TEST

PET = PETRO GRAPHIC EXAMINATION

DRG. NO. 8522 / 74

TE : POSITRA

ROCK TEST DATA SHEET

CORE PIECE NO.	DEPTH m	DENSITY		WATER CONTENT %	POROSITY %	WATER ABSOR- PTION %	SPECIFIC GRAVITY	UNIAXIAL COMPRESSIVE STRENGTH						POINT LOAD STRENGTH				OTHER TESTS SEE ADDL. SHEET	
		BULK gm/cc	DRY gm/cc					DIA- METER cm	HEIGHT cm	D:H	UNIAXIAL COMPRESSIVE STRENGTH MPa	MODULUS OF ELASTICITY Kg/cm ²	POISSON'S RATIO	CONDITION OF TEST	DIA- METER mm	LENGTH mm	CORRECTED STRENGTH INDEX IS (50) MPa	CONDITION OF TEST	
0 -	2.65 / 2.70	-	2.23	-	-	-	-	-	-	-	-	-	-	-	53	50	1.48	U	-
	-	5.40 / 5.55	-	2.40	-	-	-	5.4	9.9	1:1.83	30.0	-	-	U	-	-	-	-	-
11 1	1.0	-	2.22	-	-	-	-	-	-	-	-	-	-	-	54	64	1.09	U	-
7	2.8	-	2.15	-	-	-	-	5.2	9.6	1:1.85	20.8	-	-	U	-	-	-	-	-
13	3.5	-	2.08	-	-	-	-	5.4	10.1	1:1.87	19.4	-	-	U	-	-	-	-	-
18	5.8	-	2.20	-	-	-	-	-	-	-	-	-	-	-	54	67	2.18	U	-
23	18.5	-	2.18	-	-	-	-	5.3	7.4	1:1.40	12.7	-	-	U	-	-	-	-	-

TESTS: 1 UNIAXIAL COMPRESSIVE STRENGTH CORRECTED FOR

$$D:H = 1 \quad 2$$

2. ● INDICATES THE SAMPLE FAILED ALONG JOINTS.

3 A " " " WHILE PREPARATION.

CRUMBLIED IN WATER

S = SOAKED (FOR 24 Hrs. in water)

U = UNSOAKED

D = OVEN DRY

RLL = POINT LOAD LUMP STRENGTH

TSB = TENSILE STRENGTH (BRAZILIAN)

DTS = DIRECT TENSILE STRENGTH

TXI - 3 TRIAXIAL COMPRESSION TEST

BET - A RETRO GRAPHIC EXAMINATION

DRG NO 8522 / 74

SITE : POSITRA

ROCK TEST DATA SHEET

BORE HOLE NO.	CORE PIECE NO.	DEPTH m	DENSITY		WATER [*] CONTENT %	POROSITY %	WATER ABSORPTION %	SPECIFIC GRAVITY	UNIAXIAL COMPRESSIVE STRENGTH						POINT LOAD STRENGTH				OTHER TESTS SEE ADDL. SHEET	
			BULK	DRY					DIA-METER cm	HEIGHT cm	D:H	UNIAXIAL COMPRESSIVE STRENGTH MPa	MODULUS OF ELASTICITY Kg/cm ²	POISSON'S RATIO	CONDITION OF TEST	DIA-METER mm	LENGTH mm	CORRECTED STRENGTH INDEX IS (50) MPa	CONDITION OF TEST	
IB-12	-	0.30 / 0.35	-	2.48	-	-	-	-	-	-	-	-	-	-	-	53	53	3.75	U	-
	4	0.40	-	2.21	-	-	-	-	5.4	9.0	1:1.67	40.5	-	-	U	-	-	-	-	-
	7	0.90 / 1.20	-	2.28	-	-	-	-	5.4	10.7	1:1.98	43.6	-	-	U	-	-	-	-	-
	11	3.0	-	1.96	-	-	-	-	5.4	11.5	1:2.13	19.8	-	-	U	-	-	-	-	-
	13	3.40 / 3.55	-	1.99	-	-	-	-	5.4	10.8	1:2.00	26.2	-	-	U	-	-	-	-	-
	16	5.2	-	2.33	-	-	-	-	5.4	10.8	1:2.00	26.2	-	-	U	-	-	-	-	-
	20	7.6	-	2.30	-	-	-	-	5.4	9.7	1:1.80	15.1	-	-	U	-	-	-	-	-
IB-13	1	2.5	-	2.27	-	-	-	-	-	-	-	-	-	-	-	53	100	1.87	U	-
	4	8.5	-	2.33	-	-	-	-	-	-	-	-	-	-	-	54	79	3.27	U	-
	8	21.00	-	2.70	-	-	-	-	-	-	-	-	-	-	-	54	72	3.64	U	-

NOTES: 1. UNIAXIAL COMPRESSIVE STRENGTH CORRECTED FOR
D:H = 1:2 (As per ASTM : D 2938)

2. * INDICATES THE SAMPLE FAILED ALONG JOINTS.

3. Δ WHILE PREPARATION.

4. \blacktriangle CRUMBLED IN WATER.

S = SOAKED (FOR 24 Hrs. in water)

U = UNSOAKED

D = OVEN DRY

RLL = POINT LOAD LUMP STRENGTH

TSB = TENSILE STRENGTH (BRAZILIAN)

DTS = DIRECT TENSILE STRENGTH

TXL = TRIAXIAL COMPRESSION TEST

PET = PETRO GRAPHIC EXAMINATION

DRG. NO. 8522 / 74

TE : POSITRA

ROCK TEST DATA SHEET

TESTS : 1. UNIAXIAL COMPRESSIVE STRENGTH CORRECTED FOR
D:H = 1:2 (As per ASTM : D 2938)

2. ● INDICATES THE SAMPLE FAILED ALONG JOINTS

3. A " " " WHILE PREPARATION

CRUMBLIED IN WATER

S = SOAKED (FOR 24 Hrs. in water)

U = UNSOAKED

D = OVEN DRY

RLL = POINT LOAD LUMP STRENGTH

TSB = TENSILE STRENGTH (BRAZILIAN)

DTS = DIRECT TENSILE STRENGTH

TXI = TRIAXIAL COMPRESSION TEST

RET = RETRO GRAPHIC EXAMINATION

PER - PETROGRAPHIC EXAM
DRG. NO 8522/74

DATE: 12-4-97

FCONS

APPENDIX F

**REPORT ON ONSHORE GEOTECHNICAL
INVESTIGATION AT POSITRA**

BY

**COASTAL MARINE CONSTRUCTION
AND ENGG. LTD., MUMBAI.**

**Coastal Marine Construction
& Engineering Ltd**
COMACOE
~~██████████~~

Final Report

on

**Onshore Geotechnical
Investigation**

for

Frederic R Harris (India) Pvt. Ltd



HARRIS

**at Positra II and Positra III
Gulf Of Kutch
Gujarat**

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ON-SHORE GEOTECHNICAL INVESTIGATION AT POSITRA

1.0 INTRODUCTION

Gujarat Maritime Board, Under the port policy of Government of Gujarat, put forward a white paper on the frame work for developing various ports around the coast of Gujarat. M/s Frederic R. Harris (India) Pvt. Ltd. awarded the assignment for preparing a detailed project report for development of port facility at Positra.

At Positra, the Geotechnical investigations are required to be carried out to provide engineering properties, nature and performance of subsurface strata for deciding the load carrying capacities for movement of crane and large stock piles.

In this regard, M/s Frederic R. Harris (India) Pvt. Ltd. placed their Letter of Intent dated June 10th 1996 on Coastal Marine Construction & Engineering Limited, for the work of Geotechnical Investigation at Positra.

1.1 LOCATION AND GENERAL INFORMATION

Positra is located on the western side of the Gulf of Kutch on its southern bank. The existing OKHA port lies around 5 Knautical miles to its west.

The area in general has various small islands which cover to varied extents during different stages of high tides.

Presence of these islands cause predictable cross currents in the early flooding period which are quite strong and do not follow a precise pattern.

2.0 OBJECTIVE AND SCOPE OF THE WORK:

2.1 OBJECTIVE

The purpose of the sub soil investigation is to provide information of the extent, depth and thickness of the various soil strata underlying the project sites to establish the engineering properties of soils by insitu test as also laboratory analysis of samples collected during the course of the investigations.

2.2 SCOPE OF WORK

The scope of work includes :-

To conduct geotechnical investigation at 11 borehole locations from T-6 to T-10 are in POSITRA II and borehole T-4 and LB7 to LB11 in POSITRA III to a depth specified by FRH based on the termination criteria defined. Boreholes are located in the approach area.

Positra II locations : T-6 , T-7 , T-8 , T-9, T-10

Positra III locations : T-4 , LB7, LB8 , LB9, LB10, LB11

Bulk samples collected at T-1 to T-10 locations.

2.2.1 Mobilisation of Geotechnical Spread

- Mobilisation of suitable rotary drilling rig , drilling and sampling accessories and personnel to undertake investigation in all kind of soil and rock formation.
- Mobilisation of suitable positioning equipment and personnel for positioning the rig at above released boreholes location.
- Drilling of 100 mm diameter boreholes in all kinds of overburden soil , drilling and collection of 'NX' size rock samples in rocky strata.
- Collection of undisturbed & disturbed samples, conducting Standard penetration test in overburden soils at regular intervals .
- Conducting classification strength in the laboratory on the Soil & Rock samples.
- Submission of factual Geotechnical Report.

3.0 FIELD INVESTIGATIONS

3.1 MOBILISATION TO SITE

The rotary drilling rig was mobilised at positra to undertake the investigations at the proposed borehole locations . All requisite permissions from port / custom authorities were obtained in advance by the Base Manager.

3.2 EQUIPMENTS

The key Geotechnical Equipments mobilised to the site were as follows.

GEOTECHNICAL EQUIPMENTS

Drilling Rig with rock coring arrangement
Mud pump for water circulation
Drilling accessories
API drill string
N - Rods
NWM single and double tube core barrel
Thin walled shellby tubes (UDS)
SPT rods, Trip hammer
SPT - split spoon sampler
T.C & Diamond Drilling Bits
All other tools and tackles as required.

SURVEY EQUIPMENTS

DGPS TRIMBLE 4000 RS (Sub meter accuracy units)
CSI Modulator
CSI DTM Demodulator with active antenna
Base Texas Transmitting Tower
UHF Data link
ECHO Sounder
VHF radio with Walky talky .

3.3 POSITIONING

The positioning of the drilling rig to the borehole location was carried out using a TRIMBLE 4000 RS DGPS system. The base station (Reference station) for DGPS was installed near the light house at Okha towards the right of the approach to the existing Jetty (Okha port) at a station with known Geodetic values.

3.4 DRILLING , BORING AND SAMPLING

Borehole of 100 mm diameter was advanced using rotary drilling with sea water circulation in all kinds of overburden soils. Casings were driven up to hard rock strata to prevent collapse of Boreholes. When advancing the Boreholes in overburden soils , Standard Penetration Test & Undisturbed sampling were conducted at regular intervals in appropriate soil condition.

Rock coring of NX size was carried out using Tungsten Carbide bits and Diamond Bit. The drill string was coupled with Reamer Shell and NWM Double Tube core barrel fitted with a core catcher attached to the lower end for facilitating good recovery and retention of the core samples. Controlled water circulation, bit pressure and RPM were maintained during coring operations to ensure washing out of the core cuttings from the annular space between the outer drill string and hole and thus preventing the jamming of the drill string.

Rock coring was terminated after arriving desired depths as per the termination criterion provided by FRH which varied from location to location.

Standard penetration test (SPT) using split spoon sampler were conducted in over burden soils and in weathered rock where RQD was less than 25%, using 65.5 kgs hammer having free fall of 750mm on to anvil on top of the drill rod. The number of blows required to penetrate every successive 15cm and 7.5cm in to the strata up to maximum total depth of 45cm were recorded . The number of blows required for penetration between 15cm to 45cm were recorded as N-value for the particular stratum. The soil sample collected in the split spoon sampler were visually classified by experienced geotechnical engineer / engineering geologist on board and sent onshore for laboratory testing as disturbed samples (DS) after proper marking, sealing and logging.

3.5 DETAILS OF INVESTIGATION

POSITRA II BOREHOLES

Borehole T-6 : Borehole was extended upto 4.5m below ground level. Brownish silty fine sand with clay was observed upto 0.5 m. Limestone with 40% core recovery was encountered up to 2.0m depth. At 2.0m SPT was carried out which shows refusal and at the end of hole i.e at 4.5m SPT value 33 was observed. The ground water level was found at 3.65m..

Borehole T-7 : Borehole was extended upto 13.95 m below ground level. The overburden soil extended up 1.0m comprises of Brownish fine silty clay with sand was observed. After 1.0m highly weathered Limestone with low core recoveries was observed which is extended

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up to 5.50m. From 5.5m to end of the hole, completely weathered Limestone with considerable amount of silty sand and stiff clays was observed. In this zone SPT values were in the range of 30 to 41. In this borehole ground water was found at 2.90m depth.

Borehole T-8 : The borehole was drilled upto 15.0m below ground level. Overburden soil comprises of Reddish brown to greyish brown silty sand with stiff clay was extended upto 10.5 m. The SPT values observed in the range of 30 to 45. After 10.5 m Limestone deposits were observed upto the end of the hole. Intermittent seams of stiff clay with considerable amount of silty sand were encountered during the course of drilling. The highest value of CR & RQD have been observed at 13.5 - 15.0 m run. Ground water was found at 3.50m depth.

Borehole T-9 : The borehole was drilled upto 13.85m. below G.L. A thin layer of approximately 0.5 m. of overburden soil comprising of Dark brownish silty sands were encountered. The overburden soil is followed by Limestone stratification upto end of the hole. The highest CR & RQDs were observed in 12.3 to 13.8m run. Ground water was found at 3.19m depth.

Borehole T-10 : This borehole was drilled upto 13.50m below G.L. Overburden soils comprises of Dark brownish silty sands with Clays extends upto 9.0m depth. SPT hammer rebound was observed at 9.00 m. confirming the Limestone formation with good CR & RQDs up to end of the hole. Ground water was found at 3.11m depth.

POSITRA III BOREHOLES

BoreholeT-4 : This borehole was drilled upto 14.00m below G.L. The overburden soils comprising of dark reddish brown silty sand with clays were observed up to 2.0m depth. SPT value at 2.00 shows refusal confirming the Limestone formation afterwards. The highest value of CR & RQDs were observed in the 7.5 to 9.5 m run.

Borehole LB-7 : This borehole was drilled upto 20.33 m depth below G.L. The overburden soils comprising of dark reddish silty sands with clay extended up to 3.0 m .Below the top layer of overburden highly fractured limestone followed by completely weathered limestone was observed up to end of the borehole. The completely weathered Limestone is decomposed in nature occasionally showing seams of clay with considerable amount of silty sand. Ground was found at 5.13m depth.

Borehole LB-8 : This borehole was drilled upto 25.45m below G.L. The overburden comprises of Light brownish yellow to greyish yellow fine silty sands with clay extended up to 4.70 m where SPT value showing refusal. The overburden is followed by Limestone strata ,hard with good CR was extended upto 6.5 m. The hard Limestone becomes completely

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weathered, decomposed in nature from 6.5 m onwards. SPT values ranging between 17 to 42 have been observed till the end of the hole. Ground water was found at 5.98m depth.

Borehole LB-9: This borehole was drilled upto 12.40 m below G.L. A thin layer of about 0.5m overburden was observed with sandy soil. Dark brown to dark yellowish grey, with very closely to closely spaced fractures Limestone was observed below the existing overburden soil. Intermittent seams of clay with some amount of silty sand are encountered alternating with completely weathered Limestone. The highest value of 96% CR & 50% RQD was observed in 5.70-6.50m run. Ground water was found at 4.79m depth.

Borehole LB-10 : This borehole was drilled upto 18.45m depth below G.L. A thin layer of 0.6m overburden was observed, comprising of Brownish coarse to fine grained sand with clay. From 0.6 to 6.0 m hard Limestone was observed with highest CR of 91% and RQD of 57% at 0.6 to 1.60m run. From 6.0m to end of the hole completely weathered Limestone with SPT values ranging from 18 to 35 was observed. SPT refusal values were encountered and 14.0 and 14.5 m depth. Ground water was found at 5.17m depth.

Borehole LB-11: This borehole was drilled up to 19.29m below G.L. A thin layer of 0.22m overburden was observed comprising of silty sands. From 0.22m to end of the hole completely weathered Limestone was observed. The completely weathered Limestone is decomposed in nature with occasionally showing alternate seams of clay or silty sand. SPT values are ranging from 17 to 43. At the end of the hole SPT refusal was observed. Ground water was found at 4.27m depth.

Collection of Bulk samples : Bulk samples (10 kg each) were collected from T-1 to T-10 locations and sent to the laboratory for Compaction and C.B.R testing.

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CO-ORDINATES OF REFERENCE STATION

CLIENT : M/s Frederic R. Harris (India) Pvt. Ltd.

LOCATION : POSITRA

NAME OF STATION	LATITUDE (N)	LONGITUDE (E)
OKHA	22° 28' 39.19"	69° 04' 29.94"

4.0 GENERAL GEOLOGY

Geologically, all along the coastal tract between Positra, Dwarka & Okha Tertiary rocks are exposed with sand , clay , silt and Limestone.

4.1 HISTORY

The Tertiary era is most important in the physical history of the whole Indian region, the Himalayas as well as peninsula. It was during these ages that the most important surface features of the area were acquired and the present configuration of the country was outlined in the middle of the Eocene era and of earth movements set in which materially altered the whole geography of the Indian region. Two great events of Geodynamics and stand out prominently in these readjustments are one the final breaking up of the old Gondwana continent by the submergence of large segments of it underneath the sea, other the uplift of the Tethyan geocinclusal track of sea deposit to the north in to the lofty chain of the Himalayas.

4.2 GENERAL GEOLOGY

At the extreme East and West point of Saurashtra peninsula, tertiary era start range from Oligocene to pliocene is found overlying the Deccan trap. A trough fault was found in the Cambay area in early Eocene. This trough is known to extend beyond N.Latitude 24° north of Cambay and along the Bombay coast to the south. The traps are overlain by a fully Tertiary succession in these area.

4.3 STRATIGRAPHY

The western out crops is known as Dwarka beds of Pliocene age. Which mainly consists Gypsoferous clay , silt., Limestone. Dwarka beds cover in large area between Positra and Okha. A narrow strip of these rocks is also exposed east of the Okha Rann. The contact with the Limestone is usually marked in a thin layer of gypsiferous clays. The maximum thickness of Dwarka beds is found near the Khatumba village where the exposed cliff is about 125 feet high.

4.3.1 STRATIGRAPHY SUCCESSION

Porbandar	- Oolitic milliolite list	Pleistocene
Dwarka Beds	- Clays, silts , Limestone	Pliocene
Piram beds	- Conglomerates , grits and clays with mammalian fossils	Pliocene
Gogha Beds	- The bedded grits and sandstone exposed in the east coast.	Miocene to Pliocene

Gaj Beds - Variegated clays, marls , impure Lower Miocene
Limestone

4.3.2 AGE

A large number of determination of absolute age by radiometric method and Palaentological data are now available. As a result of the symposium held by the Geological Society of London on the Phenerozic time scale (Q.J.G.S London , Vol:120 1964) The limits are assigned to the different system in the tertiary era.

Pliocene	- 7 million years
Miocene	- 26 million years
Oligocene	- 38 million years

The Dwarka beds come under the Pliocene age.

4.4 INVESTIGATION AREA

The Geology of the area under study and from the investigation carried out which covered by silty clay and somewhere small hillocks (Limestone) are present in this area. The Limestone strata shows various degrees of weathering. The present investigations carried out in this region, it was observed that the strata shows alternate layers of weathered to completely weathered , fine grained hard Limestone with characteristic sign of Tertiary era.

The average water level around the area varies from 3 to 6m depth, it was observed during investigation from the boreholes and local sources from April 1997 to May 1997.

5.0 LABORATORY ANALYSIS

The soil and rock samples collected in the course of field investigation were visually classified and logged by Geotechnical engineer / Engineering Geologist. The samples were thereafter sealed prior to dispatch to the laboratory for carrying out tests for the various physical properties of the samples as prescribed by M/s Frederic R. Harris (India) Pvt. Ltd.

The various types of tests carried out on different kinds of sample are as enumerated below.

A) Clay / Silty samples

- a) Natural moisture content,
- b) Atterberg limits,
- c) Sieve and hydrometer analysis,
- d) Wet and dry density
- e) Triaxial shear test , consolidated undrained shear test with pore pressure (CUPP).
- f) Unconfined compression test,
- g) Consolidation test.

B) Sandy samples

- a) Natural moisture content,
- b) Unit weight ,
- c) Sieve analysis,
- d) Drained direct shear.

C) Rock samples

- a) Natural Moisture content
- b) Bulk and dry density
- c) Specific gravity
- d) Uniaxial compression strength
- e) Point load test

D) Bulk samples

- a) Atterburg Limits
- b) Grain size analysis
- c) Proctor compaction test
- d) Lab. C.B.R test

The results of laboratory analysis are given in **Annexure 5**

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6.0 ENGINEERING ANALYSIS:

From the laboratory testing some of the engineering properties of the overburden soils , Limestone and Bulk samples are given below for design purpose.

OVERBURDEN SOILS

Liquid limit range	:	22 % to 70 %
Plastic limit range	:	14 % to 28 %
Wet density range	:	1.98 to 2.09 gm/cc
Dry density range	:	1.65 to 1.85 gm/cc
Natural moisture content variation	:	13 to 20 %
Triaxial unconfined undrained		
Cohesion	:	147 to 194 Kpa
Angle of internal friction	:	0°
Unconfined compression test		
Cohesion	:	128 to 175 Kpa
Coefficient of permeability (K)	:	1.7×10^{-7} to 3.6×10^{-4} cm/sec

LIMESTONE

Liquid limit range	:	24 % to 83 %
Plastic limit range	:	15 % to 37 %
Wet density range	:	1.75 to 1.95 gm/cc
Dry density range	:	1.37 to 1.65 gm/cc
Natural moisture content variation	:	18 to 34 %
Triaxial unconfined undrained		
Cohesion	:	35 to 134 Kpa
Angle of internal friction	:	0°
Unconfined compression test		
Cohesion	:	31 to 103 Kpa
Coefficient of permeability (K)	:	1.6×10^{-7} to 2.8×10^{-4} cm/sec
Unconfined compressive strength	:	7.5 to 50.4 Mpa
Point load strength	:	0.67 to 7.84 Mpa

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BULK SAMPLES

Liquid limit range : 21 to 25 %
Plastic limit range : 13 to 15 %

Compaction

Maximum dry density : 1.81 to 1.98 gm/cc
Optimum moisture content : 9.8 to 14.8 gm/cc

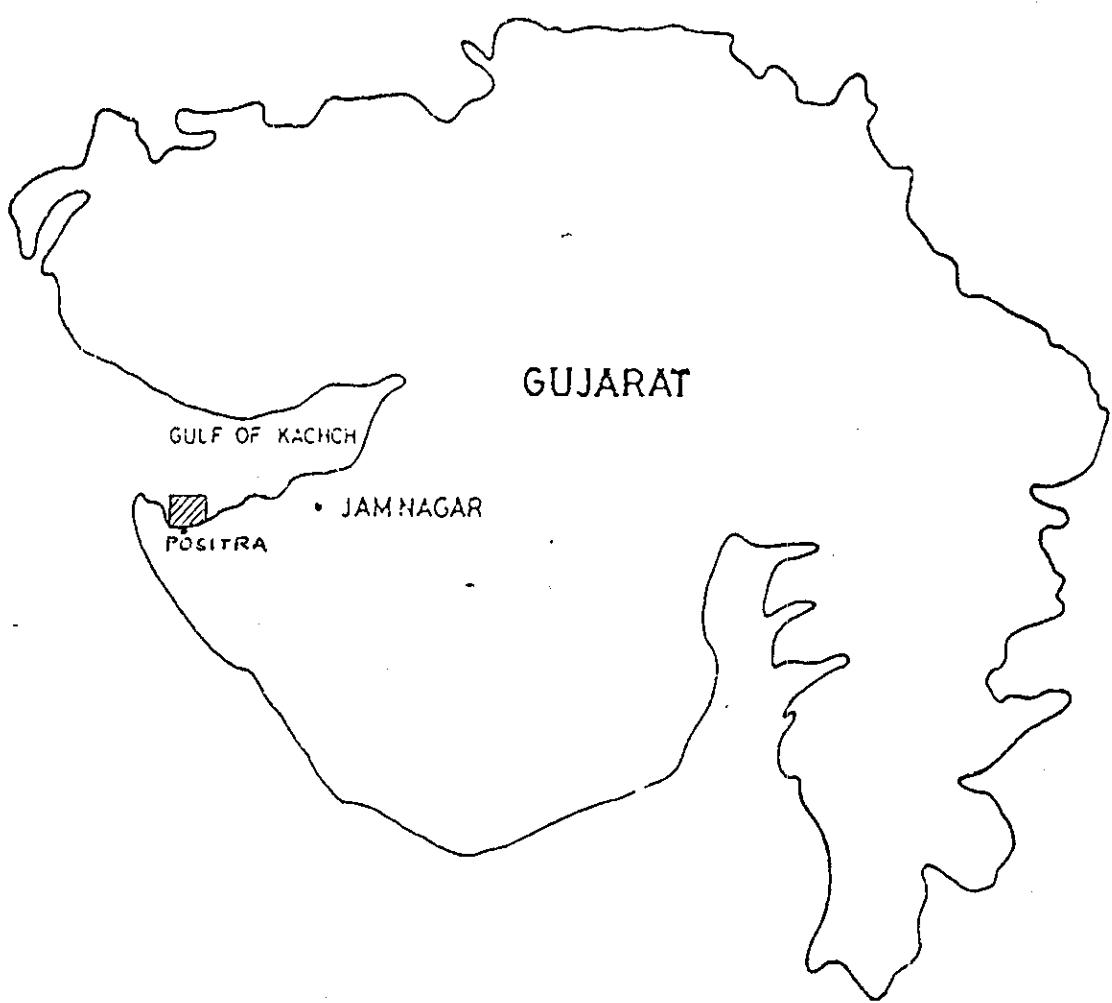
California bearing ratio value

for 2.5 mm : 9.4 to 15.9 %
for 5.0 mm : 7.6 to 14.2 %

ANNEXURE 1

PROJECT : SOIL INVESTIGATION GULF OF KACHCH
LOCATION : POSITRA

FIG-1

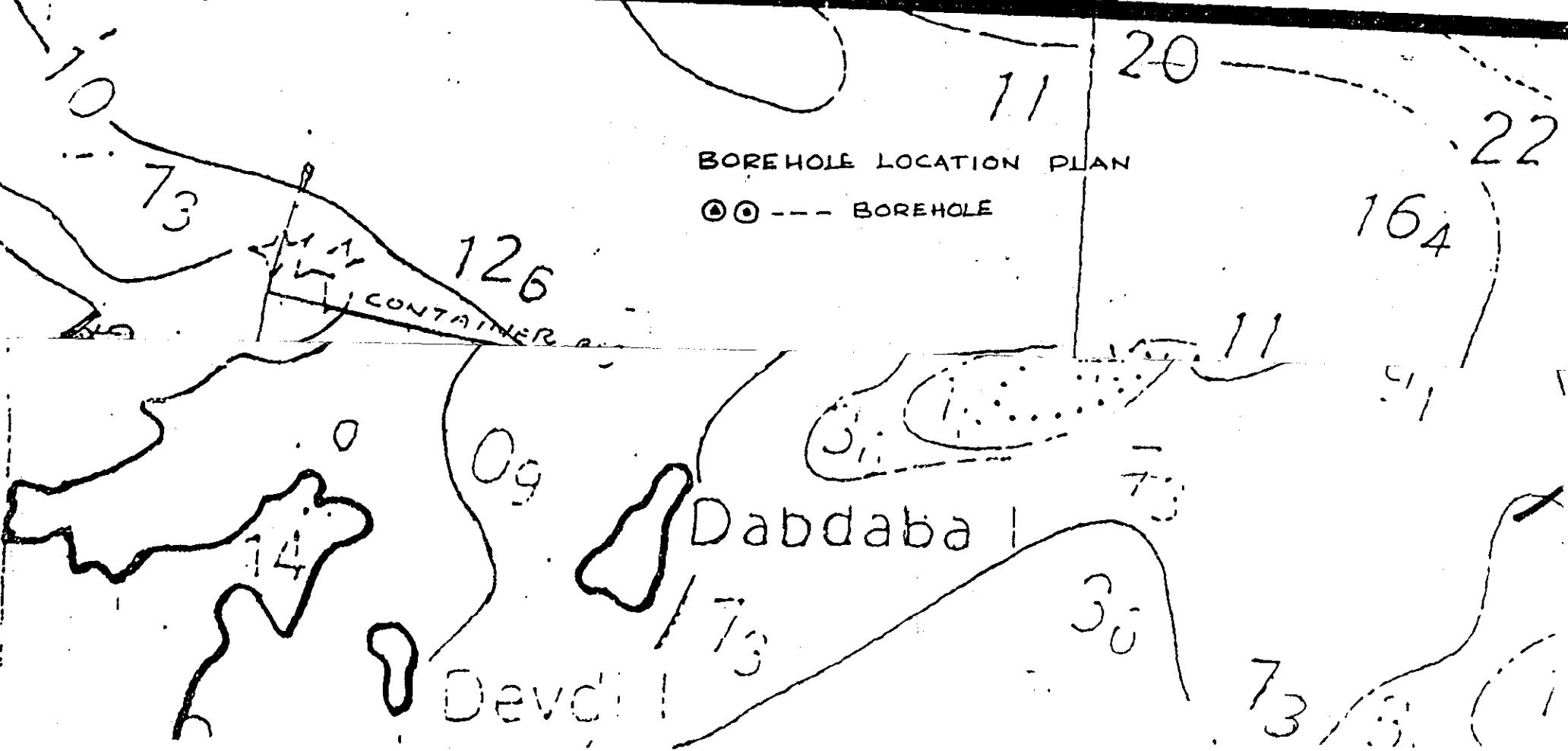


GENERAL LOCATION

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ANNEXURE 2



Legend

Locations of onshore boreholes (LB 1 to LB 10) shown thus : •

PROPOSED LOCATIONS OF ONSHORE BOREHOLE:

FIGURE NO. D-1

Scale : 1:26,000

BOREHOLE CO-ORDINATES , REDUCED AND GROUND WATER LEVELS

PROJECT : ON-SHORE POSITRA

BORE HOLE NO.	CO-ORDINATES GEOGRAPHICAL		REDUCED LEVEL ABOVE C.D M	GROUND WATER LEVEL M
	LONGITUDE	LATTITUDE		
T-10	69°11'16.00"	22°25'03.00"	4.943	3.11
T-9	69°10'59.00"	22°25'03.00"	6.719	3.19
T-8	69°10'41.00"	22°24'43.00"	5.412	3.50
T-7	69°10'29.00"	22°24'34.00"	7.197	2.90
T-6	69°11'10.00"	22°24'38.00"	5.443	3.65
T-4	69°10'35.00"	22°23'53.00"	18.685	
LB-11	69°10'56.00"	22°24'14.00"	6.648	4.27
LB-10	69°11'40.58"	22°23'53.00"	6.205	5.17
LB-8	69°11'29.28"	22°23'36.35"	8.50	5.98
LB-7	69°11'21.80"	22°23'37.00"	9.275	5.13
LB-9	69°11'30.69"	22°23'49.22"	5.650	4.76

ANNEXURE 3

VL : LAB VANE SHEAR TEST UC : UNCONFINED COMP.

UC : UNCONFINED COMP.

PP-POCKET PENTROMETER

1631

THE FINAL TEST INGRAMS

M : LAB VAGIN SMEAR TEST

UC : UNCONFINED COMP.

PP: POCKET PERIMETER

178

TU: TRIAXIAL TEST UNDRAINED

ATTERBERG LIMIT		UNIT WT.		SHEAR STRENGTH		DEPTH SAMPLE	DEPTH ^a RUN NO.	TIME DATE	TIME FROM TO	SCORING			PENETRATION / NO. OF BLOWS							BORE HOLE NO. T-9							
Plastic Limit O	Water Content %	Liquid Limit L	Dry Bult D	V.L. P.P. UC TU	KNU/CUM KG/CM ²					CR %	SCR %	RGD %	16cm	7.5cm	7.8cm	7.6cm	7.5cm	Type SAMPLE No.	SAMPLE No.	SAMPLE No.	METERS DEPTH IN MM	Sheet 1 of 2					
										20	40	60	80	100	15	20	25	200	400	600	800	1000	Date: 29 Apr.97 to 30 Apr.97				
^a All depths are in meter below bed level																											
										0.00	0.00	0.20	28-Apr	08 00	08 11												
										0.60	0.70			08 11	08 30												
										1.00	0.70	1.00		08 30	09 00	NH											
										1.00	1.00	1.10		08 00	08 20												
										2.00	1	1.00	2.00		08 20	1100	23	10	NH								
										3.00																	
										4.00	2	3.00	4.10		1100	1300	36	26	20								
										4.00	4.10	4.40		1300	1430	NH											
										5.00	4.80	4.95		1430	1500												
										6.00	4.95	5.00		1500	1700	NH											
										7.00	6.00	7.00		1700	1730												
										7.00	7.80	7.95		1730	1845	NH											
										8.00	7.80	8.00		1845	1920												
										8.00	8.00	8.35		30-Apr	08 00	08 00	NH										
										8.00	8.00	8.35		08 00	08 20	REC											
										9.00	8.00	8.00		08 20	1040	NH											
										9.00	9.00	9.45		1040	1110												
										10.00	9.00	10.00		1110	1300												
V.L: LAB VANE SHEAR TEST		UC : UNCONFINED COMP.		PP: POCKET PENETROMETER		TEST		TU: TRIAXIAL TEST UNDRAINED																			
PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.																							CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.				

IV. LAB VANE SHEAR TEST

UC : UNCOMPRESSED COMP.

PP: POCKET PENETROMETER

1031

TU: TRIAXIAL TEST UNDRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS INDIA PVT.LTD.

ATTERBERG LIMIT	UNIT WT.	SHEAR STRENGTH	DEPTH	SAMPLE	DEPTH*	TIME	COKING	PENETRATION / NO. OF BLOWS	METERS	BORE HOLE NO. T-8						Sheet 1 of 2										
										RUN NO.	FROM	TO	DATE	FROM	TO	CR %	SCR %	RQD %	16cm	7.6cm	7.6cm	7.6cm	7.6cm	CO ORDINATES	69 10 41.00 E 22 24 43.00 N	Date: 1 May.97 to 2 May.97
																	TYPE	NO.	DEPTH IN M	SAMPLE	SAMPLE	SAMPLE				
Plastic Limit	Water Content	KN/CUM	V.L	Sample	Depth	Time	Coring	Penetration / No. of Blows	Meters																	
Line O	%	Liquid Limit	Dry Bulk	PP	From	To	Date	16cm	7.6cm	7.6cm	7.6cm	7.6cm	7.6cm	COORDINATES	69 10 41.00 E 22 24 43.00 N	Site	POSITRA	Date: 1 May.97 to 2 May.97								
		CL	LL	UC											METHOD	Rotary										
		O	LL	TU											REDUCED LEVEL	5.412 m above C.D	G.W.L. — 3.60 m	100 MM	CORE DIA. 55 mm							
20	40	60	80	100	16	20	26	200	400	600	800	1000														
*All depths are in metres below bed level																				Symbol	DESCRIPTION					
0.00	0.00	0.20	1-May	1000	1010										DS	0.0										
		0.60	0.70		1010	1020									DS	0.5										
1.00	0.60	1.80		1020	1100	NH																				
		1.60	1.90		1100	1120																				
2.00																										
3.00	1.00	3.00		1120	1240	NH																				
		3.00	3.45		1240	1310																				
4.00	3.00	4.60		1310	1420	NH																				
		4.80	4.75		1420	1440	REC.																			
5.00																										
6.00	4.60	6.00		1500	1530	NH																				
		6.00	6.45		1530	1700																				
7.00	6.00	7.00		1700	1830	NH																				
		7.60	7.00		1830	1800																				
8.00																										
9.00	6.00	8.00	2-May	1800	1830	NH																				
		6.00	8.40		1830	1000																				
10.00	6.00	10.00		1900	1140	NH																				
VL: LAB VANE SHEAR TEST		UC : UNCONFINED COMP		PP: POCKET PENETROMETER TEST		TU: TRIAXIAL TEST UNDRAINED																				
PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.																				CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.						

VI. LAB VANE SHEAR TEST

UC : UNCONFIRMED COMP

PP. POCKET PENETROMETER

TEST

TU. TRIAXIAL TEST UNDRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R. HARRIS INDIA PVT. LTD.

VI. LAB VANE SHEAR TEST

UC : UNCONFINED COMP.

PP: POCKET PENETROMETER

TEST

THE TRIAXIAL TEST UNCONSTRAINED

ATTERBERG LIMIT		UNIT WT.		SHEAR STRENGTH		SAMPLE	DEPTH	DEPTH'	TIME	CORING	PENETRATION / NO. OF BLOWS							N - VALUE	TYPE	No.	SAMPLES	METERS IN	BORE HOLE NO. T- 7		Sheet 1 of 2	
Water Content %	Liquid Limit	Dry Bulk	V.L. PP UC TU	KN/CUM	KO/CM ²						FROM	TO	FROM	TO	CR %	SCR %	RQD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm	CO ORDINATES	69 10 29.008 E 22 24 34.00 N	POSITRA Rotary	Date: 3 May. 97 to 4 May. 97
Plastic Limit																										
Water Content %	Liquid Limit	Dry Bulk	V.L. PP UC TU	KN/CUM	KO/CM ²																					
20	40	40	80	100	15	20	25	200	400	600	800	800	1000													
"All depths are in metre below bed level"																										
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PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

ATTERBERG LIMIT		UNIT WT.	SHEAR STRENGTH		DEPTH	SAMPLE	RUN NO.	DEPTH*		TIME	CORING		PENETRATION / NO. OF BLOWS						BORE HOLE NO. T-6			Sheet 1 of 1											
			KN/CUM					FROM			CR %	SCR %	RQD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm	N	TYPE	SAMPLE NO.	SAMPLES	DEPTH IN METERS	CO ORDINATES	69 11 10.00 E	22 24 38.00 N	SITE	POSITRA	Date: 4 May.97				
Plastic Limit	Water Content %	Liquid Limit	Dry	P.P.				V.L.	U.C.		PP	UC	TU	20	40	80	100	15	20	25	400	800	1000	CO ORDINATES	69 11 10.00 E	22 24 38.00 N	SITE	POSITRA	Date: 4 May.97				
O	□	●	Bult	UC				TU	PP		100	200	400	800	1000	20	40	80	100	15	20	25	400	800	1000	CO ORDINATES	69 11 10.00 E	22 24 38.00 N	SITE	POSITRA	Date: 4 May.97		
*All depths are in metres below bed level																																	
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IVL: LAS VANE SWELL TEST

UC : UNCONFINED COMP

PP: POCKET PENETROMETER

TEAT

THE TRIAXIAL TEST UNSTRAINED

PREPARED BY : COASTAL MARINE CONSTR

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

ATTERBERG LIMIT		UNIT WT.	SHEAR STRENGTH		SAMPLE RUN NO.	DEPTH FROM TO	DATE FROM TO	TIME Coring	PENETRATION / NO. OF BLOWS							TYPE SAMPLE No.	SAMPLES IN METERS	BORE HOLE NO. T-4		Sheet 1 of 2		
		KN/CuM	KG/CM ²						CR %	SCR %	RQD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm		COORDINATES	69 10 35.00 E	22 23 53.00 N	Date: 6 May, 97 to 7 May, 97	
Plastic Limit %	Water Content %	Liquid Limit	Dry Bulk	o VL	o PP	o UC	o TU										SITE	POSITRA	ROTARY			
O	□	□	□	□	□	□	□	□	□	□	□	□	□	□	□	□	REDUCED LEVEL	18.686 M above chart datum	DIA. OF BORE HOLE	100 MM	CORE DIA. 55 mm	
20	40	60	80	100	15	20	25	200	400	600	800	1000										
*All depths are in metres below bed level																						
0.00		0.00	0.50		8-May	08 00	08 20										DS		6.0	-	-	
		0.50	0.70			08 20	08 40										DS		6.5	-	-	
1.00																						
2.00		0.70	2.00			08 40	1030	NH											2.0	-	-	
		2.00	2.10			1030	1120															
3.00	1	2.00	3.50			1100	1300	36	26	NH							N>100	SPT				
		3.50	3.95			1300	1340															
4.00																						
6.00	2	3.50	6.00			1340	1500	28	18	NK							22	SPT				
		6.00	6.48			1500	1520															
6.00		5.00	8.50																			
		6.00	6.88			1500	1520	NK														
7.00		6.50	7.50			1520	1546	30	17	NK							N>100	SPT				
		7.50	7.52			1546	1590															
8.00																						
8.00		7.50	8.50		7-May	08 00	1220	60	64	62												
10.00																						
VL: LAB VANE SHEAR TEST		UC : UNCONFINED COMP.		PP: POCKET PENETROMETER		TEST		TU: TRIAXIAL TEST UNDRAINED														
PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.																						CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

MC: LAB WORK SHEET TEST

TVC UNCONFIRMED COMP

PP. POCKET PERIMETER

TEST

THE TRIAXIAL TEST UNCRANED

VR: LAB VANE SHEAR TEST

UC : UNCONFINED COMP

PP POCKET PENETROMETER

TEST

TU. TRIAXIAL TEST UNDRAINED

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

VI. LAB VANE SMEAR TEST

UC : UNCONFIRMED COMP.

PP: POCKET PENETROMETER

TEST

TU: TRIAXIAL TEST UNDRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS/INDIA/PVT.LTD.

ATTERBERG LIMIT		UNIT WT.	SHEAR STRENGTH		SAMPLE RUN NO.	DEPTH FROM TO DATE	TIME FROM TO	CORING	PENETRATION / NO. OF BLOWS							N = VALUE	TYPE SAMPLE NO. SAMPLES	METERS DEPTH IN METERS	BORE HOLE NO. LB-10				Sheet 1 of 2 CO ORDINATES 69 11 40.58 E 22 23 39.53 N SITE POSITRA METHOD Rotary REDUCED LEVEL 6.205 M above chart datum G.W.L.—6.17m DIA. OF BORE HOLE 100 MM CORE DIA. 55 mm Date: 19 May.97 to 22 May.97			
		KN/CUM	KG/CM ²						V.L.	V.L.	P.P.	UC	TU	CR %	SCR %	RQD %	15cm	7.5cm	7.5cm	7.5cm	7.5cm					
Plastic Limit %		Water Content %	Liquid Limit %	Dry Bulk					VL	V.L.	P.P.	UC	TU													
O		O	O	O					20	40	60	80	100	15	20	25	200	400	600	800	1000					
*All depths are in metres below bed level																										
0.00	0.00	0.50	18-May	1300	1310																					
1.00	1	0.80	1.80		1400	1425																				
2.00	2	1.80	3.33		1600	1800	28	20	16																	
3.00	3	3.33	4.83		1800	1920	44	40	21																	
4.00	4	4.83	8.00		1920	2120	62	55	36																	
5.00	5.00	6.44	20-May	08 00	09 00																					
6.00	6.00	7.60		08 00	1100	NH																				
7.00	7.00	7.60		1100	1135	NH																				
8.00	8.00	8.00			1135	1315	NH																			
9.00	9.00	8.46			1315	1400	NH																			
10.00	8.00	10.80			1400	1630	NH																			

VL: LAB VANE SHEAR TEST

UC: UNCONFINED COMP.

PP: POCKET PENETROMETER

TEST

TU: TRIAXIAL TEST UNDRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

VI. LAB VANE SHEAR TEST

UC : UNCONFINED COMP.

PP. POCKET PENETROMETER

TEST

TU- TRIAXIAL TEST UNDRAINED

CLIENT : FREDERIC R.HARRIS INDIA PVT.LTD.

ATTERBERG LIMIT	UNIT WT.	SHEAR STRENGTH	DEPTH SAMPLE RUN NO. DEPTH FROM TO DATE FROM TO CORING CR % SCR % ROD % 15cm 7.5cm 7.5cm 7.5cm 7.5cm	TIME N + VALUE PENETRATION / NO OF BLOWS 1CM/20BLOWS REBOUND N>100	BORE HOLE NO. LB-8						Sheet 1 of 3				
					KN/CUM	KG/CM ²	VL	PP	UC	TU	SAMPLE	TYPE	NO.	METERS	CO ORDINATES
Plastic Limit	Water Content	Liquid Limit	Dry Bulk	V.L.	P.P.	UC	TU								69 11 29.26 E
O	D	L	B												22 23 36.35 N
20	40	60	80	100	15	20	25	200	400	600	800	1000			POSITRA
															Rotary
															8.50 M. above chart datum
															G.W.T.— 5.98 m
															100 MM
															CORE DIA. 55 mm

All depths are in metres below bed level.

Symbol	DESCRIPTION
0.0 - X -	Light brownish yellow to greyish yellow, fine silty sand and CLAY
0.5 - X -	
1.0 - X -	
1.5 - X -	
2.0 - X -	
3.0 - X -	
4.0 - X -	
4.3 - X -	
4.7 - X -	Light greyish yellow, fine to medium grained ,fractures are extremely closely to very closely spaced, weathered LIMESTONE.
6.0 - X -	Brownish grey to yellowish brown , fine grained , completely weathered LIMESTONE , with some silty sand and clay.
8.0 - X -	
9.0 - X -	
10.0 - X -	

VL : LAB VANE SHEAR TEST UC : UNCONFINED COMP
 PP : POCKET PENETROMETER TEST
 TU : TRIAXIAL TEST UNDRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

VL: LAB VAMPIRE SMELL TEST

UC : UNCOMPRESSED COMP

PP: POCKET PENITROMETER

150

THE TRIANAL TEST LUMORANT

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

VI. LAB VANE SHEAR TEST

UC - UNCONFINED COMP

PP: POCKET PENETROMETER

168

TU: TRIAXIAL TEST UNDRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS(INDIA)PVT.LTD.

YL-LAB VANE SMEAR TEST

UC : UNCONFIRMED COMP.

PP POCKET PENETROMETER

133

THE TRAVERSAL TEST UNSTRAINED

PREPARED BY : COASTAL MARINE CONSTRUCTION & ENGINEERING LTD.

CLIENT : FREDERIC R.HARRIS INDIA PVT.LTD.

8	3	8831	0
8	12	8431	0
9	3	8830	0
9	12	8430	0
10	3	8131	0
10	12	7431	0
11	3	6030	0
11	12	5730	0
12	3	7531	0
12	12	7031	0

YEAR - 1976

1	3	8231	0
1	12	7431	0
2	3	7429	0
2	12	6729	0
3	3	8131	0
3	12	7631	0
4	3	8329	0
4	12	7830	0
5	3	8331	0
5	12	8231	0
6	3	8530	0
6	12	8130	0
7	3	8231	0
7	12	7931	0
8	3	8931	0
8	12	8631	0
9	3	9230	0
9	12	8930	0
10	3	8631	0
10	12	8431	0
11	3	7230	0
11	12	7230	0
12	3	6131	0
12	12	6131	0

YEAR - 1977

1	3	6331	0
1	12	6131	0
2	3	7828	0
2	12	7428	0
3	3	8631	0
3	12	8230	0
4	3	8330	0
4	12	7730	0